



Bergvesenet

Postboks 3021, 7002 Trondheim

Rapportarkivet

Bergvesenet rapport nr BV 3369	Intern Journal nr	Internt arkiv nr Boks nr 20	Rapport lokalisering Nordland	Gradering
Kommer fra ..arkiv	Ekstern rapport nr BNN	Oversendt fra	Fortrolig pga	Fortrolig fra dato:
Tittel Målinger Mofjell Grube. Nr. 2				
Forfatter		Dato 19	Bedrift Bergverkselskapet Nord-Norge A/S	
Kommune Rana	Fylke Nordland	Bergdistrikt Nordlandske	1: 50 000 kartblad	1: 250 000 kartblad
Fagområde	Dokument type	Forekomster		
Råstofftype	Erneord			
Sammendrag				

Linse III

Stas	Azimuth	Δx	Δy	X	Y	dybde	L.gg
30*	105.935			925 352,440	43 721,680	-78,71	
33*	189,747			+ 2,151	31,664		
34*	95,682	+2,151	+31,664	354,591	753,344	-77,255	
33*	95,682			354,591	753,344		
34*	206,590			- 1,056	+29,587		
35*	102,272	-1,056	+29,587	353,535	782,931	77,597	
34*	102,272			353,535	782,931		
35*	194,704			+ 1,522	+32,027		
36*	96,976	+1,522	+32,027	355,057	814,958	75,676	
35*	96,976			355,057	814,958		
36*	192,168			+ 1,522	+21,522		
37*	89,144	+3,706	+21,522	358,763	836,480	-74,757	
36*	89,144			358,763	836,480		
37*	210,767			+ 1,522	+31,270		
38*	99,911	+0,044	+31,270	358,807	867,750	74,756	
37*	99,911			358,807	867,750		
38*	196,629			+ 1,296	+23,824		
39*	96,540	+1,296	+23,824	360,703	891,574	74,840	
37*	99,911			350,807	891,574		
38*	196,629			+ 1,119	+20,470		
39*	96,540	+1,119	+20,470	351,921	912,044		
37*	99,911			358,807	867,750		
38*	196,629			+ 1,119	+20,470		
39*	96,540	+1,119	+20,470	359,921	888,220	74,840	
37*	99,911			359,921	888,220		
38*	180,821			+ 8,307	+22,366		
40*	77,361	+8,307	+22,366	368,228	910,586	74,667	
39*	77,361			368,228	910,586		
40*	125,700			+ 13,265	+0,638		
b h	3,061	+13,265	+0,638	381,493	911,224		

I	S	Horisontalaust og høydeforskjell	Anmerkninger
		$33^* - 34^* = 31.737$	30^* og 33^* er innmålt fra kommunen
		$34^* - 35^* = 29.606$	$33^* - 40^*$ er horisontalauststand og høydeforskjell tatt fra tidligere beregninger
		$35^* - 36^* = 32.063$	
		$36^* - 37^* = 21.837$	
		$37^* - 38^* = 31.270$	
		$38^* - 39^* = 26.500$	
		$38^* - 39^* = 20.500$	
		$39^* - 40^* = 23.859$	
		$40^* - \text{berthull} = 13.28$	Dimantberthull nr 701

Stasi	Azimuth	Δx	Δy	x	y	dybde	l.gg
39*	77.361			368.228	910.586		
40*	201.806			+ 63.60	+ 21.653		
41*	79.167	+7.350	+21.653	375.578	932.239		
Går							
35*	96.976			355.057	814.958	-75.676	
36*	199.754						
Hp1	96.730	+1.923	+37.406	356.980	852.364	-78.287	
36*	96.730						
Hp1	200.816						
Hp2	97.546	+1.482	+38.428	358.462	890.792	-77.840	
Hp1	97.546						
Hp2	177.980						
Hp3	75.526	+11.625	+28.735	370.087	909.527	-78.257	
Hp2	75.526						
Hp3	203.174						
Hp4	78.700	+5.579	+16.048	375.666	925.575	-80.006	
Hp3	78.700						
Hp4	156.883						
37*	35.583	+10.705	+6.696	386.371	942.271	-78.806	
Hp4	35.583						
37*	211.267						
38*	46.850	+16.281	+14.744	402.652	957.015	-79.914	
37*	46.850						
38*	257.216						
39*	104.066	-1.678	+26.239	400.974	983.254	-78.844	

Anmerkungen

Forts. von S. 1

$$40^* - 41^* = 22.866$$

3.46

$$\underline{36^* - Hp1 = 37.465 \cdot 98.557}$$

$$+ 0.849$$

$$37.455$$

$$\underline{Hp1 - Hp2 = 38.46 \cdot 99.260}$$

$$+ 0.447$$

$$38.457$$

$$\underline{Hp2 - Hp3 = 31.000 \cdot 100.856}$$

$$- 0.417$$

$$30.997$$

$$\underline{Hp3 - Hp4 = 17.08 \cdot 106.530}$$

$$- 1.749$$

$$= 16.990$$

$$\underline{Hp4 - 37^* = 12.655 \cdot 104.228}$$

2.04

$$- 0.840$$

$$12.627$$

1.98

3.12

$$\underline{37^* - 38^* = 22.08 \cdot 106.493}$$

$$- 2.248$$

$$21.965$$

$$\underline{38^* - 39^* = 26.295 \cdot 99.310}$$

2.845

3.63

$$+ 0.285$$

$$26.293$$

stas	Azimuth	Δx	Δy	x	y	dybde	logg
37*	46.850			402.652	957.015		
38*	262.911						
38 ^I	109.761	-1.395	+9.024	401.257	966.039	-80.32	
38*	109.761						
38 ^I	242.932						
38 ^{II}	152.693	-14.872	+13.664	386.385	979.703	-78.725	
38*	104.066			400.974	983.254		
39*	192.923						
40*	102.039	-0.747	+23.329	400.227	^{44.} 06.583	-80.301	
39*	102.039						
40*	137.495						
40 ^N	39.534	+7.482	+5.352	407.709	011.935	-80.772	
39*	102.039			400.227	^{44.} 06.583		
40*	280.112						
40 ^I	182.151	-14.230	+4.098	385.997	^{44.} 010.681	-78.379	82.8
40*	182.151			385.997			
40 ^I	129.405						
40 ^{II}	111.556	-3.530	+19.233	382.467	^{44.} 029.914	-79.342	
39*	102.039			400.227	^{44.} 06.583		
40*	210.494						
41*	112.533	-6.996	+35.075	393.231	41.658	80.168	85.0
40*	112.533			393.231	41.658		
41*	217.676						
41 ^I	130.209	-9.611	+18.710	383.620	60.368	79.636	
41*	130.209			383.620	60.368		
41 ^I	174.233						
41 ^{II}	104.442	-1.683	+24.089	381.937	84.457	78.991	84.4

Linse 3

3

I	S	Anmerkungen	
2.845	2.70	$38^* - 38^I$ 109.761 $9.135 \cdot 101.821$	$-0.261 = 9.131$
2.51	2.63	$38^I - 38^{II} = 20.25 \cdot 95.360$	$+1.475 \quad 20.196$
3.50	2.70	$39^* - 40^* = 23.35 \cdot \frac{101.793}{\cancel{101.524}}$	23.341
		-0.657	Milt
2.585	3.215	$40^* - 40^N = 9.265 \cdot 107.585$	9.199
		-1.101	Nord
2.60	3.82	$40^* - 40^I = 14.825 \cdot 96.984$	14.808
		$+0.702$	Sdr
3.60	3.42	$40^I - 40^{II} = 19.57 \cdot 102.572$	19.554
		-0.790	Sdr
2.635	3.28	$40^* - 41^* = 35.77 \cdot 100.912$	35.766
		-0.512	
3.40	3.265	$41^* - 40^I = 21.045 \cdot 99.983$	21.034
		$+0.667$	Sdr
2.91	3.25	$41^I - 41^{II} = 24.15 \cdot 99.192$	24.148
		$+0.305$	Sdr Forts. side 30

4

Linse III Sør Øst

Stas	Azimuth	Δx	Δy	x	y	dybde	ligg
39*	77.361			925 368.228	43 910.586	-74.667	
40*	253.952			-10.606	+19.796	0.010	
12	131.313	-10.606	+19.796	357.622	930.382	74.677	
40*	131.313			357.622	930.382	-74.677	
12	155.849			+6.404	+31.325	+3.766	
22	87.162	+6.404	+31.325	364.026	961.707	70.911	
12	87.162			364.026	961.707	70.911	
22	180.437			+13.591	+24.357	+4.042	
32	67.599	+13.591	+24.357	377.617	986.064	-66.850	
22	67.599			377.617	986.064	-66.850	
32	217.194			+4.760	+19.546		
42	84.793	+4.760	+19.546	382.377	44 005.610	-63.838	
32	84.793			382.377	5.610	-63.838	
42	235.383			-9.670	+29.485		
52	120.176	-9.670	+29.485	372.707	35.095	-64.649	✓
42	120.176			372.707	35.095	64.649	
52	175.995			+1.421	+23.589	-0.335	
62	96.171	+1.421	+23.589	374.128	58.684	65.004	69.6
52	96.171			374.128	58.684	65.004	
62	201.821			+1.081	+34.257	-2.375	70.98
72	97.992	+1.081	+34.257	375.209	92.941	68.379	69.6
52	97.992			375.209	92.941	-67.379	
72	188.590			+7.981	+37.303	+1.272	
82	86.582	+7.981	+37.303	383.190	130.244	-68.107	
72	86.582			383.190	130.244	-66.107	
82	173.236			+8.399	+11.492		
92	59.818	+8.399	+11.492	391.589	141.736	-68.237	
82	59.818			391.589	141.736	-67.237	
92	221.597			+9.970	+33.174		
102	81.415	+9.970	+33.174	401.559	174.910	68.627	71.2
32	286.582						
72	370.723			375.209	92.941	67.379	
112	57.305	+9.565	+12.057	+2.865	12.057		
				381.774	104.998	67.431	

Fra linse 3 over "Drekket" til stotakull

4

I	S		Flamerkriger
319	285	$\frac{40^2 - 1^2 = 2246 \cdot 99.064}{+ 0.330} =$	22.458
246	310	$\frac{1^2 - 2^2 = 32.125 \cdot 93.795}{+ 3.126} =$	31.973
294	351	$\frac{2^2 - 3^2 = 2811 \cdot 92.074}{+ 3.491} =$	27.892
3075	3645	$\frac{3^2 - 4^2 = 20.265 \cdot 92.310}{+ 2.442} =$	$\frac{20.117}{24}$
354	268	$\frac{4^2 - 5^2 = 31.03 \cdot 99.899}{+ 0.049} =$	31.030 1446 - 13100
2445	334	$\frac{5^2 - 6^2 = 23.665 \cdot 103.363}{- 1.250} =$	23.632
3065	263	$\frac{6^2 - 7^2 = 34.40 \cdot 105.448}{- 1.250 \quad - 2.940} =$	$\frac{34.274}{23.632}$
2225	398	$\frac{7^2 - 8^2 = 38.15 \cdot 100.806}{- 0.263 \quad - 0.483} =$	38.147
372	302	$\frac{8^2 - 9^2 = 14.24 \cdot 101.921}{- 0.430} =$	14.234
2765	338	$\frac{9^2 - 10^2 = 34.64 \cdot 100.010}{- 0.005} =$	34.640
226	231	$\frac{7^2 - 10^2 = 15.39 \cdot 100.42}{- 0.102} =$	15.39 Forts. side 5

Stus	Azimuth	Δx	Δy	x	y	dybde	lygg
9 ²	81.415			401.559	174.910	-66.627	
10 ²	217.559			+ 0.524	+ 32.496		
11 ²	98.974	+ 0.524	+ 32.496	402.083	207.406	-66.712	
10 ²	98.974			402.083	207.406	-65.712	
11 ²	207.243			- 3.123	+ 31.877		
12 ²	106.217	- 3.123	+ 31.877	398.960	239.285	- 66.005	
				398.960	239.283		
11 ²	106.217			398.960	239.283	-66.005	
12 ²	191.157			+ 1.260	+ 30.538		
13 ²	97.374	+ 1.260	+ 30.538	400.220	269.821	-68.123	
10 ²	298.974			401.559	174.910	66.627	
10 ²	342.672			+ 12.817	+ 9.829		
H _p I	41.646	+ 12.817	+ 9.829	414.376	184.739	-67.906	
6 ²	97.992			375.209	92.941	-67.379	
7 ²	165.248			14.450	+		
H _p II	63.240	+ 14.450	+ 22.179	389.659	115.120	-68.028	72.4
12 ²	97.374			400.220	269.821	-67.123	
13 ²	145.209			+ 10.965	+ 8.808		
14 ²	43.083	+ 10.965	+ 8.808	411.185	278.629	-67.861	
13 ²	43.083			411.185	278.629	-66.861	
14 ²	248.067			+ 2.975	+ 21.259		
15 ²	91.150	+ 2.975	+ 21.259	414.160	299.888	-66.997	
14 ²	91.150			414.160	299.888	-65.997	
15 ²	186.549						
16 ²	77.699	+ 8.312	+ 22.749	+ 8.312	+ 22.749		
				422.472	322.637	-68.111	
15 ²	77.699			422.472	322.637		
16 ²	201.185			+ 9.361	+ 27.179		
17 ²	78.884	+ 9.361	+ 27.179	431.833	349.861	-67.963	
16 ²	78.884			431.833	349.861	-60.963	
17 ²	175.856			+ 18.312	+ 27.345		
18 ²	54.740	+ 18.312	+ 27.345	450.215	371.206	-62.493	

I	S	Anmerkungen Forts fra side 4
3,035	3,99	$\frac{10^2 - 11^2 = 32,50 \cdot 100,079}{-0,040} = 32,500$
3,74	3,40	$\frac{11^2 - 12^2 = 32,03 \cdot 99,907}{+0,047} = 32,030$
3,15	3,17	$\frac{12^2 - 13^2 = 30,585 \cdot 102,369}{-1,138} = 30,564$
3,20	3,435	$\frac{10^2 - H_p I = 16,16 \cdot 102,026}{-0,514} = 16,152$
2,32	2,91	$\frac{7^2 - H_p II = 26,50 \cdot 102,977}{-1,239} = 26,471$
2,945	3,12	$\frac{13^2 - 14^2 = 14,065 \cdot 99,604}{+0,087} = 14,065$
3,08	3,52	$\frac{14^2 - 15^2 = 21,47 \cdot 98,743}{+0,424} = 21,466$
3,33	4,305	$\frac{15^2 - 16^2 = 24,295 \cdot 94,987}{+1,911} = 24,220$
4,155	4,035	$\frac{16^2 - 17^2 = 28,835 \cdot 94,988}{+2,268} = 28,746$
3,66	3,33	$\frac{17^2 - 18^2 = 28,17 \cdot 100,435}{-0,200} = 28,169$ J. A. 15
		Forts. side 15

Stas	Azimuth	Δx	Δy	X	Y	dybde	Ligg.
34*	102.272			92.5	43		
35*	154.455			353.535	782.931	-77.597	
33y	56.727	+7.229	+8.944	+7.229	+8.944	-0.168	
				360.764	791.875	-77.765	-82.20
35*	56.727			360.764	791.875	-77.765	
33y	83.505			+32.669	+23.978	-0.230	
34y	40.232	+32.669	+23.918	393.433	815.793	77.995	82.20
33y	40.232			393.433	815.793	77.995	
34y	221.366			+10.220	+14.836	-1.515	
35y	61.598	+10.220	+14.836	403.653	830.629	79.510	84.10
34y	61.598			403.653	830.629	79.510	
35y	245.269			-2.973	+27.452	-2.145	
36y	106.867	-2.973	+27.452	400.680	858.081	81.655	86.10
							2 1/2
13*	43.083			411.185	278.629	67.861	
14*	56.602						
14A	299.685	-0.193	-38.905	410.99	2239.724	60.566	
14*	299.685						
14A	204.243						
14B	303.928	+2.241	-36.272	413.233	203.452	58.916	
14A	303.928						
14B	384.540						
R.pI	88.468	+2.816	+15.374	416.049	218.826	218.826	
14B	88.468						
R.pI	195.623						
R.pII	84.091	+8.021	+31.427	424.070	250.235	56.993	
14B	88.468						
I	194.270						
II	82.738	+8.357	+30.063	424.406	248.889		
I	82.738						
II	215.760						
III	98.498	+0.526	+22.289	424.932	271.178		

1 S

Anmerkungen

$$35x - 33y = \frac{11.50 \cdot 99.960}{+0.007} = 11.500$$

$$33y - 34y = \frac{40.49 \cdot 100.440}{-0.28} = 40.489$$

$$34y - 35y = \frac{18.125 \cdot 107.021}{-1.995} = 18.015$$

$$35y - 36y = \frac{27.68 \cdot 104.454}{-1.935} = 27.612$$

3.175

3.33

$$142 - 14A = \frac{39.555 \cdot 88.445}{+7.140} = 38.905$$

321

3.17

$$14A - 14B = \frac{36.38 \cdot 97.041}{+1.690} = 36.340$$

$$14B - \text{Retn. plugg} = \frac{15.63 \cdot 100.200}{-0.049} = 15.630 \quad (191,5)$$

$$BpI - BpII = \frac{32.49 \cdot 96.299}{+1.888} = 32.435$$

$$I - II = \frac{31.27 \cdot 95.835}{+2.044} = 31.203$$

2.07

2.76

$$II - III = \frac{22.41 \cdot 106.455}{-2.268} = 22.295$$

2.76

2.45

2 1/2

1 5

Hameckinger

St.	Azimuth	Δx	Δy	X	y	dybde	L.gg
C	69.487			925	43		
B	222.670			397.030	059.450	-43.620	
3	92.157	+4.051	+32.716	+4.051	+32.716	-2.022	
				401.081	092.166	45.642	
B2	92.157			401.081	92.166	45.642	
3	206.087			+1.001	+36.269	-0.951	
4	98.244	+1.001	+36.269	402.082	128.435	46.593	
3	98.244			402.082	128.435	46.593	
4	209.637			-4.063	+32.651	-0.382	
5	107.881	-4.063	+32.651	398.019	161.086	46.975	
4	107.881			398.019	161.086	46.975	
5	194.809			-1.719	+40.663	-0.419	
6	102.690	-1.719	+40.663	396.300	201.749	47.394	
5	102.690			396.300	201.749	47.394	
6	203.372			-2.851	+29.847	1.913	
7	106.062	-2.851	+29.847	393.449	231.596	49.317	
6	106.062			393.449	231.596	49.317	
7	173.389			+3.979	+11.896	0.370	
8	79.451	+3.979	+11.896	397.428	243.492	49.687	
7	79.451			397.428	243.492	49.687	
8	223.956			-1.163	+26.350	-0.405	
8*	102.807	-1.163	+26.350	396.265	269.842	50.092	54.72
8	102.807			396.265	269.842	50.092	
8*	197.526			-0.137	+26.232	-0.795	
9*	100.333	-0.137	+26.232	396.128	296.074	50.887	55.5
8*	100.333			396.128	296.074	50.887	
9*	201.716			-0.920	+28.568	2.013	
10*	102.049	-0.920	+28.568	395.208	324.642	52.900	57.20
9*	102.049			395.208	324.642	52.900	
10*	198.411			-0.158	+21.822	0.440	
11*	100.460	-0.158	+21.822	395.050	346.464	53.340	58.20

I	S	Anmerkninger
	Bolt 4-3	
31 0 296	3-2 = $\frac{33.02 \cdot 103.631}{-1.882}$ = 32.966	Utgangspunkt er i ve. krysset ved linse II
2.69 2.47	3-4 = $\frac{36.29 \cdot 101.248}{-0.711}$ = 36.283	
2.245 2.24	4-5 = $\frac{32.905 \cdot 100.730}{-0.377}$ = 32.903	
2.185 2.705	5-6 = $\frac{40.71 \cdot 101.469}{-0.939}$ = 40.699	
2.42 2.97	6-7 = $\frac{30.085 \cdot 105.239}{-2.473}$ = 29.983	
2.96 2.39	7-8 = $\frac{12.55 \cdot 101.927}{-0.380}$ = 12.544	
2.25 3.37	8-8* = $\frac{26.42 \cdot 103.676}{-1.525}$ = 26.376	
	8*-9* = $\frac{26.25 \cdot 102.319}{-0.955}$ = 26.232	Før punkt
	9*-10* = $\frac{28.635 \cdot 103.844}{-1.728}$ = 28.583	
	10*-11* = $\frac{21.87 \cdot 104.194}{-1.440}$ = 21.823	

st	Azimuth	Δx	Δy	X	Y	dybde	Ligg
109	100.460			395.050	346.464	53.340	
119	203.188			- 2.259	+ 39.361	0.086	
129	103.648	-2.259	+ 39.361	392.791	385.825	53.426	53.40
119	103.648			392.791	385.825	53.426	
129	201.010			- 2.153	+ 29.372	+ 2.170	
139	104.658	-2.153	+ 29.372	390.638	415.197	51.256	56.4
139							
129	104.658			390.638	415.197	51.256	
139	166.475			+ 10.582	+ 21.716	+ 1.128	
149	71.133	+ 10.582	+ 21.716	401.220	436.913	50.128	55.30
139	+ 71.133			401.220	436.913	50.128	
149	211.923			+ 5.556	+ 20.441	+ 2.332	
159	83.106	+ 5.556	+ 20.441	406.776	457.354	47.796	
149	83.106			406.776	457.354	47.796	
159	210.258			+ 3.073	+ 29.370	+ 2.118	
169	93.364	+ 3.073	+ 29.370	466.849	486.724	45.678	
159	93.364			409.849	486.724	45.678	
169	199.234			+ 2.631	+ 22.524	+ 2.068	
179	92.598	+ 2.631	+ 22.524	412.480	509.248	43.610	
169	92.598			412.480	509.248	43.610	
179	199.227			+ 2.407	+ 22.510	+ 3.009	
189	91.825	+ 2.407	+ 22.510	415.387	531.758	40.601	
159	83.106						
159	93.364						
169	209.476						
179	92.582	+ 3.445	+ 29.432	410.221	486.786		
169	92.582						
179	201.034						
189	93.616	+ 2.261	+ 22.470	412.482	509.256		
179	93.616						
189	199.401						
199	93.017	+ 2.346	+ 30.380	415.828	539.636		

I	S		Anmerkungen
		$\begin{array}{r} 119 - 124 = 39.43.100.850 \\ - 0.526 \end{array}$	Forts fra side 8 39.426
		$\begin{array}{r} 129 - 134 = 29.52.95.641 \\ + 2.020 \end{array}$	29.451
		$\begin{array}{r} 139 - 144 = 24.18.97.241 \\ + 1.048 \end{array}$	24.157
		$\begin{array}{r} 149 - 154 = 21.34.92.278 \\ + 2.582 \end{array}$	21.183
3.465 3.86		$\begin{array}{r} 159 - 164 = 29.58.96.290 \\ + 1.723 \end{array}$	29.530
4.36 3.88		$\begin{array}{r} 169 - 174 = 22.82.92.827 \\ + 2.548 \end{array}$	22.677
3.86 4.19		$\begin{array}{r} 179 - 184 = 22.855.96.821 \\ + 2.679 \end{array}$	22.697
		$\begin{array}{r} 164 - 174 = 29.675.96.603 \\ + 1.583 \end{array}$	29.633
		$\begin{array}{r} 174 - 184 = 22.71.93.258 \\ + 1.272 \\ + 2.401 \end{array}$	30. 22.583
		$\begin{array}{r} 184 - 194 = 30.59.97.351 \\ + 1.272 \end{array}$	30.564 Forts. side 13

Linse II sør

St.	Azimuth	Δx	Δy	X	Y	dybde L. 99
				925	43	
7*	100.569			396,265	269,842	50,092
8*	224.081			- 9,626	+23,605	-1,30
10*	124,650	-9,626	+23,605	386,639	293,447	51,392 55,80
8*	124,650			386,639	293,447	51,392
10*	192,200			- 4,981	+18,379	-2,251
11*	116,850	-4,981	+18,379	381,658	311,826	53,643 58,12
10*	116,850			381,658	311,826	53,643
11*	182,360			+ 0,487	+39,209	-1,843
12*	99,210	+0,487	+39,209	382,145	351,035	55,486 60,00
11*	99,210			382,145	351,035	55,486
12*	201,101			- 0,113	+23,140	+0,446
13*	100,311	-0,113	+23,140	382,032	374,175	55,040 60,90
12*	100,311			382,032	374,175	55,040
13*	207,466	-3895	+31,722	- 3,895	+31,722	+0,293
14*	107,777	-4,864	+40,066	378,137	405,897	54,747 59,30
13*	107,777			378,137	405,897	54,747
14*	199,914			- 4,864	+40,066	-0,257
15*	107,691	-4,864	+40,066	373,273	445,963	55,004 59m
14*	107,691			373,273	445,963	55,004
15*	190,130			+ 0,792	+23,116	-0,725
16*	97,821	+0,792	+23,116	374,065	469,079	55,729 59,80
15*	97,821			374,065	469,079	55,729
16*	190,576			+ 3,257	+17,684	-0,180
17*	88,397	+3,257	+17,684	377,324	486,763	55,909 60,40
15*	97,821			374,065	469,079	55,909
16*	192,149			+ 2,812	+17,702	-0,208
17*	89,970	+2,812	+17,702	376,877	486,781	56,117 60,6
16*	89,970			376,877	486,781	56,117
17*	202,529			+ 3,331	+28,140	-0,334
18*	92,499	+2,812				
		+3,331	+28,140	380,208	514,921	56,451 61,0

1	5		Anmerkninger
		$\begin{array}{r} 8^* - 10^* = 25,50 \cdot 101,549 \\ - 0,620 \\ \hline \end{array} = 25,492$	87* - 8* er
		$\begin{array}{r} 10^* - 11^* = 19,215 \cdot 108,559 \\ - 2,576 \\ \hline \end{array} = 19,042$	korrigeret med
		$\begin{array}{r} 11^* - 12^* = 39,29 \cdot 104,001 \\ - 2,468 \\ \hline \end{array} = 39,212$	+0,2679 i forhold til
		$\begin{array}{r} 12^* - 13^* = 23,14 \cdot 99,790 \\ + 0,076 \\ \hline \end{array} = 23,14$	det gamle koord. net.
		$\begin{array}{r} 13^* - 14^* = 31,96 \cdot 99,814 \\ + 0,093 \\ \hline \end{array} = 31,960$	
		$\begin{array}{r} 14^* - 15^* = 40,36 \cdot 99,893 \\ + 0,068 \\ \hline \end{array} = 40,360$	
		$\begin{array}{r} 15^* - 16^* = 23,15 \cdot 102,655 \\ - 0,965 \\ \hline \end{array} = 23,130$	
		$\begin{array}{r} 16^* - 17^* = 18,00 \cdot 102,828 \\ - 0,800 \\ \hline \end{array} = 17,982$	
2,67	3,23	$\begin{array}{r} 16^* - 17^* = 17,94 \cdot 102,726 \\ - 0,768 \\ \hline \end{array} = 17,924$	
2,98	3,38	$\begin{array}{r} 17^* - 18^* = 28,345 \cdot 101,648 \\ - 0,734 \\ \hline \end{array} = 28,336$	
			Fortz. side 11

St.	Azimuth	Δx	Δy	X	Y	dybde	L.gg
17*	92.499			925 380.208	43 514.921	56.451	
18*	196.543			+ 5.304	+ 30.507	- 0.947	
19*	89.042	+ 5.304	+ 30.507	385.512	545.428	- 57.398	62.0
17*	92.499			380.208	514.921	57.398	
18*	158.260			+ 16.470	+ 16.868	+ 1.705	
2b	50.759	+ 16.470	+ 16.868	396.678	531.789	55.693	
18*	89.042			385.512	545.428	- 57.398	
19*	209.653			+ 0.685	+ 33.420	+ 0.919	
20*	98.695	+ 0.685	+ 33.420	386.197	578.848	- 56.479	60.00
18*	50.759			396.678	531.789	- 55.693	
2b	245.886			+ 1.859	+ 35.240		
3b	96.645	+ 1.859	+ 35.240	398.537	567.029	54.572	
19*	98.695			386.197	578.848	- 56.479	
20*	202.485			- 0.475	+ 25.643		
21*	101.180	- 0.475	+ 25.643	385.722	604.491	- 57.443	
20*	101.180			385.722	604.491	- 57.443	
21*	190.293			+ 1.269	+ 20.017		
22*	91.473	+ 2.697	+ 20.017	388.419	624.508	- 58.136	
2b	96.645			398.537	567.029	- 54.572	
3b	210.855			- 2.800	+ 23.660		
4b	107.500	- 2.800	+ 23.660	395.737	590.689	- 55.321	
3b	107.500			395.737	590.689	- 55.321	
4b	184.796			+ 4.227	+ 34.761		
5b	92.296	+ 4.227	+ 34.761	399.964	625.450	- 55.426	
20*	101.180			385.722	604.491	57.443	
21*	193.752			+ 1.957	+ 24.527		
22*	94.932	+ 1.957	+ 24.527	387.679	629.018	58.689	
21*	94.932			387.679	629.018	58.689	
22*	224.543			- 1.045	+ 22.307		
23*	119.475	- 2.045	+ 22.307	380.634	651.325	58.863	

I	S		Forts. fra s 10
3.07	3.60	$\begin{array}{r} 18^* - 19^* 31.00 \cdot 103.035 \\ - 1.477 \\ \hline \end{array} = 30.965$	
3.07	2.77	$\begin{array}{r} 18^* - 26 - 23.66 \cdot 94.600 \\ + 2.005 \\ \hline \end{array} = 23.575$	Ort nr 3
3.30	3.475	$\begin{array}{r} 19^* - 20^* = 33.435 \cdot 98.584 \\ + 0.744 \\ \hline \end{array} = 33.427$	
2.785	3.70	$\begin{array}{r} 26 - 36 = 35.29 \cdot 99.629 \\ + 0.206 \\ \hline \end{array} = 35.289$	Ort nr 3
3.22	3.35	$\begin{array}{r} 20^* - 21^* = 25.67 \cdot 102.713 \\ - 1.094 \\ \hline \end{array} = 25.647$	
3.035	3.18	$\begin{array}{r} 21^* - 22^* = 20.15 \cdot 102.436 \\ - 0.838 \\ \hline \end{array} = 20.198$	
3.71	2.955	$\begin{array}{r} 36 - 46 = 23.825 \cdot 99.985 \\ + 0.006 \\ \hline \end{array} = 23.825$	Ort nr 3
2.62	3.285	$\begin{array}{r} 46 - 56 = 35.017 \cdot 101.362 \\ - 0.760 \\ \hline \end{array} = 35.017$	Ort nr 3
3.03	2.65	$\begin{array}{r} 21^* - 22^* = 24.62 \cdot 102.240 \\ - 0.866 \\ \hline \end{array} = 24.605$	
2.34	3.80	$\begin{array}{r} 22^* - 23^* = 23.45 \cdot 104.440 \\ - 1.634 \\ \hline \end{array} = 23.393$	Forts. s. 14

12

Linse II ort nr 2

St.	Azimuth	Δx	Δy	X	Y	dybde	L.gg
13y	71.133			401.220	436.913	-50.128	
14y	245.717			-6.782	+25.022		
1a	116.850	-6.782	+25.022	-6.78 394.438	461.935	-50.678	
14y	116.850			394.438	461.935	50.678	
1a	175.391			+3.494	+28.527		
2a	92.241	+3.494	+28.527	397.932	490.462	50.859	
1a	92.241			397.932	490.462	50.859	
2a	194.670			4.033	+19.338		
3a	86.911	+4.033	+19.338	401.965	509.800	50.630	
2a	86.911			401.965	509.800	50.630	
3a	199.810			+28.135			
4a	86.721	+8.072	+28.135	410.037	537.935	50.305	
				38.135			
2a	86.911			401.965	509.800	50.630	
3a	201.513			+8.252	+44.878		
4a	88.424	+8.252	+44.878	410.217	554.678	50.382	
3a	88.424			410.217	554.678	50.382	
4a	207.239			+1.412	+14.836		
5a	95.663	+1.012	+14.836	411.229	569.514	50.496	
	424					50.382	
3a	88.2			410.217	554.678	50.496	
4a	207.239			+1.012	+14.836		
5a	95.663	+1.012	+14.836	411.229	569.514	50.496	
4a	95.663			411.229	569.514	50.496	
5a	206.201			-0.740	+25.269		
6a	101.864	-0.740	+25.269	410.489	594.783	50.158	
5a	101.864			410.489	594.783	50.158	
6a	202.046			-1.541	+25.053		
7a	103.910	-1.541	+25.053	408.948	619.836	50.380	

I	S	Anmerkninger
		$\frac{149 \cdot 1a = 2593 \cdot 101,226}{-0,499} = 25,925$
		$\frac{1a - 2a = 28,74 \cdot 100,025}{-0,011} = 28,740$
2,56	329	$\frac{2a - 3a = 1976 \cdot 101,614}{-0,501} = 19,754$
3,04	350	$\frac{3a - 4a = 38,95 \cdot 100,124}{-0,135} = 38,980$
3,06	332	$\frac{3a - 4a = 45,64 \cdot 100,017}{-0,012} = 45,640$
2,91	270	$\frac{4a - 5a = 14,87 \cdot 99,587}{+0,096} = 14,870$
		$\frac{4a - 5a \quad 14,87 \cdot 99,587}{+0,096} = 14,870$
2,40	264	$\frac{5a - 6a = 25,28 \cdot 99,754}{+0,098} = 25,280$
2,48	326	$\frac{6a - 7a = 25,12 \cdot 102,540}{-1,002} = 25,100$
		Forts. ort nr 2 side 14

ST	AZIMUTH	Δx	Δy	X	Y	DYBOE	LIGG
14y	83.106			406.776	457.354		
15y	209.476			+ 3.445	+ 29.432	-47.796	
16y	92.582	+ 3.445	+ 29.432	410.221	486.786	45.588	
15y	92.582			410.221	486.786	45.588	
16y	201.034			+ 2.261	+ 22.470		
17y	93.616	+ 2.261	+ 22.470	412.482	509.256	42.677	
16y	93.616			412.482	509.256	42.677	
17y	199.401			+ 3.346	30.380		
+18y	93.017	+ 3.346	+ 30.380	415.828	539.636	42.25	
17y	93.012			415.828	539.636	42.250	
18y	195.562			+ 5.514	+ 30.416		
+19y	88.584	+ 5.514	+ 30.416	421.342	570.052	41.330	
18y	88.584			+ 3.354	570.052	41.330	
19y	206.071			421.342	+ 39.853		
20y	94.655	+ 3.354	+ 39.853	424.696	609.905	39.861	44.66
19y	94.655			424.696	609.905		
20y	203.195			+ 0.960	+ 28.401		
21y	97.850	+ 0.960	+ 28.401	425.656	638.306	39.468	44.4
20y	97.850			425.656	638.306	39.468	
21y	158.066			+ 8.218	+ 9.907		
22y	55.916	+ 8.218	+ 9.907	433.874	648.213	39.096	43.6
21y	55.916			433.874	648.213		
22y	247.367			+ 17.992	- 0.929		
23y	103.283	+ 17.992	- 0.929	451.866	647.284	-38.639	
21y	55.916			433.874	648.213		
22y	247.367			- 0.929	+ 17.992		
23y	103.283	- 0.929	+ 17.992	432.945	666.205	-38.639	42.8
20y	97.850			425.656	638.306	39.468	
21y	222.140			- 6.987	22.516		
1d	119.990	- 6.987	+ 22.516	418.669	660.822	41.234	46.2

Nr 1

13

I	S		Anmerkninger
365	3,99	$\frac{159-169:29.675 \cdot 96.603}{+1.583} = 29.633$	Forts. fra s 9
390	4,41	$\frac{169-179:22.71 \cdot 93.258}{+2.401} = 22.583$	
1005	3,16	$\frac{179-189:30.59 \cdot 97.351}{+1.272} = 30.564$	
330	2,785	$\frac{189-199:30.945 \cdot 97.047}{+1.435} = 30.912$	
290	3,95	$\frac{199-209:40.005 \cdot 98.537}{+0.919} = 39.994$	
321	2,46	$\frac{209-219:28.44 \cdot 97.441}{+1.143} = 28.417$	
335	3,25	$\frac{219-229:12.88 \cdot 97.741}{+0.457} = 12.872$	
298	2,735	$\frac{229-239:18.13 \cdot 97.519}{+0.702} = 18.016$	
298	2,735	$\frac{229-239:18.03 \cdot 97.519}{+0.702} = 18.016$	
323	3,73	$\frac{229-1d:22.735 \cdot 106.355}{-2.266} = \frac{22.622}{21.815}$	Forts side 21

SL.	AZIMUTH	Δx	Δy	X	Y	DBDE	L.99
20*	101.180			385.722	604.491	-57.443	
21*	198.305			+ 0.172	+ 21.216		
22*	99.485	+0.172	+21.216	385.894	625.707	-58.347	63.7
21*	99.485			385.894	625.707	-58.347	
22*	214.645			- 7.425	+ 32.901		
23*	214.130	-7.425	+32.901	378.469	658.608	-61.751	66.3
21*	99.485			385.894	625.707	-58.347	
22*	134.968			+11.198	+6.730		
Hp	34.453	+11.198	+6.730	397.092	632.437		
22*	34.453			397.092	632.437		
Hp	278.986			- 3.840	+17.920		
4b	113.439	3.840	+17.920	393.252	650.357		
Hp	113.439			393.252	650.357	-58.347	
4b	115.120			+10.123	+4.873		
8a	28.559	+10.123	+4.873	403.375	655.230		
21*	99.485			385.894	625.707	-58.347	
22*	129.815			+10.915	+5.411		
Hp	29.300	+10.915	+5.411	396.809	631.118	-60.734	
22*	29.300			396.809	631.118	-60.734	
Hp	282.357			- 3.561	+19.233		
4b	111.656	-3.561	+19.233	393.248	650.351	57.909	62.4
Hp	111.656			393.248	650.351	-57.909	
4b	197.565			- 5.163	+35.397		
5b	109.221	-5.163	+35.397	388.085	685.748	-58.112	62.9
5b	309.221			393.248	650.351	-57.909	
4b	319.369			+10.071	+4.853		
8a	28.590	+10.071	+4.853	403.319	655.204	-56.940	62.0
4b	28.590			403.319	655.204	-56.940	
8a	267.760			+ 1.514	+26.372		
9a	96.350	+1.514	+26.372	404.833	681.576	-57.342	
8a	96.350			404.833	681.576	-57.342	
9a	216.893			+ 6.159	+29.177		
10a	113.243	-6.159	+29.177	398.674	710.753	-57.014	

I	S'		Anmerkninger
3.12	3.79	$\frac{21^* - 22^* = 21.275 \cdot 104.713}{-1.574} = 21.217$	Forts fra s 11.
3.73	1.79	$\frac{22^* - 23^* = 33.76 \cdot 102.761}{-1.464} = 33.728$	4b, 8a må kontrollmåles
3.70	0.0	$\frac{22^* - Hp = 13.065 \cdot 99.719}{+0.060} = 13.065$ Hp : ligg	
1.35		$\frac{Hp - 4b = 18.33 \cdot 101.149}{-0.331} = 18.327$ Ort nr 3	
2.78	3.95	$\frac{4b - 8a = 11.183 \cdot 101.234}{-0.217} = 11.183$ Ort nr 2	
3.80	-	$\frac{22^* - Hp = 12.265 \cdot 92.650}{+1.413} = 12.183$	
-	2.87	$\frac{Hp - 4b = 19.56 \cdot 100.145}{-0.045} = 19.560$	Hp = Hjelpepunkt : ligg
2.75	3.69	$\frac{4b - 5b = 35.79 \cdot 102.034}{-1.143} = 35.772$	
2.76	3.55	$\frac{4b - 8a = 11.18 \cdot 98.980}{+0.179} = 11.179$	Ligg
3.50	3.20	$\frac{8a - 9a = 26.415 \cdot 100.247}{-0.102} = 26.415$ 11.179	
3.09	3.55	$\frac{9a - 10a = 29.82 \cdot 100.282}{-0.132} = 29.82$	
		Forts. side 17	

15 ST	AZIMUTH	Δx	Δy	X	Y	H
17 ²	54.740			450.215	371.206	-61.493
18 ²	203.264			+76.300	+21.017	
19 ²	58.004	+16.300	+21.017	466.515	392.223	-60.276
11 ²	298.974			401.559	174.910	-66.627
10 ²	79.036			-12.382	+4.456	
Ms	178.010	-12.382	+4.456	389.177	179.366	71.818
10 ²	178.010			389.177	179.366	
Ms	146.190			-9.186	+22.990	
1	124.200	-10.146	+25.394	379.991	202.356	72.432
		-9.186	+22.990		204.760	
Ms	124.200			379.991	202.356	
1	173.985			+0.706	+24.747	
2	98.185	+0.706	+24.747	380.697	227.103	
				379.737	229.507	75.152
9 ²	81.415			401.559	174.910	
10 ²	309.316			-23.467	+3.441	
Hp	190.731	-23.467	+3.441	378.092	178.351	-73.599
10 ²	190.731			378.092	182.807	
Hp	106.971			+0.954	+26.416	
1	97.702	+0.954	+26.416	379.046	209.223	-72.442
					204.767	
HP	97.702			379.046	209.223	
1	200.497			+0.700	+24.760	
2	98.199	+0.700	+24.750	379.746	229.517	-74.182
					233.973	
1	98.199			379.746	233.973	
2	171.269			+12.965	24.427	
3	69.468	+12.965	+24.927	392.711	254.444	-78.630
					258.900	
2	69.468			392.711	254.444	
3	176.543			+6.635	+5.854	
4	46.011	+6.635	+5.854	399.346	260.298	-78.504

I	S		Anmerkninger
3.02	3.415	$\begin{array}{r} 182 - 182 \cdot 86.47 \cdot 98.033 \\ \hline 26.597 \\ - 0.822 \end{array}$	Forts fra side 5
303	—	$\begin{array}{r} 102 \cdot Ms - 13.21 \cdot 105.610 \\ \hline 13.159 \\ - 1.161 \end{array}$	
—	3.05	$\begin{array}{r} Ms - 1 \cdot 27.69 \cdot 108.488 \\ \hline 27.346 \\ - 3.664 \end{array}$	Ms. ikke fastmarke Ligg - 74.6
2.58	3.04	$\begin{array}{r} 1 - 2 \cdot 24.98 \cdot 108.132 \\ \hline 24.757 \\ - 3.180 \end{array}$	Ligg - 78.7
2.99	—	$\begin{array}{r} 102 - Hp : 2405 \cdot 110.590 \\ \hline 23.718 \\ - 3.982 \end{array}$	Hp ikke fastmarke
—	3.64	$\begin{array}{r} Hp - 1 = 26.475 \cdot 103.568 \\ \hline 26.433 \\ - 1.483 \end{array}$	
3.46	2.83	$\begin{array}{r} 1 - 2 : 2485 \cdot 105.413 \\ \hline 24.760 \\ - 2.110 \end{array}$	
2.795	2.69	$\begin{array}{r} 2 \cdot 3 \cdot 28.295 \cdot 107.529 \\ \hline 28.097 \\ - 3.343 \end{array}$	Forts. side 27
2.505	2.03	$\begin{array}{r} 3 - 4 \cdot 8.86 \cdot 102.871 \\ \hline 8.851 \\ - 0.399 \end{array}$	Dårlige måleforh. for nr 4 Ma kontrolleres

ST	Azimuth	Δx	Δy	X	Y	H
62	296.171			372.707	44. 035.095	-64.649
52	238.205			+11.727		
Ms	334.376	+11.727	-19.565	384.434	015.530	66.921
52	334.376			384.434	015.530	
Ms	290.547			+8.591	+3.546	
7W	24.923	+8.591	+3.546	393.025	019.076	62.847
Ms	24.923			393.025	019.076	
1W	272.071			+1.610	+34.070	
10	96.994	+1.610	+34.070	394.635	053.146	-56.740
Ms	24.923			393.025	019.076	
1W	88.741			+6.451	-29.591	
2W	385.735 813.664	+6.451	-29.591	399.476	43. 989.485	-57.457
112	102					
Ms.						
1W	96.994			394.635	44. 053.146	
10	118.829			+9.022	+2.290	
1N	15.823	+9.022	+2.290	403.657	055.436	-56.874
10	15.823			403.657	055.436	
1N	98.599			+7.149	-31.015	
2N	314.422	+7.149	-31.015	410.806	024.421	54.149
1N	215.823			394.635	053.146	
10	108.735			-9.405	+23.158	
20	124.558	-9.405	+23.158	385.230	076.304	-58.635
10	124.558			385.230	076.304	
20	111.230			+12.355	+7.783	
30	35.788	+12.355	+7.783	397.585	084.087	-58.722

I S

Bemerkninger

$$2.305 \quad - \quad 52 - Ms = 22.81 \cdot 99.907 \\ + 0.033 = 22.810$$

Ms = meloms.kt
ikke fast.punkt

$$- \quad 2.60 \quad Ms - 1W = 9.41 \cdot 89.968 \\ + 1.474 = 9.294$$

Ligg 66.95

$$2.52 \quad 4.23 \quad 1W - Ms - 10 = 34.39 \cdot 91.838 \\ + 4.397 = 34.108$$

Ligg 62.35

$$2.52 \quad 2.28 \quad 1W - 2W = 30.805 \cdot 88.300 \\ + 5.630 = 30.286$$

Ligg 61.85

$$- \quad 102 - Ms = 13.21 \cdot 105.600 \\ - 1.161 = 13.159$$

$$3.925 \quad 3.25 \quad 10 - 1N = 9.325 \cdot 96.119 \\ + 0.568 = 9.308$$

Ligg 61.3

$$1N - 2N = 31.94 \cdot 94.677 \\ + 2.668 = 31.828$$

Ligg - 58.5

$$10 - 20 = 25.03 \cdot 103.371 \\ - 1.325 = 24.995$$

Ligg - 63.4

$$20 - 30 = 14.61 \cdot 97.851 \\ + 0.493 = 14.602$$

Ligg - 63.7

Stasi	Azimuth	Δx	Δy	X	Y	<u>Heng</u> I S		<u>Heng</u> Ligg
22*	114,130			378,469	658,608			-61,751
23*	187,809			-1,161	+38,090			
24*	101,939	-1,161	+38,090	377,308	696,698	3,005	3,385	-61,768
22*	114,130			378,469	658,608			-61,751
23*	222,639			-11,564	+17,744			
1 ^c	136,769	-11,564	+17,744	366,905	676,352	3,005	2,96	-62,451
23*	136,769			366,905	676,352			-62,451
1 ^c	163,356			-0,064	+32,528			
2 ^c	100,125	-0,064	+32,528	366,841	708,880	2,63	3,785	-62,199
1 ^c	100,125			366,841	708,880			
2 ^c	199,825			+0,026	+32,618			
3 ^c	99,950	+0,026	+32,618	366,867	741,498	3,35	2,795	-63,622
4b	109,221			388,085	685,748			-58,112
5b	187,465			+1,883	+36,134			
Hp	96,686	+1,883	+36,134	389,968	721,882	3,23	-	-63,188
5b	96,686			389,968	721,882			
Hp	208,044			-1,826	+24,526			
6b	104,730	-1,826	+24,526	388,142	746,408	-	3,33	-58,968
8a	96,350			409,833	681,576			-57,342
9a	215,706			-6,153	+32,104			
Hp	112,056	-6,153	+32,104	398,680	713,680	3,10	-	-61,322
9a	112,056			398,680	713,680			
Hp	187,362			+0,227	+24,884			
10a	99,418	+0,227	+24,884	398,907	738,564	-	3,21	-57,245
Hp	99,418			398,907	738,564			
10a	192,163			+2,525	+18,841			
11a	91,581	+2,525	+18,841	401,432	757,405	2,93	3,10	-56,838

		Ligg	Bemerkninger
$\begin{array}{r} 23^* - 24^* = 38.11 \cdot 100.664 \\ - 0.397 \\ \hline \end{array}$	$= 38.108$	66.4	Forts fra s. 14 x drag forts side 19
$\begin{array}{r} 23^* - 1^c = 21.19 \cdot 101.968 \\ - 0.655 \\ \hline \end{array}$	21.180		Ort nr 5 Heng-66.6
$\begin{array}{r} 1^c - 2^c = \cancel{101} 32.54 \cdot 101.709 \\ - 0.873 \\ \hline \end{array}$	32.528	67.2	Ort nr 5
$\begin{array}{r} 2^c - 3^c = 32.63 \cdot 101.694 \\ - 0.868 \\ \hline \end{array}$	32.618	68.0	Ort nr 5
$\begin{array}{r} 5b - Hp = 36.23 \cdot 103.246 \\ - 1.846 \\ \hline \end{array}$	36.183		Hp = hjælpepunkt i Ligg. 19
$\begin{array}{r} Hp - 6b = 24.61 \cdot 97.698 \\ + 0.890 \\ \hline \end{array}$	24.594	63.7	Ort nr 3
$\begin{array}{r} 9a - Hp = 32.70 \cdot 101.713 \\ - 0.88 \\ \hline \end{array}$	32.688		Ort nr 2
$\begin{array}{r} Hp - 10a = 24.90 \cdot 97.783 \\ + 0.867 \\ \hline \end{array}$	24.885	61.8	Hp = hjælpepunkt i Ligg
$\begin{array}{r} 10a - 11a = 19.01 \cdot 99.205 \\ + 0.237 \\ \hline \end{array}$	19.009		Forts. side 18

stasi	Azimuth	Δx	Δy	x	y	I	S
4b	109.221			388.085	685.748		
5b	188.032			+ 1.565	+ 36.252	3.19	—
Hp	97.253	+ 1.565	+ 36.252	389.650	722.000		
5b	97.253			389.650	722.000		
Hp	206.661			- 1.502	+ 24.395	—	3.175
6b	103.914	- 1.502	+ 24.395	388.148	746.395		
Hp	103.914			388.148	746.395		
6b	195.703			+ 0.220	+ 36.520	3.15	3.56
7b	99.617	+ 0.220	+ 36.520	388.368	782.915		
2c	99.950			366.867	741.498		
3c	200.076						
4c	100.026	- 0.013	+ 32.590	366.854	774.088	2.67	3.44
7b	299.617			388.148	746.395		
6b	382.652		0	+ 9.136	+ 31.949		
11a	82.269	+ 9.136	31.949	397.284	778.344	3.17	2.81
3c	100.026			366.854	774.088		
4c	200.119						
5c	100.145	- 0.072	+ 33.902	366.782	807.990	3.35	3.48
4c	100.145						
5c	201.351						
6c	101.496	- 0.442	+ 19.193	366.340	827.183	3.46	3.175
5c	101.496			366.340	827.183		
6c	182.081			+ 6.451	+ 24.450		
7c	83.577	+ 6.451	+ 24.450	372.791	851.633	2.965	2.61

Heng	Ligg		Bemerkninger
-58,112		$\frac{5b - Hp = 36.33 \cdot 103.146}{-1.795} = 36.286$	Hp. <u>ikke</u> fastm
63,097			
58,948		$\frac{Hp - 6b = 24.46 \cdot 97.463}{+0.974} = 24.441$	
59,705			
-63,622		$\frac{6b - 7b = 36.54 \cdot 102.033}{-1.167} = 36.521$	
62,835	67.80	$\frac{3^c - 4^c = 32.59 \cdot 99.968}{+0.017} = 32.590$	4 ^c innmålt under rnnskelige forhold bør kontrolleres
59,169		$\frac{6b - Nr = \overset{0}{33.23} \cdot 99.733}{+0.139} = 33.230$	
-61,215	66.1	$\frac{4^c - 5^c = 33.935 \cdot 97.204}{+1.490} = 33.902$	
-60,860	-65,4	$\frac{5^c - 6^c = 19.21 \cdot 97.880}{+0.640} = 19.199$	
-60,856		$\frac{6^c - 7^c = 25.29 \cdot 99.097}{+0.359} = 25.287$	Forts side 20

Stasj	Azimuth	Δx	Δy	X	Y	I	S
23*	101.939			377.308	696.698		
24*	197.893			+ 0.092	+ 34.900	3.11	3.44
25*	99.832	+ 0.092	+ 34.900	377.400	731.598		
24*	99.832			377.400	731.598		
25*	200.493			- 0.151	+ 29.585	3.20	3.56
26*	100.325	- 0.151	+ 29.585	377.249	761.183		
25*	100.325			377.249	761.183		
26*	199.486			+ 0.076	+ 25.448	3.446	3.78
		+ 0.076					
27*	99.811	+ 0.076	+ 25.448	377.325	786.631		
26*	99.811			377.325	786.631		
27*	200.080			+ 0.070	+ 40.937	3.49	3.97
28*	99.891	+ 0.070	+ 40.937	377.395	827.568		
27*	99.891			377.395	827.568		
28*	183.845			+ 5.684	+ 21.762	3.52	3.52
29*	83.736	+ 5.684	+ 21.762	383.079	849.330		
28*	83.736			383.079	849.330		
29*	199.360			+ 5.645	+ 20.759	3.44	3.79
30*	83.096	+ 5.645	+ 20.759	388.724	870.089		

Heng	Ligg		Bemerkninger
-62.24	67.2	$\begin{array}{r} 24^* - 25^* = 34.40 \cdot 101.530 \\ - 0.812 \\ \hline \end{array} = 34.390$	Forts. fra side 17 25* og 26* er inn- målt under svært ugunstige forhold.
-62.012	-67.1	$\begin{array}{r} 25^* - 26^* = 29.585 \cdot 100.284 \\ - 0.132 \\ \hline \end{array} = 29.585$	<u>må ettermåles</u>
60.894		$\begin{array}{r} 26^* - 27^* = 25.46 \cdot 98.043 \\ + 0.783 \\ \hline \end{array} = 25.448$	
59.043	-64.2	$\begin{array}{r} 27^* - 28^* = 40.96 \cdot 97.869 \\ + 1.371 \\ \hline \end{array} = 40.937$	
-58.462		$\begin{array}{r} 28^* - 29^* = 22.50 \cdot 98.356 \\ + 0.581 \\ \hline \end{array} = 22.492$	
57.562		$\begin{array}{r} 29^* - 30^* = 21.52 \cdot 98.373 \\ + 0.550 \\ \hline \end{array} = 21.513$	Dårlike måleforh. 25* til 30* kontrollert. Korreksjon på retningsvinkler og koordinater side 22

STASO.	Azimuth	Δx	Δy	x	y	Heng	Ligg
5 ^c	101.496			366.340	827.183		
6 ^c	182.074			+ 6.449	+ 24.431		
7 ^c	83.570	+6.449	+24.431	372.789	851.614	-60.856	64.9
6 ^c	83.570			372.789	851.614		
7 ^c	214.217			+ 1.401	+ 40.288		
8 ^c	97.787	+1.401	+40.288	374.190	891.902	-61.329	65.9
7 ^c	97.787			374.190	891.902		
8 ^c	199.999			+ 1.060	+ 30.474		
9 ^c	97.786	+1.060	+30.474	375.250	922.376	-60.791	65.6
8 ^c	97.786			375.250	922.376		
9 ^c	203.227			- 0.452	+ 28.401		
10 ^c	101.013	-0.452	+ 28.401	374.798	950.777	-60.527	65.33
9 ^c	101.013			374.798	950.777		
10 ^c	176.281			+ 14.624	+ 39.249		
HpI	77.294	+14.624	+39.249	389.422	990.026	61.008 -61.008	
10 ^c	77.294			389.422	990.026		
HpI	186.242			+ 4.755	+ 7.373		
HpII	63.536	+4.755	+7.373	394.177	997.399	-61.486	
HpI	63.536			394.177	997.399		
HpII	271.411			+ 4.603	- 7.526		
2W	334.947	+4.603	-7.526	398.780	989.873	-56.656	

I	S		Bemerkninger
		$\begin{array}{r} 6^c - 7^c = 25,27 \cdot 99,303 \\ + 0,277 \end{array} = 25,268$	Forts fra s. 18
2.49	3.22	$\begin{array}{r} 7^c - 8^c = 40,33 \cdot 101,899 \\ - 1,203 \end{array}$	40,312
3.14	3.225	$\begin{array}{r} 8^c - 9^c = 30,495 \cdot 99,055 \\ + 0,453 \end{array}$	30,492
3.22	3.495	$\begin{array}{r} 9^c - 10^c = 28,405 \cdot 100,025 \\ - 0,0115 \end{array}$	28,405 Fortsatt s 28
3.31		$\begin{array}{r} 10^c - Hp I = 41,98 \cdot 100,707 \\ + 2,829 \end{array}$	41,885 Blindstasjon
		$\begin{array}{r} Hp I - Hp II = 8,785 \cdot 103,321 \\ - 0,458 \end{array}$	8,773 Blindstasjon
3.08		$\begin{array}{r} Hp II - 2W = 8,819 \cdot 82,663 \\ + 1,731 \end{array}$	8,822

STATION	Azimuth	Δx	Δy	x	y	Heng	Ligg
21y 1d	119.990 179.685			418.669 + 0.188	660.822 + 36.730	-41.234	
2d	99.675	+0.188	+36.730	418.857	697.552	-43.373	48.27
22y 23y	103.283 198.366			432.945 - 0.861	666.205 + 33.227	-38.639	
24y 1d 2d	101.649 99.675 235.018	-0.861	+33.227	432.084 418.857 - 7.596	699.432 697.552 + 12.531	-39.391	44.7
3d	134.693	-7.596	+12.531	411.261	710.083	-44.612	48.5
2d 3d	134.693 134.408			411.261 + 10.337	710.083 + 19.559		
25y 26y 3d	69.101 269.101 41.159	+10.337	+19.599	421.598 411.261 - 3.742	729.642 710.083 + 23.019	-44.218	48.9
4d	110.260	-3.742	+22.019	407.519	733.102	-45.259	49.55
3d 25y	69.101 223.936			421.598 + 3.417	729.642		
26y	93.037	+3.417	+31.114	425.015	760.756	-43.153	48.2
2d 3d	134.693 174.074			411.261	710.083 + 22.898		
4d	108.767	-3.173	+22.898	408.088	732.981	-45.305	49.55
25y 26y	93.037 284.189			425.015 - 15.473	760.756 + 5.784		
27y	177.226	-15.473	+5.784	409.542	766.540	46.158	

I	S		Bemerkninger
3.41	3.54	$\frac{1d - 2d = 36,80 \cdot 103,927}{- 2,269} = 36,730$	Forts fra s. 13
2.67	3.78	$\frac{234 - 244 = 33,29 \cdot 103,564}{- 1,862} = 33,238$	
3.36	3.25	$\frac{2d - 3d = 14,71 \cdot 105,591}{- 1,129} = 14,653$	
2.96	3.03	$\frac{3d - 259 = 22,16 \cdot 99,069}{+ 0,324} = 22,158$	
2.88	3.495	$\frac{3d - 4d = 23,355 \cdot 103,443}{- 1,262} = 23,321$	
3.02	3.58	$\frac{254 - 264 = 31,305 \cdot 98,972}{+ 0,505} = 31,301$	
2.80	3.52	$\frac{3d - 4d = 23,16 \cdot 103,886}{- 1,413} = 23,117$	
3.45	2.03	$\frac{264 - 274 = 16,595 \cdot 106,091}{- 1,585} = 16,519$	

Stag	Azimuth	Δx	Δy	x	y	Heng	ligg
23*	101,939			377,380	696,698		
24*	198,004			+ 0,031	+34,390		
25*	99,943	+0,031	+34,390	377,411	731,088	-62,240	-67.2
24*	99,943			377,411	731,088		
25*	200,455			- 0,185	+29,584		
26*	100,398	-0,185	+29,584	377,226	760,672	-62,012	-67.1
25*	100,398			377,226	760,672		
26*	199,486			+ 0,046	+25,448		
27*	99,884	+0,046	+25,448	377,272	786,120	-60,894	65,9
26*	99,884			377,272	786,120		
27*	200,080			+ 0,023	+40,937		
28*	99,964	+0,023	+40,937	377,295	827,057	-59,043	64.1
27*	99,964			377,295	827,057		
28*	183,845			+ 5,659	+21,768		
29*	83,809	+5,659	+21,768	382,954	848,825	-58,462	63.5
28*	83,809			382,954	848,825		
29*	199,358			+ 5,622	+20,765		
30*	83,167	+5,622	+20,765	388,576	869,590	-57,562	63.3
29*	83,167			388,576	869,590		
30*	214,206			+ 0,936	+28,003		
31*	97,873	+0,936	+28,003	389,512	897,593	60,507	65.10
29*	83,167			388,576	869,590		
30*	214,703			+ 0,938	+28,021		
31*	97,870	+0,938	+28,021	389,514	897,611	60,488	65.1

I	S		Anmerkungen
3.11	3.44	$\frac{24^* - 25^* = 34,40 \cdot 101,530}{-0,812} = 34,390$	
3.20	3.56	$\frac{25^* - 26^* = 29,585 \cdot 100,284}{-0,132} = 29,585$	
3.445	3.78	$\frac{26^* - 27^* = 25,46 \cdot 98,043}{+0,783} = 25,448$	
3.49	3.97	$\frac{27^* - 28^* = 40,96 \cdot 97,869}{+1,371} = 40,937$	
3.52	3.52	$\frac{28^* - 29^* = 22,50 \cdot 98,356}{+0,581} = 22,492$	
3.44	3.79	$\frac{29^* - 30^* = 21,52 \cdot 98,373}{+0,550} = 21,513$	
3.96	3.085	$\frac{30^* - 31^* = 28,095 \cdot 104,696}{-2,070} = 28,019$	
1.075	3.035	$\frac{30^* - 31^* = 28,10 \cdot 104,277}{-1,886} = 28,037$	

Forts. s. 23

23 Forts In. & 22									
St	Azimuth	Δx	Δy	x	y	H	I	S	
30*	97.870			389.514	897.611				
31*	209.682			-2.707	+22.709				
32*	107.552	-2.707	+22.709	386.807	920.320	-60.271	2.795	3.49	
31*	107.552			386.807	920.320				
32*	184.808			+2.770	+22.968		3.185	3.47	
33*	92.360	+2.770	+22.968	389.577	943.288	-59.474			
30*	97.870			389.514	897.611				
31*	142.142			+10.633	+7.728		2.875		
11a	40.012	+10.633	+7.728	400.147	905.339	-60.587		2.84	
31*	40.012			400.147	905.339				
11a	256.327			+1.605	+27.884		2.625		
12a	96.339	+1.605	27.884	401.752	933.223	-59.650		3.04	
32*	92.360			389.577	943.288				
33*	193.113								
HpA	85.473	+7.060	+30.402	396.637	973.690	58.867	3.265	-	
33*	85.473								
HpA	206.332								
2W	91.805	+2.096	+16.190	398.733	989.880				
33*	85.473			396.637	973.690				
HpA	11.333								
HpB	296.806	-0.783	-15.600	395.854	958.09	-65.651	-	-	
29*	283.809			377.295	827.057	59.043			
28*	374.811								
28I	58.620	+4.378	+5.760	381.673	832.817	52.933	3.605	3.05	
28*	58.620								
28I	123.541								
28I	382.161	+24.009	-6.909	405.682	825.908	57.322	2.85	2.38	

$$\underline{31^x - 32^x = 22.875 \cdot 101.330}$$

$$-0.478$$

$$22.870$$

$$-65$$

$$\underline{32^x - 33^x = 23.14 \cdot 98.593}$$

$$+0.512$$

$$23.134$$

$$64.2$$

$$\underline{31^x - 11^a = 13.145 \cdot 100.211}$$

$$-0.044$$

$$13.145$$

$$\underline{11^a - 12^a = 27.935 \cdot 98.856}$$

$$+0.502$$

$$27.930$$

$$\underline{33^x - HpA = 31.45 \cdot 92.142}$$

$$+3.872$$

$$31.211$$

Blindstasjon

$$\underline{HpA - 2W = 16.355 \cdot 103.872}$$

$$-0.994$$

$$16.325$$

$$\underline{HpA - HpB = 17.03 \cdot 126.085}$$

$$-6.784$$

$$15.620$$

Blindstasjon

$$\underline{28^I - 28^I = 7.265 \cdot 94.168}$$

$$+0.665$$

$$7.235$$

$$\underline{28^I - 28^{II} = 25.07 \cdot 94.710}$$

$$+2.081$$

$$24.983$$

St.	Azimuth	Δx	Δy	X	Y	H	<u>24</u>
4 B	292,157 203,423			397,030	43,059,450 - 41,692	-43,620	
1	295,580	-2,899	-41,692	394,131	43,017,758	-44,453	
B 1	295,580 200,450			394,131 - 2,986	43,017,758 - 47,828		
2	296,030	-2,986	-47,828	391,145	42,969,930	-41,221	
1 2	296,030 280,947			391,145 - 5,935	42,969,930 - 15,889		
FMI	276,977	-5,935	-15,689	385,210	42,954,241	-38,297	
1 2	296,030 206,686			391,145 + 1,249	42,969,93		
3	302,716	+1,249	-29,254	392,394	42,940,676	-39,438	
2 3	302,716 202,302			392,394 + 2,628	42,940,676 33,269		
4	305,018	+2,628	-33,269	395,022	42,907,407	-37,324	
3 4	305,018 200,527			395,022 + 2,350	42,907,407 - 27,403		
5	305,445	+2,350	-27,403	397,372	42,880,004	-35,498	
4 5	305,445 40,630			397,372 - 3,647	42,880,004 + 4,127		
FMI	146,075	-3,647	+4,127	393,725	42,884,131	-33,407	2
4 5	305,445 192,752			397,372 - 0,214	42,880,004 - 7,544		
FMIII	298,197	-0,214	-7,544	397,158	42,872,466	-31,430	
4 5	305,445 197,840			397,372 + 1,576	42,880,004 - 30,510		
6	303,285	+1,576	-30,510	398,948	42,849,494	-32,182	

3.01

$$B-1 = 41.85 \cdot 96.687$$

$$+ 2.177$$

$$41.793$$

$$1-2 = 48.03 \cdot 95.713$$

$$+ 3.232$$

$$47.921$$

2.46

$$2 - FMI = 16.78 \cdot 98.240$$

$$+ 0.464$$

$$16.774$$

$$2-3 = 29.335 \cdot 96.129$$

$$+ 1.783$$

$$29.281$$

$$3-4 = 33.44 \cdot 95.773$$

$$+ 2.114$$

$$33.373$$

$$4-5 = 27.565 \cdot 95.779$$

$$+ 1.826$$

$$27.504$$

$$5 - FMII = 5.525 \cdot 104.950$$

$$- 0.429$$

$$5.508$$

2.52

$$5 - FMIII = 7.575 \cdot 94.550$$

$$+ 0.648$$

$$7.547$$

3.42

$$5-6 = 30.73 \cdot 93.116$$

$$+ 3.316$$

$$30.551$$

Oppmåling av
bilstøll. fra krysset
linse II og restover.

$$Sy = -178.53x$$

$$1457.874$$

$$H = -34.76$$

FM III er gammelt

fastmerke i det

gamle koordinatnett

$$= Sy \quad H: \text{det gamle nett} - 34.76$$

$$Avvik = 3.33$$

Forts

St.	Heimath	Δx	Δy	X	Y	H
5	303,285			398,948	42,849,494	
6	199,792			+ 1,951		
7	303,077	+1,951	-40,336	400,899	42,809,158	-27,989
6	303,077			400,899	42,809,158	
7	122,636			+ 7,044	+ 3,010	
				407,943	42,812,168	
FMV	25,713	+7,044	+3,010	393,855	42,806,148	-27,11
6	303,077			400,899	42,809,158	
7	220,134			+ 7,822	- 20,495	
8	323,211	+7,822	-20,495	408,721	42. 788,663	-26,987
7	323,211			408,721	788,663	
8	176,553			- 0,152	- 41,056	
9	299,764	-0,152	-41,056	408,569	42. 747,607	-22,142
8	299,764			408,569	747,607	
9	386,590			+ 1,652	+ 7,589	
FMV	86,354	+1,652	+7,589	410,221	42. 755,196	-21,072
8	299,764				747,607	
9	194,455				- 40,190	
FMV	294,219	-3,660	-40,190	404,909	42. 707,417	18,808
VII	92,551			410,221	755,196	21,072
V	212,652					
I	105,203	-3,011	+36,761	407,210	791,957	-27,253
IV	105,203					
I	207,934					
2	113,137	-6,520	+31,144	400,690	823,101	-29,054
2	313,137			407,210	791,957	
I	382,630					
3	95,767	+1,936	+29,078	409,146	821,035	-27,950

I S

$$6-7 = 40.60 \cdot 93.414$$

$$+ 4,193$$

$$40,383$$

$$7 - FM IV = 7.66 \cdot 99.595$$

$$0.83$$

$$+ 0,049$$

$$7.660$$

$$7-8 = 21.96 \cdot 97.069$$

$$+ 1,011$$

$$21,937$$

$$8-9 = 41.34 \cdot 92.535$$

$$+ 4,836$$

$$41,056$$

$$9 - FM V = 106,291 \cdot 7.805$$

$$1.84$$

$$- 0,770$$

$$7,767$$

$$9 - FM VI = 40.38 \cdot 97.822$$

$$+ 1,382$$

$$40,356$$

Glemt & måle
signalthøyde

$$1.74$$

$$I-1 = 37.15 \cdot 107.628$$

$$- 4,446$$

$$36,884$$

$$1-2 = 31.87 \cdot 103.600$$

$$- 1,801$$

$$31,819$$

$$1-3 = 29.15 \cdot 101.523$$

$$- 0,697$$

$$29,142$$

Forts 339

26 Linse 3 fönseringsort

St.	Azimuth	Δx	Δy	X	Y	H	I	S
2	69.468			392.711	254.444	-77.630		
3	208.586			+07.189	20.039		2.54	
4	78.072	+7.189	+20.039	399.900	274.483	-79.665		2.95
3	78.072			399.900	274.483			
4	211.500			+04.518	+27.332		2.885	
5	89.572	+4.518	+27.332	404.418	301.815	-81.406		2.995
2	69.468							
3	208.400						3.10	2.625
4	77.868							
3	77.868							
4	211.321						2.935	2.705
5								
4								
5							2.53	3.195
6								

Garut

Linse 2.

2W	113.664			393.025	019.076	-62.847		
1W	30.895			399.476			2.64	3.035
1W	344.559	+7.230	-8.585	400.255	010.491	-61.766		
1W	344.559							
1WI	246.634						2.94	2.45
1W	391.193	+16.501	-2.297	416.756	008.194	-62.289		
1WI	391.193							
1WI	301.813							
1W	93.006	+4.330	+39.251	421.036	047.445	-62.464	2.27	3.04

Forts fra 15 26

Amm.

Dårlig måleforh.

må ettermåles

$$\begin{array}{r} 3-4: 21,43 \cdot 107,281 \\ \hline -2,445 \end{array}$$

21,290

$$\begin{array}{r} 4-5: 27,745 \cdot 104,247 \\ \hline -1,851 \end{array}$$

27,703

$$3-4: 21,425 \cdot 107,560$$

$$4-5: 27,73 \cdot 103,478$$

$$5-6: 18,165 \cdot 102,743$$

$$\begin{array}{r} IW - IW^I = 11,245 \cdot 96,115 \\ \hline +0,686 \end{array}$$

11,224

$$\begin{array}{r} IW^I - IW^II = 16,66 \cdot 100,128 \\ \hline -0,033 \end{array}$$

16,66

$$\begin{array}{r} IW^II - IW^III = 39,50 \cdot 101,524 \\ \hline -0,945 \end{array}$$

39,489

"BREKKET"

St	Altitude	Δx	Δy	x	y	H	I
2	69.468			392,711	254,444		
3	208,580			+ 7,191	+ 20,022		<u>3.10</u>
4	78,048	+ 7,191	+ 20,022	399,902	274,466	- 82,676 80,643	2.135
3	78,048			399,902	274,466		
4	211,501			+ 4,525	+ 27,317		2.935
5	89,549	+ 4,525	+ 27,317	404,427	301,783	- 82,438 82,387	
4	89,549			404,427	301,783		
5	185,347			+ 6,972	+ 16,755		2.53
6	74,896	+ 6,972	+ 16,755	411,399	318,538	- 82,555 82,504	
5	74,896			411,399	318,538		
6	231,744			- 2,989			<u>2.985</u>
7	106,640	- 2,989	+ 28,549	408,410	347,087	- 82,277	
5	74,896			411,399	318,538		
6	231,767						2.985
7	106,663	- 2,998	+ 28,538	408,401	347,076	82,277	
6	106,663			408,401	347,076		
7	192,075						
8	98,738	+ 0,620	+ 31,294	409,021	378,370	- 82,141	3.08
7	98,738						
8	200,285						
9	99,023	+ 0,515	+ 33,567	409,536	411,937	- 82,287	3.20
8	99,023						
9	204,695						
10	103,718	- 1,921	+ 32,847	407,615	444,784	- 82,372	3.67
9	103,718						
10	180,102						
11	83,820	+ 9,147	35,213	426,76	479,997	⁹⁰ - 87,638	2.74

2.625

$$3-4 = 21,425 \cdot 107,560$$

$$- 2,538$$

21.274

På grunn av
feil målt inst.

2.705

$$4-5 = 27,73 \cdot 103,478$$

$$- 1,514$$

27,689

høyde i p. 3
er høydene i
p 4,5 og 6

korrigert

3.195

$$5-6 = 18,165 \cdot 102,743$$

$$- 0,782$$

18,148

3.14

$$6-7 = 28,705 \cdot 89,787$$

$$+ 0,123$$

28,705

$$6-7 = 28,695 \cdot 100,112$$

$$- 0,050$$

28,695

85,7

3.14

$$7-8 = 31,30 \cdot 99,805$$

$$+ 0,096$$

31,300

Ligg - 85,80

3.12

$$8-9 = 33,625 \cdot 103,592$$

$$- 1,896$$

33,571

- 87,6

3.95

$$9-10 = 33,075 \cdot 106,487$$

$$- 3,365$$

32,903

- 90,7

2.95

$$10-11 = 36,585 \cdot 106,704$$

$$- 3,846$$

36,382

3.32

28 Fortsatt fra s 20

St.	Azimuth	Δx	Δy	X	Y	H	I	S
9c	101,013			374,798	950,777	60,527		
10c	130,986							
Hpl	31,999	+14,786	+8,128	389,584	958,905	-65,452	3,315	-
10c	31,999			389,584				
Hpl	164,857							
13a	396,856	+20,473	-1,012	410,057	957,893	-63,754		2,40
Hpl	396,856							
13a	301,836							
14a	98,692	+0,383	+18,650	410,440	976,543	-64,530	2,15	2,54
8c	Kontrollmåling fra 9c L.L. 42 og 52, bereknet *			375,250	922,376	-60,791		
9c	199,062						3,23	
I	96,848	+1,268	+25,599	376,581	947,975	64,026		
9c	96,848							
I	191,393							
II	88,241	+5,141	+27,514	381,659	975,489	64,092		
I	88,241							
II	176,785							
III	65,026	+14,090	+23,014	395,749	998,503	62,919		
II	65,026							
III	238,396							
IV	803,422	+1,124	+20,891	394,625	19,394	64,738		
III	803,422							
IV	348,058							
42	251,480	-12,653	-13,255	381,972	6,139	63,154		3,24
IV	251,480							
42	68,710							
52	120,190	-9,669	+29,459	372,303	35,598			

$$\underline{10^a - Hp1 = 16.95 \cdot 106.056}$$

$$-1.610$$

$$16.873$$

$$\underline{Hp1 - 13a = 20.51 \cdot 102.179}$$

$$-0.702$$

$$20.498$$

$$\underline{13a - 14a = 18.69 \cdot 103.975}$$

$$-1.166$$

$$18.654$$

$$\underline{9^c - I = 25.63 \cdot 100.013}$$

$$-0.005$$

$$25.630$$

$$\underline{I - II = 27.99 \cdot 100.149}$$

$$-0.066$$

$$27.990$$

$$\underline{II - III = 27.01 \cdot 97.235}$$

$$+1.173$$

$$26.985$$

$$\underline{III - IV = 21.00 \cdot 105.522}$$

$$-1.819$$

$$20.921$$

Koordinater for 42
mält fra Linse 3 =

$$x: 382,377$$

$$y: 44005,610$$

$$H = -63.838$$

$$\Phi 42-52 = 120,176$$

$$\underline{IV - 42 = 18.40 \cdot 105.739}$$

$$-1.656$$

$$18.325$$

$$\underline{42 - 52 = 31.005 \cdot 99.952}$$

$$+0.023$$

$$31.005$$

29								
St.	Azimuth	Δx	Δy	x	y	H	I	S
9	103.718							
10	171.101							
Hp	74.819	+4.579 +4.330	+10.967 +10.370	412.194	455.751	-82.038	2.74	3.22
10	83.820			416.760 479.997	479.997			
11	204.515							
12	88.335	+7.718	+41.647	424.478	521.644	-94.54	3.21	3.42
11	88.335							
12	203.125							
13	91.460	+2.821	+20.904	427.299	542.548	93.236	3.24	3.76
12	91.460							
13	207.496							
14	98.956	+0.456	+27.826	427.755	570.374	99.524	3.66	2.35
13	98.956			427.755	570.374			
14	194.420							
15	93.376	+2.975	+28.682	430.750	599.056	-98.342	2.555	3.08
13	98.956			427.755	570.374			
14	99.776							
Hp ^I	398.729	+9.148	-0.183	436.903	570.191	95.123	2.555	3.05
14	93.376			430.750	599.056			
15	169.530							
16	62.906	+13.500	+26.486	444.250	619.542	94.700 94.700	3.045	3.855
15	62.906			444.250	619.542			
16	39.711							
Hp ^{II}	302.617	+0.886	-21.532	445.136	598.010	-95.305	3.485	3.54
14	398.729							
Hp ^I	233.970							
Hp ³	32.699	+16.540	+9.331	453.443	579.522	-95.243	3.36	2.51

Forsering

$$\begin{array}{r} 10-H_p \in 1194 \cdot 106,129 \\ \hline \end{array}$$

$$\begin{array}{r} \hline -1,085 \\ \hline -1,148 \end{array}$$

$$\begin{array}{r} \hline -1,238 \\ \hline 11,885 \end{array}$$

$$\begin{array}{r} 11-12 = 42,555 \cdot 106,161 \\ \hline \end{array}$$

$$\begin{array}{r} \hline -4,112 \\ \hline \end{array}$$

$$42,356$$

$$12-13 = 21,095 \cdot 100,653$$

$$\begin{array}{r} \hline -0,216 \\ \hline \end{array}$$

$$21,094$$

$$13-14 = 27,83 \cdot 99,949$$

$$\begin{array}{r} \hline +0,022 \\ \hline \end{array}$$

$$27,830$$

$$14-15 = 28,84 \cdot 100,758$$

$$\begin{array}{r} \hline -0,343 \\ \hline \end{array}$$

$$28,838$$

$$-98,4$$

$$14-H_p^I = 9,15 \cdot 100,342$$

$$\begin{array}{r} \hline -0,049 \\ \hline \end{array}$$

$$9,150$$

$$15-16 = 24,535 \cdot 100,436$$

$$\begin{array}{r} \hline -0,168 \\ \hline \end{array}$$

$$24,534$$

$$16-H_p^{II} = 21,56 \cdot 101,950$$

$$\begin{array}{r} \hline -0,660 \\ \hline \end{array}$$

$$21,55$$

$$H_p^I - H_p^{III} = 19,005 \cdot 97,560$$

$$\begin{array}{r} \hline +0,728 \\ \hline \end{array}$$

$$18,991$$

Forts side 33

30 Forst. fra s 3

St	Azimuth	Δx	Δy	x	y	H	L.99
40*	112.533			393.231	41.658	-80.168	
41*	187.023						
42*	99.556	+0.197	+28.192	393.428	69.850	-80.103	
41*	99.556						
42*	74.040						
42N	373.596	+8.341	-3.673	401.769	66.177	79.835	
41 ^I	104.442			381.937	84.457		
41 ^{II}	174.261						
41 ^{III}	78.703	+6.689	+19.245	388.626	103.702	79.502	84.5
41*	99.556			393.428	69.850		
42*	177.842						
43*	77.398	+7.166	+19.329	400.594	89.179	78.015	
42*	77.398						
43*	155.943						
44*	33.341	+7.225	+4.172	407.819	93.351	78.329	83.1
43*	33.341						
44*	233.559						
45*	233.55 66.900	+12.657	22.109	420.476	115.460	77.577	82.6
42*	77.398			400.594	89.179		
43*	68.052						
43N	340.450	+8.487	-11.510	409.081	77.669	78.878	
43*	340.450						
43N	323.306						
44N	63.756	+22.446	+35.072	431.527	112.741	79.038	83.2

Linse 3.

30

I S

3.47

3.19

$$41^* - 42^* = 28.195 \cdot 99.220$$

+ 0,345

28.193

3.29

4.01

$$42^* - 40^N = 9.13 \cdot 103.779$$

- 0,542

9.114

3.84

3.835

$$41^{\text{II}} \cdot 41^{\text{III}} = 20.38 \cdot 101.580$$

- 0,506

20.374

3.28

4.58

$$42^* - 43^* = 20.63 \cdot 97.569$$

+ 0,788

20.615

4.485

3.50

$$43^* - 44^* = 8.37 \cdot 94.889$$

+ 0,671

8.343

3.30

3.59

$$44^* - 45^* = 25.48 \cdot 98.845$$

+ 0,462

25.476

82.6

4.46

4.11

$$43^* - 43^N = 14.31 \cdot 102.281$$

- 0,513

14.301

3.615

3.38

$$43^N - 44^N = 41.64 \cdot 99.885$$

+ 0,075

41.640

ST	Azimuth	Δx	Δy	X	Y	H
4/II 4/III	78,703 188,483			388,626	103,702	
4/II	67,186	+10,391	+18,341	399,017	122,043	-79,075
44x 45x	66,900 233,811			420,426	115,460	77,577
46x	100,711	-0,324	+28,978	420,152	144,438	-77,372
45x 46x	100,711 288,218					
46B	188,929	-9,211	+1,618	410,941	146,056	77,969
43N 44N	63,756 234,458			431,527	112,741	-79,038
45N	98,244	+0,920	+32,800	432,447	145,541	-79,208
45x 46x	100,711 200,209			420,152	144,438	77,372
47x	100,920	-0,468	+32,392	419,684	176,830	78,114
46x 47x	100,920 301,495			419,684	176,830	77,372 78,114
47B	202,415	-9,876	-0,375	409,808	176,455	78,981
46x 47x	100,920 305,450			419,684	176,830	78,114
47I	206,370	-21,114	-2,120	398,570	174,710	-79,057
47I 47x	6,370 218,110			419,684	176,830	
47N	24,480	+11,438	+4,629	431,122	181,459	-79,765
47x 47I	206,370 93,650			398,570	174,710	
47II	100,020	-0,012	+37,605	398,558	212,315	-80,389

		Linse 3		31
3.73	3.23	$\frac{41\text{III} - 41\text{IV} = 21.10 \cdot 97.202}{+0.927}$	21.080	83.9
3.605	3.63	$\frac{45^* - 46^* = 28.98 \cdot 99.825}{+0.080}$	28.980	82.2
3.43	3.41	$\frac{46^* - 46\text{B} = 9.37 \cdot 103.920}{-0.577}$	9.352	83.5
2.89	4.04	$\frac{44\text{N} - 45\text{N} = 32.84 \cdot 102.560}{-1.320}$	32.813	85.2
3.51	3.77	$\frac{46^* - 47^* = 32.41 \cdot 101.968}{-1.002}$	32.395	83.1
3.465	2.78	$\frac{47^* - 47\text{B} = 9.885 \cdot 101.280}{-0.199}$	9.883	83.5
3.465	3.74	$\frac{47^* - 47\text{I} = 21.255 \cdot 103.650}{-1.218}$	21.220	83.5
3.405	3.99	$\frac{47^* - 47\text{N} = 12.54 \cdot 111.414}{-2.236}$	12.339	85.2
3.41	3.13	$\frac{47\text{I} - 47\text{II} = 37.62 \cdot 101.780}{-1.052}$	37.605	-85

32	St	Azimut	Δx	Δy	x	y	H	I
	1W ^{II}	93.006			421.084	47.445	-62.464	
	1W ^{III}	226.037						
	11 ^c	119.043	-7.552	+24.490	413.534	71.935		
	1W ^{III}	119.043			413.534	71.935		
	11 ^c	179.267						
	12 ^c	98.810	+0.508	19.133	414.048	91.068		

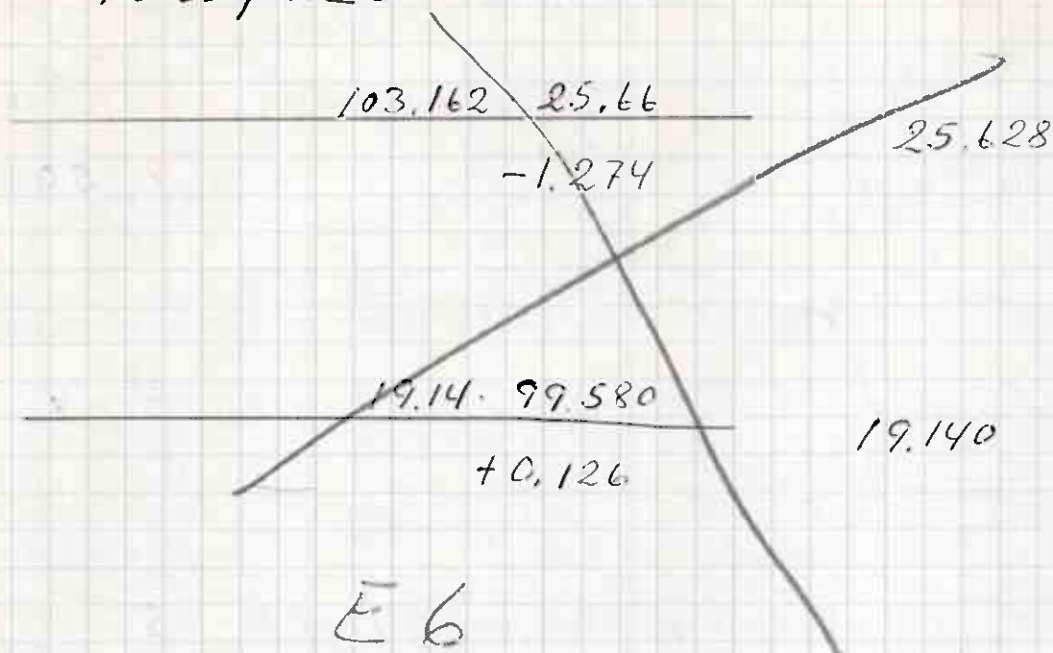
Linse 3 „nye bilstoll“ restover

	43M	63.756			431.527	112.741	-79.038	
	44W	51.615						
	A	315.371	+4.560	-18.885	436.087	93.856	-79.115	3.09
	44M	315.371						
	A	179.717						
	B	295.088	-2.547	-32.939	433.540	60.917	-79.362	2.98
	A	295.088						
	B	179.466						
	C	274.554	-8.899	-21.066	424.641	52.018 39.851	-79.702	2.65
	B	274.554						
	C	233.575						
	D	308.129	+3.701	-28.824	428.342	011.027	-83.623	2.77

S

Forst f.s 26 Brekket

32



$$\begin{array}{rcl} 2.785 & 44N - A = 19.45 \cdot 99.253 & 19.449 \quad 83.5 \\ & + 0.228 & \end{array}$$

$$\begin{array}{rcl} 3.645 & A - B = 33.05 \cdot 101.760 & 33.037 \quad 83.6 \\ & - 0.914 & \end{array}$$

$$\begin{array}{rcl} 2.48 & B - C = 22.87 \cdot 100.475 & 22.869 \quad 83.7 \\ & - 0.170 & \end{array}$$

$$\begin{array}{rcl} 2.85 & C - D = 29.335 \cdot 108.710 & 29.061 \\ & - 4.001 & \end{array}$$

ST	Azimuth	Δx	Δy	X	Y	H	I
15	62.906			444,250	619,542		
16	222.396				598,010	-93,697	
17	85.302	+7.281	+30.976	451,531	650,518	-98,290	3.49
16	85.302						
17	215.348						
18	100.650	-0.226	+22.129	451,305	672,647	-98,264	3.55
17	100.650						
18	169.640						
19	70.290	+9.284	+18.428	460,589	691,075	-99,385	3.225
18	70.290						
19	231.917						
20	102,207	-1.059	+30.533	459,530	721,608	99,734	2.17
19	102,207						
20	192.308						
21	94.515	+2.403	+27.826	461,933	749,434	95,496	4.05
15	293,376			427.755	570,374	94,524	
14	308.490						
A	1,866	+17.572	+0.515	445,327	570,889	99,37	
14	1,866						
A	124.465						
B	326,331	+6.321	-14.400	451,648	556,489	-92,687	
20	94.515						
21	205.555						
Hp	100,070	-0.021	+18.791	461,912	768,225		
20	94.515			461,933	749,434		
21	205.548						
22	100,063	-0.019	+18.783	461,914	768,217	-99,509	2.90
21	100,063						
22	196,355						4.335
23	96.418	+1.676	+29.747	463,590	797,964	98,352	

$$\begin{array}{r}
 3.97 \quad \underline{16-17 = 31.82 \cdot 100.060} \\
 \quad \quad - 0.030 \\
 \quad \quad \quad 31.820
 \end{array}$$

$$\begin{array}{r}
 3.40 \quad \underline{17-18 = 22.13 \cdot 99.609} \\
 \quad \quad + 0.136 \\
 \quad \quad \quad 22.130
 \end{array}$$

$$\begin{array}{r}
 2.32 \quad \underline{18-19 = 20.635 \cdot 100.667} \\
 \quad \quad - 0.216 \times \\
 \quad \quad \quad 20.634 \quad 97.8
 \end{array}$$

$$\begin{array}{r}
 4.015 \quad \underline{19-20 = 30.63 \cdot 104.563} \\
 \quad \quad - 2.194 \\
 \quad \quad \quad 30.551
 \end{array}$$

$$\begin{array}{r}
 3.33 \quad \underline{20-21 = 27.93 \cdot 100.095} \\
 \quad \quad - 0.042 \\
 \quad \quad \quad 27.930
 \end{array}$$

$$\begin{array}{r}
 \underline{14-A = 17.58 \cdot 100.114} \\
 \quad \quad - 0.031 \\
 \quad \quad \quad 17.580
 \end{array}$$

$$\begin{array}{r}
 B-A \\
 \underline{A-B = 15.88 \cdot 108.860} \\
 \quad \quad - 2.203 \\
 \quad \quad \quad 15.726
 \end{array}$$

$$\begin{array}{r}
 \underline{21-Hp = 18.795 \cdot 101.238} \\
 \quad \quad - 0.365 \\
 \quad \quad \quad 18.791
 \end{array}$$

$$\begin{array}{r}
 4.15 \quad \underline{21-22 = 18.785 \cdot 100.891} \\
 \quad \quad - 0.263 \\
 \quad \quad \quad 18.783
 \end{array}$$

$$\begin{array}{r}
 3.40 \quad \underline{22-23 = 29.855 \cdot 104.072} \\
 \quad \quad - 1.908 \\
 \quad \quad \quad 29.794
 \end{array}$$

34	NR I LINSE 2 ost						
264	177,226			409,542	766,540	-46,158	1
274	110,677						
284	87,903	+5,449	+28,331	414,991	794,871	-45,813	2.30
274	87,903						
284	188,943						
294	76,846	+6,059	+15,917	421,05	810,786	-44,926	2.675
284	76,846						
294	211,769						
304	88,615	+3,890	+21,522	424,940	832,308	-42,769	2.875
294	88,615						
304	222,513						
314	111,128	-5,053	+28,614	419,887	860,922	42,609	2.56
304	111,128						
314	192,672						
324	103,800	-1,999	+33,453	417,888	894,375	44,243	3.00
314	103,800						
324	203,835						
334	107,635	-4,889	+40,571	412,999	934,946	45,104	2.04

S

$$\underline{274 - 284 = 28.85 \cdot 100.143}$$

2.71

-0.065

28.850

3.21

$$\underline{284 - 294 = 17.035 \cdot 98.685}$$

+0.352

17.031

2.65

$$\underline{294 - 304 = 22.00 \cdot 93.094}$$

+2.382

21.871

Ligg 46.8

3.115

$$\underline{304 - 314 = 29.06 \cdot 100.865}$$

-0.395

29.057

Ligg 47.1

2.32

$$\underline{314 - 324 = 33.57 \cdot 103.709}$$

-1.954

33.513

3.10

$$\underline{324 - 334 = 40.91 \cdot 102.991}$$

-1.921

40.865

Forts. side 8 ny protokoll

35		Δx	Δy	X	Y	H	
46 ^x 100,920				419,684	176,830	-78,114	I
47 ^x 199,238							
48 ^x 100,158	-0,082	+32,851	419,602	209,681	-79,584	3,425	
47 ^x 100,158							
48 ^x 283,642							
48B 183,800	-10,137	+2,637	409,465	212,318	80,948	3,40	
47 ^x 100,158			419,602	209,681			
48 ^x 200,300							
49 ^x 100,458	-0,298	+41,481	419,304	251,162	-82,784	3,63	
48 ^x 100,458							
49 ^x 178,144						2,51	
I 78,602	+5,048	+14,449	424,352	265,671			
49 ^x 78,602							
I 236,295							
II 114,897	-6,632	+27,821	417,720	293,432			
I 114,897							
II 336,553							
4 251,450	-18,092	-18,935	399,628	274,497	-80,54	80,54	
II 251,450							
4 38,143							
5 89,593	+4,509	+27,334	404,137	301,831	82,250	2,755	

Linse 3

Forts fra s 30

$$\begin{array}{r} S \\ 3.55 \end{array} \quad \begin{array}{r} 47^* - 48^* = 32.89 \cdot 103.088 \\ -1.595 \end{array}$$

32.851

84.9

$$\begin{array}{r} 3.42 \end{array} \quad \begin{array}{r} 48^* - 48B = 10.565 \cdot 108.362 \\ -1.384 \end{array}$$

10.474

86.0

$$\begin{array}{r} 2.625 \end{array} \quad \begin{array}{r} 48^* - 49^* = 41.54 \cdot 103.366 \\ -2.195 \end{array}$$

41.482

-86.7

$$\begin{array}{r} 49^* - I = 15.305 \cdot 100.255 \\ -0.061 \end{array}$$

15.305

Blindstasjon

$$\begin{array}{r} I - II = 28.60 \cdot 100.168 \\ -0.075 \end{array}$$

28.600

$$\begin{array}{r} 2.96 \end{array} \quad \begin{array}{r} II - 4 = 26.26 \cdot 95.316 \\ +1.930 \end{array}$$

26.189

$$\begin{array}{r} 2.48 \end{array} \quad \begin{array}{r} 4 - 5 = 27.74 \cdot 103.295 \\ -1.435 \end{array}$$

27.703

Koordinater for p.s målt fra brekket

X: 404.427 Y: 301.783 H: -82.438

$$\phi_{4-5} = 89.549$$

Försering			x	y	H	I
14	1.866			445.32757	0.889	-95.37
A	124.400					
B	326.266	+6.305	-14.405	451.632	656.484	2.68
A	326.266					
B	159.852					
C	286.118	-6.794	-30.661	444.838	525.823	
22	96.418			463.590	797.964	
23	211.282					92.352
24	107.700	-1.790	+14.728	463.		
				461.800		
				465.380	812.692	92.977 3.165
23	107.700					
24	228.666					
25	136.366	-15.558	+24.207	446.242	836.899	¹⁰⁰ 99.116 2.93
24	136.366					
25	199.145					
26	135.511	-17.901	+28.692	428.341	865.591	-100.508 2.70
25	135.511					
26	198.590					
27	134.101	-13.306	+22.418	415.035	888.009	-100.833 3.085
26	134.101					
27	163.653					
28	97.754	+0.037	+26.555	415.972	914.564	-98.862 2.81
27	97.754					
28	188.506					
29	86.260	+6.29	+28.689	422.626	943.253	¹⁰⁰ -99.334 3.985
28	86.260					
29	214.342					
30	100.602	-0.250	+26.444	422.376	969.697	⁹⁹ 98.249 2.35

$$A-B = 15.88 \cdot 91.088$$

$$+2.216$$

15.725

Ventilasjonsort

$$B-C = 31.51 \cdot 94.803$$

$$+2.570$$

31.405

Ventilasjonsort

$$23-24 = 14.845 \cdot 102.230$$

$$-0.520$$

14.836

3.06

$$24-25 = 28.81 \cdot 103.148$$

$$-1.424$$

28.775

3.215

$$25-26 = 33.865 \cdot 103.352$$

$$-1.782$$

33.818

3.09

$$26-27 = 26.07 \cdot 100.061$$

$$-0.025$$

26.070

2.785

$$27-28 = 26.625 \cdot 95.977$$

$$+1.681$$

26.572

4.10

$$28-29 = 29.37 \cdot 99.972$$

$$+0.013$$

29.370

2.50

$$29-30 = 26.445 \cdot 100.025$$

$$-0.010$$

26.445

3.445

ST	Aeimuth	Δx	Δy	X	Y	H	I
13	98.956			427.755	427.755	570.374	-94.524
14	286.734						
14 ^I	185.690	-23.736	+5.427	404.019	575.801	95.352	2.36
14	185.690						
14 ^I	125.703						
14 ^{II}	111.393	-4.769	+26.361	399.250	602.162	98.615	2.53
14 ^I	111.393						
14 ^{II}	179.285						
14 ^{III}	90.678	+6.290	+42.649	405.540	644.811	-95.249	3.18
14 ^I	90.678						
14 ^{III}	210.759						
14 ^{IV}	101.437	-0.626	+27.729	404.914	672.540	-96.048	3.40
14 ^{II}	101.437						
14 ^{IV}	194.967						
14 ^V	96.404	+2.055	+36.334	406.969	708.874	-95.547	2.84
IV	96.404						
V	199.063						
VI	95.467	+2.883	+40.417	409.852	749.291	-95.842	3.53
V	95.467						
VI	201.977						
VII	97.444	+0.676	+16.834	410.528	766.125	-96.314	3.09

$$14 \cdot 14^I = 24.35 \cdot 100.675$$

2.79

- 0.258

24.349

L. 99 = 97.7

$$14^I - 14^{II} = 26.79 \cdot 100.459$$

3.46

- 0.193

26.789

L. 99 99.4

$$14^{II} - 14^{III} = 43.12 \cdot 101.349$$

3.46

- 0.914

43.110

100.3

$$14^{III} - 14^{IV} = 27.74 \cdot 101.031$$

3.05

- 0.449

27.736

100.4

$$14^{IV} - 14^V = 36.395 \cdot 100.768$$

3.78

- 0.439

36.392

100.9

$$14^V - 14^{VI} = 40.52 \cdot 100.196$$

3.36

- 0.125

40.520

$$14^{VI} - 14^{VII} = 16.86 \cdot 102.387$$

3.25

- 0.632

16.848

ST	A = math	Δx	Δy	x	y	H	I	S
16 ²	78.884			431.833	349.861	-61.963		
17 ²	164.288						3.48	
18 ²	43.172	+13.890	+11.190	445.723	361.051	-61.424		2.15
17 ²	43.172							
18 ²	231.195						2.07	
19 ²	74.367	+6.586	+15.463	452.309	376.514	58.011		2.50
18 ²	74.367							
19 ²	121.740						2.54	
20 ²	396.107	+21.401	-1.310	450.999 473.710	375.204	53.535		4.53
19 ²	396.107							
20 ²	102.221							
21 ²	298.328	-0.638	-24.283	473.073	350.921	52.377	4.44	3.40
20 ²	298.328							
21 ²	196.779							
22 ²	295.107	-3.002	-38.977	470.071	311.944	50.803	3.32	4.08
21 ²	98.328			473.710	375.204			
20 ²	217.901							
21 ²	116.229	-3.967	+15.222	469.743	390.426	55.273	4.38	3.32
20 ²	116.229							
21 ²	171.355							
22 ²	87.584	+4.013	+20.314	473.756	410.740	55.815	3.30	3.49
21 ²	295.107							
22 ²	199.467			470.071	311.944	-50.803		
23 ²	294.574	-1.746	-20.442	468.325	291.502	49.531	4.02	4.41
22 ²	294.574							
23 ²	209.108							
24 ²	303.682	+1.471	-25.410	469.796	266.092	46.997	4.16	2.83
								?

$$\begin{aligned} \underline{17^2 - 18^2} &= 17.935 \cdot 93.353 \\ &+ 1.869 \end{aligned}$$

17.837

$$\begin{aligned} \underline{18^2 - 19^2} &= 17.07 \cdot 88.817 \\ &+ 2.983 \end{aligned} = 16.807$$

$$\begin{aligned} \underline{19^2 - 20^2} &= 21.585 \cdot 92.653 \\ &+ 2.486 \end{aligned}$$

21.441

$$\begin{aligned} \underline{20^2 - 21^2} &= 24.39 \cdot 94.254 \\ &+ 2.198 \end{aligned} = 24.291$$

$$\begin{aligned} \underline{21^2 - 22^2} &= 39.10 \cdot 98.675 \\ &+ 0.814 \end{aligned}$$

39.092

22² Skutt vekk

$$\begin{aligned} \underline{20^2 - 21^2} &= 15.745 \cdot 102.742 \\ &- 0.678 \end{aligned}$$

15.730

AKP ØST

$$\begin{aligned} \underline{21^2 - 22^2} &= 20.72 \cdot 102.251 \\ &- 0.732 \end{aligned}$$

20.707

AKP ØST

$$\begin{aligned} \underline{22^2 - 23^2} &= 20.535 \cdot 97.266 \\ &+ 0.882 \end{aligned}$$

20.516

$$\begin{aligned} \underline{23^2 - 24^2} &= 25.775 \cdot 89.920 \\ &+ 4.064 \end{aligned}$$

25.453

Nr I Linse 2 og vestover til Loh. strossene

St	Azimuth	Δx	Δy	X	Y	H	I
214	55.916			433,874	648,213	-39,096	
224	66.401						
I	322.317	+4,878	-13,339	438,752	634,874	-39,776	2.975
224	322.317						
I	173.278						
II	295.595	-2,066	-29,812	436,686	605,062	-37,286	
22	322.317						
I	173.279						2.625
II	295.596	-2,066	-29,814	436,686	605,062	-37,286	
I	295.596						
II	198.249						
III	293.845	-2,210	-22,789	434,476	582,271	37,011	2.95
1	95.767						
3	202.785						
4	98.552	+0,489	+21,474	409,635	842,509	-27,916	
3	98.552						
4	199.155						
5	97.707	+1,042	+28,909	410,677	871,418	-33,436	
4	97.707						
5	27.028						
27	324.735	+9,364	-22,875	420,041	848,543	-32,648	
4	97.707						
5	195.610						
23	93.317	+0,367	+3,485	411,044	874,903	-31,980	

Går ut

S

$$224 - I = 14,21 \cdot 101,996$$

2.74

$$- 0,445$$

14.203

$$I - II = 29,95 \cdot 95,783$$

gar ut
- 1,982

29.884

3.15

$$I - II = 29,95 \cdot 95,821$$

$$+ 1,965$$

29.885

$$II - III = 22,90 \cdot 98,860$$

2.815

$$+ 0,410$$

22.896

$$3-4 = 21,48 \cdot 99,899$$

$$+ 0,034$$

21.480

Kasse 8 L. 2
kom. ord.

Forts. f. s 25

$$4-5 = 29,45 \cdot 112,004$$

$$- 5,520$$

28.928

$$27 = 1433,744$$

$$- 156,32 x$$

$$H = -35,972$$

$$5-27 = 24,72 \cdot 101,060$$

$$- 0,412$$

24.717

1.20

$$28 \quad y = 1448,195$$

$$x = 141,928$$

$$H = 31,869$$

$$5-28^x = 3,51 \cdot 103,71$$

$$- 0,204$$

3.504

1.66

$$28^x \quad y = 1460,136$$

$$x = -165,283$$

$$H = 35,31$$

gamle koordinater

$$35,31$$

$$31,98$$

$$3,33$$

ST	Azimuth	Δx	Δy	x	y	H	I	S
23 ²	303.682			469.796	266.092	-46.797		
24 ²	207.603							
25 ²	311.285	+4.146	-23.145	473.942	242.947	-42.851	4.50	4.75
21A	87.584			473.756	410.740			
22A	214.188							
23A	101.772	-0.891	+31.997	472.865	442.737	-59.966		3.575
22A	101.772							
23A	201.739							
24A	103.511	-0.930	+16.842	471.935	459.579	-60.987	3.56	2.80
23A	103.511							
24A	171.549							
25A	75.060	+10.228	+24.759	482.163	484.338	-57.887	2.62	1.37
24 ²	311.285			473.942	242.947	-42.851		
25 ²	192.906							
26 ²	304.191	+2.140	-32.457	476.082	210.490	-35.882	3.93	4.69
24A	75.060			482.163	484.338			
25A	213.653							
26A	88.713	+4.360	+24.335	486.523	508.673	-57.694	4.07	3.34
25 ²	304.191							
26 ²	192.340							
27 ²	296.531	-7.701	-31.183	474.381	179.307	-30.782	4.25	4.72
26 ²	296.531							
27 ²	204.728							
28 ²	301.259	+0.709	-35.854	475.090	1143.457	-27.793	4.60	5.15

$$\underline{24^2 - 25^2 = 23.92 \cdot 88.234}$$

$$+ 4.396$$

$$23.513$$

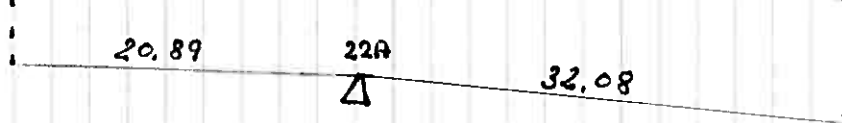
$$\underline{22A - 23A = 32.08 \cdot 104.248}$$

$$- 2.139$$

$$32.009$$

Høyden for 23A er beregnet slik

21A
3.18



23A
3.575

Vertikal 21A -
22A = 109.016

$$\underline{23A - 24A = 16.87 \cdot 100.985}$$

$$- 0.261$$

$$16.868$$

$$\underline{24A - 25A = 27.14 \cdot 89.752}$$

$$+ 4.350$$

$$26.789$$

$$\underline{25^2 - 26^2 = 32.99 \cdot 89.320}$$

$$+ 5.509$$

$$32.527 \text{ AKP vest}$$

$$\underline{25A - 26A = 24.74 \cdot 97.624}$$

$$+ 0.923$$

$$24.723$$

$$\text{AKP ØST}$$

$$\underline{26^2 - 27^2 = 31.57 \cdot 90.630}$$

$$+ 4.630$$

$$31.229$$

$$\text{AKP vest}$$

$$\text{Forts side 11}$$

$$\text{"ny" protokoll}$$

$$\underline{27^2 - 28^2 = 35.94 \cdot 95.677}$$

$$+ 2.439$$

$$35.857$$

Linse 3 og vestover fra brekket
til nye bilstoll

ST	Azimuth	Δx	Δy	X	Y	H
52 42	320,176 155,167			382.377	44. 005.610	-63838
I	275.343	-12,332	-30,232	370.045	975.378	-71,878
42 I	275.343 201,484					
II	276,827	-12,024	-31,561	358,021	943,817	-75,962
I II	276,827 238,682					
III	315.509	+6,992	-28,130	365,013	915,687	77,729
II III	315.509 174,007					
IV	289,516	-5,202 -5,143	-31,303 -30,946	359,811 359,870	884,384 884,741	-77,656
III IV	289,516 205,565					
V	295,081	-2,346	-30,296	357,465 357,524	854,088 854,445	-78,103
IV V	295,081 199,274					
VI	294,355	-2,483	-27,926	354,982 355,041	826,162 826,519	-78,579
V VI	294,355 208,556					
VII	302,911	+1,614	-35,267	356,596 356,655	790,895 791,252	-80,564
VI VII	302,911 330,996					
VIII	33,907	+26,448	+15,589	383,044 383,103	806,484 806,841	77,087
1y						

E 6

41

I

S

122.204

3.255

$$42 - I = 33.00 \cdot 109.264$$

$$- 4.785$$

32.651

$$I - II = 34.02 \cdot 107.660$$

$$- 4.084$$

33.774

$$II - III = 29.04 \cdot 103.875$$

$$- 1.767$$

28.986

$$III - IV = 31.73 \cdot 99.854$$

$$+ 0.073$$

 31.730
~~31.370~~

$$IV - V = 30.39 \cdot 100.937$$

$$- 0.447$$

30.387

$$V - VI = 28.04 \cdot 101.080$$

$$- 0.476$$

28.036

$$VI - VII = 35.36 \cdot 103.575$$

$$- 1.985$$

35.304

$$VII - 14 = 30.70 \cdot 99.840$$

$$+ 0.077$$

30.700

3.40

Forts. n. side

ST	Azimuth	Δx	Δy	x	y	H	I
24	33.907						
24	201.432						
24	35.329	+23.497	+14.567	406.541 406.604	821.051 821.408	-78.108	3.32
14	35.329						
24	218.617						
34	53.946	+22.647	+25.644	429.188 429.247	846.695 847.052	-77.403	2.59
24	53.946						
34	255.015						
Rp.	108.961	-2.371	+16.730	426.876	863.782	-77.11	2.23
24	53.946						
34	255.012						2.685
44	108.958	-2.369	+16.721	426.819 426.878	863.416 863.773	-77.110	
34	108.958						
44	184.242						4.155
54	93.200	+2.362	+22.025	429.181 429.240	885.441 885.798	-81.000	
44	93.200						
54	194.614						2.85
64	87.814	+2.040	+10.528	428 431.280 431.221	895.969 896.326	-80.956	
54	87.814						
64	275.701						
74	163.515	-11.811	+7.622	419.410 419.469	903.591 903.948	-81.729	3.115
64	163.515						
74	137.975						
84	75.850			418.846	927.683		2.93
74	101.490	-0.564	+24.092	418.905 418.905	928.040 928.040	-82.041	
74	101.490						
84	75.850						
84	158.942						
94	39.242			425.263	936.642		3.29
	60.432	+6.417	+8.959	425.322 425.322	936.999 936.999	-81.353	

5

E6 Östover

42

2.77

$$\begin{aligned} 1y - 2y &= 27.65 \cdot 101.086 \\ &- 0.471 \end{aligned}$$

27.646

E6 vestover
side 45

2.89

$$\begin{aligned} 2y - 3y &= 34.215 \cdot 99.247 \\ &+ 0.405 \end{aligned}$$

34.213

Ligg -81.6

4.23

$$\begin{aligned} 3y - Rp &= 16.94 \cdot 104.555 \\ &- 1.211 \end{aligned}$$

16.897

4.175

$$\begin{aligned} 3y - 4y &= 16.93 \cdot 104.505 \\ &- 1.197 \end{aligned}$$

16.888

82.8

3.01

$$\begin{aligned} 4y - 5y &= 22.32 \cdot 107.850 \\ &- 2.745 \end{aligned}$$

22.151

Ligg 5y
Kontroller +85.4
vertikalvinkel 85
på neste måling

3.25

$$\begin{aligned} 5y - 6y &= 10.73 \cdot 102.110 \\ &- 0.356 \end{aligned}$$

10.724

85.7

2.95

$$\begin{aligned} 6y - 7y &= 14.05 \cdot 102.755 \\ &- 0.608 \end{aligned}$$

14.037

86.2

3.49

$$\begin{aligned} 7y - 8y &= 24.115 \cdot 102.304 \\ &- 0.872 \end{aligned}$$

24.099

87

3.31

$$\begin{aligned} 8y - 9y &= 11.04 \cdot 96.144 \\ &+ 0.668 \end{aligned}$$

11.020

86

ST	Azimuth	Δx	Δy	x	y	H	I	S
B1	172,374			520,74				
B2	192,507					+28.24	1.845	
I	164,881	-25,914	+15,947	494,826	142,307	24.017		
B2	164,881							
I	200,865							
II	165,746	-27,163	+16,211	467,663	158,518	+20,962		
I	165,746							
II	200,647							
III	166,393	-27,132	+15,820	440,531	174,338	17,76		
II	166,393							
III	197,928							
IV	164,321	-35,588	+22,334	404,934	196,672	12,696		
III	164,321							
IV	267,497							
3V	231,818	-17,956	-9,804	386,987	186,868	+15,390		2.41
IV	231,818							
3V	266,106							
4V	297,924	-1,205	-36,954	385,782	149,914	+16,935	2.54	1.88
3V	297,924							
4V	145,404							
5V	243,328	-16,951	-13,724	368,831				
4V	243,328							
5V	204,615							
6V	247,943	-23,334	-21,873	345,497				

Fra åpning i bilstollen til vaskehall 43
Fastmerkene i betongtak. Bolt 1 og 2

$$\text{Bolt 2 - I} \quad 30.52 \cdot 104.965$$

$$- 2.378$$

$$30.427$$

$$\text{I - II} = 31.78 \cdot 106.129$$

$$- 3.055$$

$$31.633$$

$$\text{II - III} = 31.57 \cdot 106.469$$

$$- 3.202$$

$$31.407$$

$$\text{III - IV} = 42.32 \cdot 107.636$$

$$- 5.064$$

$$42.016$$

$$\text{IV - FM} = 20.46 \cdot 99.117$$

$$+ 0.284$$

$$20.458 \quad \text{3V er gammelt f.m.}$$

$$x = -194.046 \quad y = 712.13$$

$$H = +14$$

$$\text{3V - 4V} \quad 37.04 \cdot 96.208$$

$$+ 2.205$$

$$36.974$$

$$\text{4V - 5V} = 21.81 \cdot 99.906$$

$$+ 0.032$$

$$21.810$$

$$\text{5V - 6V} = 32.20 \cdot 107.391$$

$$- 3.730$$

$$31.983$$

							I	S
5V	247.943							
6V	187.082							
7V	235.025	-27.314	-16.753	318.183				
3V	297.924							
4V	195.404							
5V	293.328	-2.282	-21.690	383.500	128.224	+18.067	1.87	2.97
4V	293.328							
5V	204.615							
6V	297.943	-1.033	-31.966	382.467	096.258	13.957	2.99	2.61
5V	297.943							
6V	187.082							
7V	285.025	-7.468	-31.160	374.999	065.098	12.115	2.59	3.83
6V	285.025							
7V	207.617							
8V	292.642	-2.795	-24.077	372.204	41.021	+7.43	3.675	—
7V	292.642							
8V	170.590							
9V	263.232	-8.071	-12.385	364.133	28.636	+9.882	—	2.68
8V	263.232							
9V	246.496							
10V	309.728	+2.061	-13.305	366.194	15.331	?	2.57	?
9V	309.728							
10V	195.855							
11V	305.583	+1.797	-20.441	367.991	41.994	890		
10V	305.583							
11V	183.456							
12V	289.039	-6.129	-35.246	361.862	959.644		2.90	3.25

$$\begin{array}{r}
 6V - 7V = 32.19 \cdot 106.195 \\
 - 3.082 \\
 \hline
 32.042
 \end{array}$$

$$\begin{array}{r}
 4V - 5V = 21.81 \cdot 99.906 \\
 + 0.032 \\
 \hline
 21.810
 \end{array}$$

$$\begin{array}{r}
 5V - 6V = 32.20 \cdot 107.391 \\
 - 3.730 \\
 \hline
 31.983
 \end{array}$$

$$\begin{array}{l}
 6V = 715 \\
 H = +12.74
 \end{array}$$

$$\begin{array}{r}
 6V - 7V = 32.19 \cdot 106.195 \\
 - 3.082 \\
 \hline
 32.042
 \end{array}$$

$$\begin{array}{r}
 7V - 8V = 24.26 \cdot 102.648 \\
 - 1.009 \\
 \hline
 24.239
 \end{array}$$

Blindstasjon

$$\begin{array}{r}
 8V - 9V = 14.785 \cdot 100.985 \\
 - 0.229 \\
 \hline
 14.783
 \end{array}$$

$$\begin{array}{r}
 9V - 10V = 13.47 \cdot 101.920 \\
 - 0.406 \\
 \hline
 13.464
 \end{array}$$

Signalhøyde ikke målt

$$\begin{array}{r}
 10V - 11V = 20.52 \cdot 100.212 \\
 - 0.068 \\
 \hline
 20.520
 \end{array}$$

$$\begin{array}{r}
 11V - 12V = 35.79 \cdot 101.871 \\
 - 1.052 \\
 \hline
 35.775
 \end{array}$$

ST	Azimuth	Δx	Δy	X	Y	H	I	S
1y	35.329			406.541	821.051			
2y	152.826			406.600	821.408	-78.108	1	S
10y	393.155	+13.991	-1.510	420.632	819.541			
				420.591	819.898	-80.010	2.64	2.485
2y	393.155							
10y	93.343							
11y	286.498	-3.824	-17.759	416.708	801.782			
				416.767	802.139	-80.234	2.485	3.38
10y	286.498							
11y	217.285							
12y	303.783	+1.836	-30.860	418.544	770.922			
				418.603	771.279	-80.301	3.11	3.10
11y	303.783							
12y	188.887							
13y	292.670	-4.112	-35.552	414.491	735.727	-80.418	2.93	3.055
11y	303.783			418.603	771.279	-80.301		
12y	189.413							
13y	293.196	-2.703	-25.194	415.841	745.728			
				415.900	746.085	-79.81	2.70	3.42
12y	293.196							
13y	242.305							
14y	340.501	+9.220	-12.482	425.061	733.246			
				425.12	733.603	-80.976	3.18	2.29
13y	340.501							
14y	159.427							
15y	299.928	-0.032	-28.460	425.029	704.786	-81.444	2.25	1.89
13y	340.501							
14y	136.600							
Hp	272.101	-4.507	-11.985	420.554	721.261	-82.842	-	-
14y	299.928							
15y	204.157							
16y	304.085	+1.957	-30.451	426.986	674.335	-82.824	1.74	3.14

Går ut

$$\begin{array}{r} 2y - 10y = 14,18 \cdot 107,864 \\ - 1,747 \end{array}$$

14,072

$$\begin{array}{r} 10y - 11y = 18,20 \cdot 103,917 \\ - 1,119 \end{array}$$

18,166

$$\begin{array}{r} 11y - 12y = 30,915 \cdot 100,117 \\ - 0,057 \end{array}$$

30,915

$$\begin{array}{r} 12y - 13y = 35,779 \cdot 100,429 \\ - 0,242 \end{array}$$

35,789

$$\begin{array}{r} 12y - 13y = 25,34 \cdot 100,577 \\ - 0,229 \end{array}$$

25,339

$$\begin{array}{r} 13y - 14y = 15,52 \cdot 101,132 \\ - 0,276 \end{array}$$

15,518

$$\begin{array}{r} 14y - 15y = 28,46 \cdot 100,243 \\ - 0,108 \end{array}$$

28,460

$$\begin{array}{r} 14y - 14p = 12,81 \cdot 98,090 \\ + 0,384 \end{array}$$

12,804

Blinclstasjon

$$\begin{array}{r} 15y - 16y = 30,64 \cdot 105,784 \\ - 2,78 \end{array}$$

30,594

11V 289.039			361.862	959.644	H	2.78	3.35
12V 210.390							
13V 299.429	-0.269	-30.034	361.593	929.610	+10.267		
12V 299.429							
13V 213.207							
I 312.636	+6.736	-33.492	368.329	896.118	12.356	3.33	
13 312.636							
I 168.473							
II 281.109	-8.087	-26.447	360.242	869.671	7.216		
I 281.109							
II 215.160							
III 296.269	-1.783	-30.392	358.459	839.279	8.205		
II 296.269							
III 193.445							
IV 294.714	-1.840	-22.112	356.619	817.167	9.189		
12V 299.429							
13V 207.744							
14V 307.173	+1.215	-10.735	362.808	918.875	+11.510	3.07	3.56
13V 307.173							
14V 177.747							
15V 284.920	-5.568	-23.064	357.240	895.811	+9.680	3.62	2.59
13V 307.173							
14V 231.022							
15V 338.195	+13.581	-19.852	376.889	899.023	+13.611	3.62	3.24
14V 284.920							
15V 202.503							
16V 287.423	-6.798	-23.96	350.442	861.851	+12.129	2.26	3.67

Nivelering
fra 9V - 13V

$$12V - 13V = 30.04 \cdot 98.847$$

$$+ 0.544$$

$$30.035$$

$$13 - I = 34.59 \cdot 89.985$$

$$+ 5.419$$

34.163 Blindstasjon

$$I - II = 28.13 \cdot 111.698$$

$$- 5.140$$

27.656 Blindstasjon

$$II - III = 30.46 \cdot 97.733$$

$$- 0.989$$

30.444 - "

$$III - IV = 22.21 \cdot 97.180$$

$$+ 0.984$$

22.188 - "

gjelder oppmåling av
sørvegg mot sjakt 1

$$13V - 14V = 10.83 \cdot 95.572$$

$$+ 0.753$$

$$10.804$$

$$14V - 15V = 23.74 \cdot 102.146$$

$$- 0.800$$

23.727 Forts. side 32
ny protokoll

$$14V - 15V = 24.78 \cdot 93.469$$

$$+ 2.476$$

24.053 Gjennomslag stor feste

$$15V - 16V = 34.65 \cdot 98.090$$

$$+ 1.039$$

34.634 Skutt vekk

10.52

Triangelpunkt ved Fageråsen Camping

y 41118.22 x 925.307,76

H + ~~8~~ 57.8
