



Bergvesenet rapport nr <b>2427</b>	Intern Journal nr 09/00084-1 vedl 1	Internt arkiv nr 	Rapport lokalisering	Gradering
Kommer fra ..arkiv Intex Resources ASA	Ekstern rapport nr 11656-001	Oversendt fra Molynor AS	Fortrolig pga 	Fortrolig fra dato:
Tittel An Investigation into the Recovery of Molybdenum Ore Composite from the Hurdal Orebody				
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Kommune Hurdal	Fylke Akershus	Bergdistrikt	1: 50 000 kartblad 19154	1: 250 000 kartblad Hamar
Fagområde Oppredning miljø	Dokument type		Forekomster (forekomst, gruvefelt, undersøkelsesfelt) Hurdalfeltet Nordli Nordliforekomsten	
Råstoffgruppe Malm/metall	Råstofftype Mo			

### Sammenheng, innholdsfortegnelse eller innholdsbeskrivelse

Rapporten er på engelsk og er utført av SGS Lakefield Research Limited på oppdrag for Intex Resources ASA). Rapporten omhandler formålstesting av reagenser og flytskjema-muligheter for flotasjonsutvinningen av molybden på malm fra Hurdalen.

En får beskrevet hvordan 155 kg med borkjernemateriale blir prosessert ned til aktuelle provestørrelser for de forskjellige testene som maletest og flere forskjellige oppredningstekniske forsøk.

Rapporten beskriver videre bruken av forskjellige reagenser i flot.forsøkene. her oppnår en et konsentrat på 57% Mo med en utvinning på 78%. Det anslås at en kontinuerlig flotasjon vil øke utvinningen til 85-90%.

Det foreslås flere alternativer til flotasjonsagenser, flotasjon fra flere soner i forekomsten, malbarheten i forhold til malmhardhet og avgangens påvirkning på det ytre miljøet.

IKKE SKANNET

VEDLEGG 1 av 5  
J.nr. 09/00084-1

**An Investigation into**  
**THE RECOVERY OF MOLYBDENUM ORE**  
**COMPOSITE FROM THE HURDAL ORE BODY**

prepared for

**Intex Resources ASA**

Project 11656-001 – Final Report  
July 22, 2008

**NOTE:**

This report refers to the samples as received.

The practice of this Company in issuing reports of this nature is to require the recipient not to publish the report or any part thereof without the written consent of SGS Minerals Services.

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## *Executive Summary*

This report summarizes scoping testwork completed for Intex Resources ASA (formerly Crew Minerals AS). The testwork investigated reagent and flowsheet options for the flotation recovery of molybdenum, on ore from the Hurdal property in Sweden. The scope of the program involved: sample preparation of a single composite, grindability testing, high-definition QEMSCAN<sup>TM</sup> mineralogical characterization, rougher kinetics testing, and batch cleaner testing. The Hurdal composite graded 0.12% Mo and 0.79% S. Grindability testing on the Hurdal composite resulted in a Bond Ball Work Index (BWI) of 14.7 kWh/t. Relative to other BWI indices in the SGS database, this result is indicative of a medium hardness ore.

Four rougher kinetics tests were performed. Commercial diesel (Diesel #2) was used as the 'fuel oil' collector, and pine oil was used as the frother. The rougher kinetics tests indicated that a flotation time of at least 20 minutes would be required for maximum recovery of molybdenum, at a primary grind of  $P_{80} = 114 \mu\text{m}$ . Rougher molybdenum recoveries using this primary grind were typically in the range of 90-92%.

Subsequent cleaner testing further explored changes and optimization to reagent addition in the roughers. Fuel oil dosage was reduced from 80 g/t to 55 g/t, and pine oil was eliminated in favour of MIBC. The combined effect of these two changes allowed for better molybdenum upgrading in the cleaners. MIBC dosage in the roughers was 50 g/t.

Six cleaner tests were performed to study the effects of different reagents, dosages, and regrind, on the upgrading characteristics of the ore. It was determined that only 4-5 cleaner stages were required to sufficiently upgrade the final concentrate to a saleable grade (at least 50% Mo).

Two dispersants were tested to mitigate the presence of talc-like mineralization (phyllosilicates) in the cleaner concentrates: carboxy-methyl cellulose (CMC) and sodium silicate ( $\text{Na}_2\text{SiO}_3$ ). Sodium silicate was more effective at this function since CMC adversely affected molybdenum recovery. With higher sodium silicate dosages, concentrate grades improved but at the expense of molybdenum recovery to the final concentrate.

The cleaner test with the best metallurgical performance utilized a conventional lime/NaCN pyrite depressant scheme, five stages of cleaning, and a second regrind before the fifth stage of cleaning. The final concentrate graded 57% Mo with a 78% molybdenum recovery to the final concentrate. In a continuous environment with re-circulation of middling streams, SGS anticipates molybdenum recoveries would improve to 85-90%.

Mineralogical characterization (by XRD and QEMSCAN<sup>TM</sup> analysis) of a rougher concentrate indicated that it largely consisted of molybdenite, with minor amounts of pyrite. The largest constituent of non-sulphide gangue was quartz. Molybdenite was highly liberated in the rougher concentrate sample. Based on the test results and the mineralogical investigation, the Hurdal ore is not considered to be highly refractory in nature. Molybdenite liberation of 96% can be achieved with a regrind size of 20 µm.

## ***Introduction***

This report summarizes scoping testwork completed for Intex Resources ASA (formerly Crew Minerals AS). The testwork investigated reagent and flowsheet options for the flotation recovery of molybdenum on ore from the Hurdal property in Sweden. The scope of the program involved: sample preparation of a single composite, grindability testing, QEMSCAN<sup>TM</sup> mineralogical characterization, rougher kinetics testing, and batch cleaner testing. All work referenced in this report was completed under the internal SGS project number of CALR-11656-001.

The primary goal of this testwork was to assess the flotation response of the ore and conceptualize a flowsheet. Various reagents and flowsheets were examined to achieve this goal.

The testing program was completed over the months of September 2007 to January 2008. Mr. Jon Steen Petersen, and Ms. Jette Blomsterberg, both of Intex Resources ASA, were regularly updated with new results as the testing progressed.



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## *Testwork Summary*

### 1. Sample Receipt and Preparation

Approximately 155 kg of drill core shipped from Crew Minerals' Hurdal Molybdenum ore body was received at the SGS Lakefield site on August 28, 2007. This shipment was assigned the receipt number of 0373-AUG07. Upon receipt, sample inventory and weights were taken, and compared with a shipping list from the client. The inventory list is given in Appendix A. Once inventoried, the drill core was crushed to -6 mesh and combined, and 10 kg of material riffled out for Bond ball mill work index testing. The remainder of the material was stage crushed to -10 mesh and riffled into 10 kg charges. Approximately 150 grams of material was extracted for head sample chemical analysis.

### 2. Material Characterization

#### 2.1. Chemical Analysis

The head analysis sample obtained from initial sample preparation was assayed for Mo, W, and S and included an ICP metal scan. A list of the assays is given in Table 1.

**Table 1. Head Assay of Hurdal Drill Core Composite**

Element	Assay	Element	Assay
<i>XRF</i>		<i>ICP</i>	
Mo %	0.12	Li g/t	< 5
W %	< 0.01	Mg g/t	1800
S %	0.79	Mn g/t	200
<i>ICP</i>		Na g/t	28000
Ag g/t	0.3	Ni g/t	25
Al g/t	60000	P g/t	390
As g/t	< 10	Pb g/t	6
Ba g/t	460	Sb g/t	< 0.8
Be g/t	3.3	Se g/t	< 10
Bi g/t	< 0.6	Sn g/t	< 2
Cu g/t	2300	Sr g/t	160
Cd g/t	< 2	Ti g/t	1700
Co g/t	< 0.6	Tl g/t	0.5
Cr g/t	14	U g/t	5.3
Cu g/t	7.9	V g/t	3
Fe g/t	8600	Y g/t	7.5
K g/t	37000	Zn g/t	29

The analyses indicate that sulphides were mainly comprised of molybdenite and iron sulphides, in a ratio of approximately 1:6.



### 3. Bond Ball Mill Work Index Testing

The Bond ball mill grindability test is performed according to the original Bond procedure. The closing size of the BWI for this test was 150 mesh (106µm) with a product  $P_{80}$  of 127 µm. The BWI was determined to be 14.7 kWh/t for the Hurdal ore. This is considered to be a 'medium hardness' ore in the context of the SGS BWI database. A histogram of the relative hardness of the Hurdal ore is shown in Figure 1. Details on testing data and calculations can be found in Appendix B.

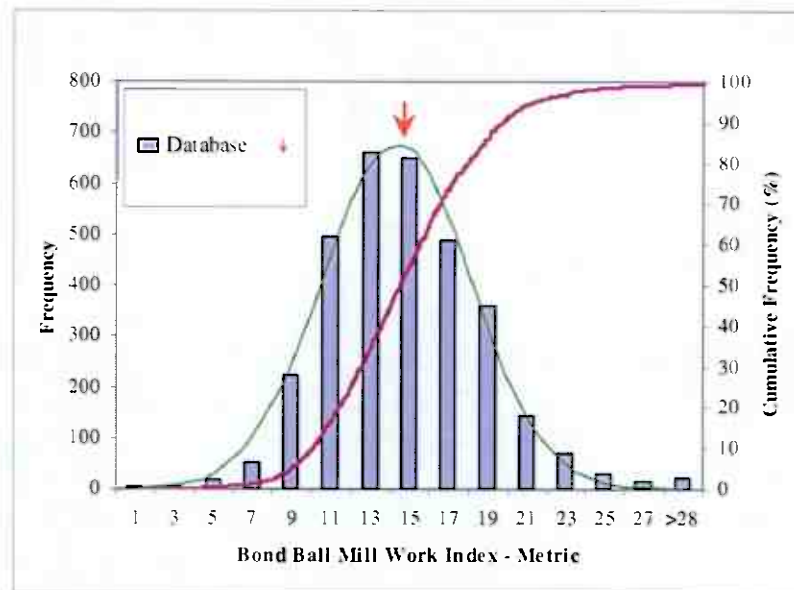


Figure 1. Hardness of the Hurdal Ore (Red Arrow) Relative to the SGS BWI Database

### 4. Metallurgical Testwork

The suite of tests discussed here serve as a 'scoping' test program to investigate the metallurgical response of Hurdal ore with flotation. An initial set of rougher tests were conducted to establish a basic rougher flowsheet and grind times for further testwork. Cleaner testwork was completed to assess upgrading potential of the ore to a saleable concentrate. In total, four rougher, and eight batch cleaner tests were completed.

#### 4.1. Rougher Metallurgy

Four rougher tests, F1-F4, were conducted, with the results presented in Table 2. The test sheets are provided in Appendix C. Commercial Diesel Fuel was used as the collector (the Diesel has been called “fuel oil” in this report). Pine oil was used as the frother. These tests were performed to establish an appropriate rougher flowsheet, as well as to establish an appropriate grind for optimal Mo recovery. Up to four incremental rougher concentrates were collected for each test, followed by a scavenger concentrate. The fuel oil was added to the primary grind because high attrition forces are required to adequately disperse the fuel oil over the mineral surfaces. Test F1 had a rougher time of 10 minutes, with an additional 4 minute scavenger stage.

The rougher Mo recovery was 86%, and with the scavenger concentrate, overall Mo recovery of the flowsheet was 88%. Results for F1 (Appendix C) indicated that the Mo grade of the third rougher concentrate was 0.36% Mo. The rougher scavenger concentrate assayed at 0.56% Mo. Collector was added in the scavenger stage, and ideally, the scavenger concentrate should assay at head grade (since in a plant process the scavenger concentrate will be recycled back into the roughers).

The significance of the Mo grade in the scavenger concentrate being both higher than the third rougher concentrate, and the head grade, is that either more collector or more residence time is required in the roughers. An increase in rougher time was implemented in tests F2-F4, with the inclusion of a 4 minute rougher stage. Tests F1 and F4 had the same primary grind and the inclusion of the additional 4 minute rougher stage increased Mo recovery by 1%. The scavenger time in F2-F4 was extended to 6 minutes. The total float time in tests F2-F4 increased to 20 minutes. Test F3 had the highest Mo recovery in the overall rougher concentrate at 91%, and improved to 92% with the scavenger.

Test F3 had the finest grind at 114  $\mu\text{m}$ , with a total fuel oil dosage of 80g/t. Test F2 had the same fuel oil dosage as F3, but had a coarser grind at 150  $\mu\text{m}$ . Mo recovery in F3 was 2% greater than F2. Mass pull to the rougher concentrate was highest in F3 at ~ 4%. The kinetic and grade-recovery data of the rougher kinetics tests are illustrated in Figures 1-4.

**Table 2. Test Summary of Initial Rougher Tests**

Test# / Flowsheet / Conditions	Product	Wt. (%)	Grade (%)		Distribution (%)	
			Mo	S	Mo	S
F1 P80 = 205 µm Diesel in Grind: 40 g/t Total Diesel = 55 g/t Pine Oil = 50 g/t Float time = 14 min	Mo Ro Conc 1	1.06	9.26	0.81	75.1	32.4
	Mo Ro Conc 1-2	1.81	6.14	1.45	85.0	38.4
	Mo Ro Conc 1-3	2.16	5.19	1.77	85.9	39.7
	Mo Ro Scav Conc + Ro Conc 1-3	2.65	4.33	2.20	88.1	41.1
	Ro Tls	97.3	0.016	0.14	11.9	58.9
	Head (Calc)		0.13	0.23		
F2 P80 = 194 µm Diesel in Grind: 60 g/t Total Diesel = 80 g/t Pine Oil = 50 g/t Float Time = 20 min	Mo Ro Conc 1	1.12	8.67	1.19	77.0	18.7
	Mo Ro Conc 1-2	2.09	5.25	2.38	86.9	22.7
	Mo Ro Conc 1-3	2.76	4.06	3.22	88.9	23.8
	Mo Ro Conc 1-4	3.15	3.58	3.70	89.5	24.1
	Mo Ro Scav Conc + Ro Conc 1-4	3.65	3.11	4.34	90.1	24.6
	Ro Tls	96.4	0.013	0.43	9.9	75.4
	Head (Calc)		0.13	0.55		
F3 P80 = 114 µm Diesel in Grind: 60 g/t Total Diesel = 80 g/t Pine Oil = 50 g/t Float Time = 20 min	Mo Ro Conc 1	1.81	4.99	2.47	70.0	21.6
	Mo Ro Conc 1-2	2.74	4.09	3.69	86.8	26.5
	Mo Ro Conc 1-3	3.24	3.60	4.38	90.3	27.6
	Mo Ro Conc 1-4	3.87	3.05	5.45	91.4	29.1
	Mo Ro Scav Conc + Ro Conc 1-4	4.33	2.74	6.19	91.9	29.7
	Ro Tls	95.7	0.011	0.42	8.1	70.3
	Head (Calc)		0.13	0.57		
F4 P80 = 202 µm Diesel in Grind: 40 g/t Total Diesel = 60 g/t Pine Oil = 50 g/t Float Time = 20 min	Mo Ro Conc 1	1.16	7.50	1.05	68.0	15.1
	Mo Ro Conc 1-2	1.83	5.58	1.78	80.0	19.0
	Mo Ro Conc 1-3	2.41	4.48	2.38	84.5	20.5
	Mo Ro Conc 1-4	2.77	4.02	2.78	87.0	21.4
	Mo Ro Scav Conc + Ro Conc 1-4	3.22	3.49	3.30	87.9	22.0
	Ro Tls	96.8	0.016	0.42	12.1	78.0
	Head (Calc)		0.13	0.52		

Figure 2 presents the grade-recovery curves of the rougher kinetics tests. It is evident that test F3 produced the highest recovery, but at the expense of grade. The grinds of tests F2 and F4 were coarser and thus likely had less Mo liberation than test F3. Figure 3 shows that for F3, Mo recovery to the first rougher concentrate is not as high as F1 or F2, even though Mo liberation should be better. It is possible that there was either more floatable gangue or slower flotation kinetics (due to finer grind) in F3. This may be compensated by the addition of more collector. Over the course of the test, F3 eventually recovers more Mo. The higher recovery appears to be also connected with a higher mass pull, as shown in Figure 3.

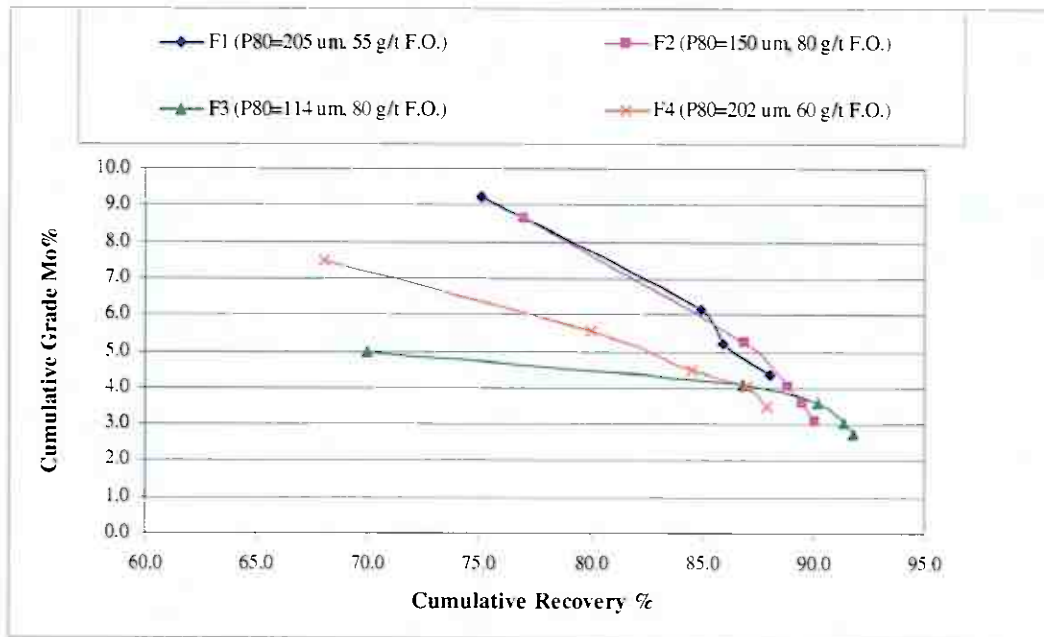


Figure 2. Mo Rougher Grade-Recovery Curves

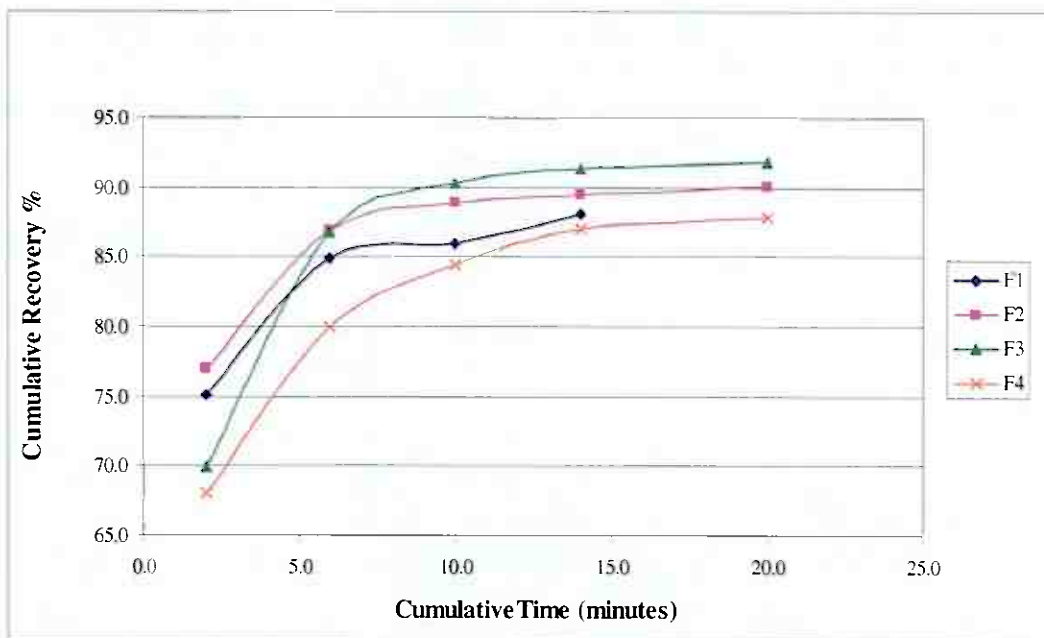
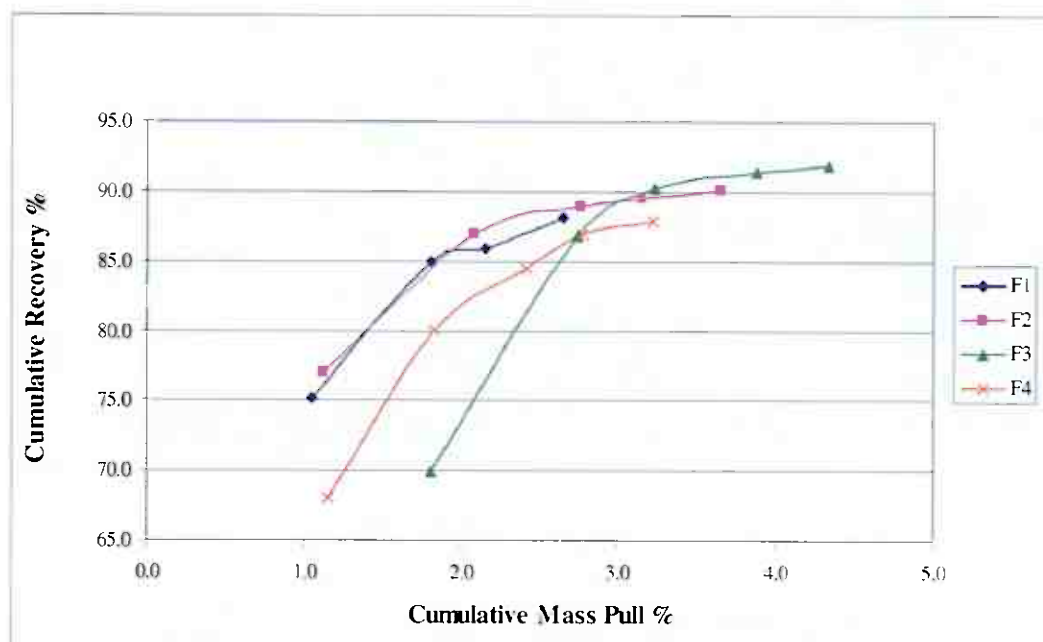


Figure 3. Mo Rougher Kinetics



**Figure 4. Rougher Recovery as Function of Mass Pull**

The results of the rougher kinetics tests can be summarized as follows:

- Molybdenum occurrence is likely bimodal. Fast floating, well liberated molybdenum floats in the first several minutes of the roughers followed by more poorly liberated molybdenum in the later rougher/scavenger stages.
- Rougher Mo recovery appears to be partially related to mass pull. The finer grind in test F3 also appears to have a positive impact on recovery. A grind time of 45 minutes for  $P_{80} = 114\mu\text{m}$ , 20 minutes flotation time, and total of 80 g/t fuel oil produced the best overall molybdenum rougher recovery of 92%.

#### 4.2. Cleaner Metallurgy

Eight cleaner tests, F5, F6, and F8-F13, were conducted to investigate various reagent and flowsheet alternatives for the production of a saleable molybdenum concentrate. A summary of these results is presented in Table 3. The test sheets are provided in Appendix D.

Tests F5 and F6 compared the effect of primary grind time on cleaner performance. Pine oil was used as the frother in these two tests. The rougher circuit targeted higher mass pull than the rougher tests. No regrind was applied to the rougher concentrate. Four cleaner stages were used. No depressants were added in the cleaner circuit. Both tests resulted in a concentrate with 85% molybdenum recovery, at a grade of 23% Mo. Molybdenum recovery to the final concentrate in F6 was also 85%, and graded 23%

Mo. The different primary grind times had no perceivable effect. Under a microscope, the gangue in the final concentrates appeared to consist of large liberated silicate particles and a small proportion of fine pyrite grains. With the large silicate particles reporting to the final concentrate, it was suspected that either the fuel oil dosage was too high or the pine oil frother was too aggressive.

**Table 3. Summary of Cleaner Test Results**

Test# / Flowchart / Conditions	Objective	Product	Wt. (%)	Grade (%)		Distribution (%)	
				Mo	S	Mo	S
F5 P <sub>80</sub> = 153 µm Diesel in Grind: 40 g/l Total Diesel = 40 g/l Pine Oil = 50 g/l Flint time = 14 min	Test cleaners with 35 mm primary grind.	Mo Cr 4 Conc	0.5	22.6	18.3	84.8	15.1
		Mo Cr 3 Conc	0.6	17.5	14.4	86.7	13.3
		Mo Cr 2 Conc	0.8	12.3	10.8	87.9	12.1
		Mo Cr 1 Conc	1.6	6.96	6.11	89.2	10.8
		Mo Ro Conc	6.9	1.76	8.03	90.9	9.1
		Ro Tls	93.1	0.012	0.47	9.15	78.6
		Head (Calc)		0.12	0.56		
F6 P <sub>80</sub> = 124 µm Diesel in Grind: 60 g/l Total Diesel = 40 g/l Pine Oil = 50 g/l Flint Time = 20 min	Test cleaners with 45 mm primary grind.	Mo Cr 4 Conc	0.5	22.6	20.4	84.9	15.1
		Mo Cr 3 Conc	0.6	18.3	17.0	86.5	13.5
		Mo Cr 2 Conc	0.8	13.3	12.7	87.7	12.3
		Mo Cr 1 Conc	1.6	6.70	6.79	89.1	10.9
		Mo Ro Conc	6.9	1.78	7.73	90.8	9.2
		Ro Tls	93.3	0.012	0.43	9.2	76.4
		Head (Calc)		0.12	0.52		
F8 Primary P80 = 119 µm Second Re-grind P80 = N/A Diesel in Grind: 40 g/l Total Diesel = 55 g/l NaCN = 90 g/l MBIC = 40 g/l CMB = 10 g/l	Lower diesel dosage and CMB in cleaners	Mo Cr 4 Conc	0.1	55.1	35.3	49.6	6.9
		Mo Cr 3 Conc	0.1	54.0	35.2	50.0	7.0
		Mo Cr 2 Conc	0.1	42.5	27.6	56.5	8.0
		Mo Cr 1 Conc	0.6	14.2	11.5	79.1	14.0
		Mo Cr 1 Conc + Cr 1 Scav. Conc.	0.9	10.0	8.43	88.2	10.2
		Mo Ro Conc	4.0	2.38	2.27	93.6	18.9
		Mo Ro Conc + Ro Scav. Conc.	5.0	1.93	1.90	93.0	19.5
F9 Primary P80 = 119 µm Second Re-grind P80 = 18 µm Diesel in Grind: 40 g/l Total Diesel = 55 g/l NaCN = 40 g/l MBIC = 42.5 g/l Na <sub>2</sub> O*SiO <sub>2</sub> = 1000 g/l	Lower diesel dosage Add Sodium Silicate (Na <sub>2</sub> O*SiO <sub>2</sub> ) in cleaners	Mo Cr 4 Conc	0.1	55.5	34.4	64.1	6.84
		Mo Cr 3 Conc	0.1	53.4	32.3	70.1	7.46
		Mo Cr 2 Conc	0.2	41.3	25.8	76.4	8.22
		Mo Cr 1 Conc	0.6	13.6	9.87	83.5	10.4
		Mo Cr 1 Conc + Cr 1 Scav. Conc.	0.8	11.1	7.71	88.6	10.7
		Mo Ro Conc	2.6	1.25	4.09	92.1	19.9
		Mo Ro Conc + Ro Scav. Conc.	3.4	2.75	3.51	92.4	20.3
F10 Primary P80 = 149 µm Second Re-grind P80 = 24 µm Diesel in Grind: 40 g/l NaCN = 40 g/l Line = 76 g/l Total Diesel = 55.5 g/l MBIC = 51.5 g/l Na <sub>2</sub> O*SiO <sub>2</sub> = 200 g/l	Staged primary grind Lower Sodium Silicate	Mo Cr 4 Conc	0.2	45.1	32.1	76.0	8.6
		Mo Cr 3 Conc	0.2	43.5	31.6	82.1	9.4
		Mo Cr 2 Conc	0.2	37.9	28.5	84.5	10.1
		Mo Cr 1 Conc	0.5	16.1	13.9	88.9	11.6
		Mo Cr 1 Conc + Cr 1 Scav. Conc.	0.7	12.6	10.4	90.7	12.0
		Mo Ro Conc	4.2	2.17	4.17	92.2	28.0
		Mo Ro Conc + Ro Scav. Conc.	5.0	1.84	3.50	92.7	28.6
F11 Primary P80 = 142 µm Second Re-grind P80 = 23 µm Diesel in Grind: 40 g/l Line = 90 g/l Total Diesel = 55.5 g/l MBIC = 51.5 g/l Na <sub>2</sub> O*SiO <sub>2</sub> = 200 g/l	Staged primary grind Lower Sodium Silicate No NaCN added	Mo Cr 4 Conc	0.1	45.2	30.5	72.6	7.3
		Mo Cr 3 Conc	0.2	43.4	30.1	76.2	7.3
		Mo Cr 2 Conc	0.2	33.3	27.6	78.9	8.03
		Mo Cr 1 Conc	0.4	21.1	15.3	82.8	8.7
		Mo Cr 1 Conc + Cr 1 Scav. Conc.	0.6	15.3	9.84	88.3	9.0
		Mo Ro Conc	3.9	2.24	3.92	90.7	25.1
		Mo Ro Conc + Ro Scav. Conc.	4.4	2.01	3.55	91.0	25.5
F12 Primary P80 = 134 µm Second Re-grind P80 = 23 µm Diesel in Grind: 40 g/l Line = 20 g/l NaCN = 200 g/l Total Diesel = 55.5 g/l MBIC = 50 g/l Na <sub>2</sub> O*SiO <sub>2</sub> = 1000 g/l	Staged primary grind Substitute NaCN for NaCN to depress pyrite 1000 g/l Sodium Silicate	Mo Cr 4 Conc	0.1	55.6	36.2	51.3	5.9
		Mo Cr 3 Conc	0.1	50.8	31.0	67.0	2.0
		Mo Cr 2 Conc	0.2	43.2	29.5	76.7	1.3
		Mo Cr 1 Conc	0.3	25.80	17.8	89.2	1.1
		Mo Cr 1 Conc + Cr 1 Scav. Conc.	0.6	15.71	10.7	88.3	0.3
		Mo Ro Conc	2.8	3.44	4.32	92.1	9.8
		Mo Ro Conc + Ro Scav. Conc.	3.7	2.61	3.36	92.5	0.6
F13 Primary P <sub>80</sub> = 148 µm Second Re-grind P <sub>80</sub> = 18 µm Diesel in Grind: 40 g/l NaCN = 90 g/l OPN = 25.5 g/l Total Diesel = 55 g/l MBIC = 55 g/l Na <sub>2</sub> O*SiO <sub>2</sub> = 800 g/l Line = 23 g/l	Staged primary grind Addition of second re-grind in cleaners	Mo Cr 4 Conc	0.1	56.6	37.0	77.6	10.0
		Mo Cr 3 Conc	0.2	45.5	29.8	80.6	10.7
		Mo Cr 2 Conc	0.2	44.4	30.5	82.9	11.2
		Mo Cr 1 Conc	0.2	39.8	28.6	83.7	11.6
		Mo Cr 1 Conc + Cr 1 Scav. Conc.	0.3	30.4	22.8	84.1	12.5
		Mo Cr 1 Conc + Cr 1 Scav. Conc.	0.6	14.4	12.5	88.4	15.2
		Mo Ro Conc	3.6	2.56	5.97	90.0	41.5
F14 Primary P <sub>80</sub> = 148 µm Second Re-grind P <sub>80</sub> = 18 µm Diesel in Grind: 40 g/l NaCN = 90 g/l OPN = 25.5 g/l Total Diesel = 55 g/l MBIC = 55 g/l Na <sub>2</sub> O*SiO <sub>2</sub> = 800 g/l Line = 23 g/l	Staged primary grind Addition of second re-grind in cleaners	Mo Ro Conc + Ro Scav. Conc.	4.2	2.13	5.14	93.5	41.9
		Mo Ro Tls	95.8	0.010	0.31	9.5	58.1
	Head (Calc)			0.10	0.51		

Another test, F7, was performed to generate a rougher concentrate which would then be used for QEMSCAN™ mineralogical characterization. Fuel oil dosage in the roughers was kept the same as F5 and F6, and MIBC was used as the frother to determine if it would minimize the recovery of liberated silicates in the froth. A mock cleaner test was performed on the rougher concentrate. Throughout the cleaner stages, each stage concentrate was examined under microscope to determine the visual degree of concentrate upgrading.

Large silicate particles were still present in the final concentrate. It was decided that the fuel oil dosage in the roughers should be lowered. Another issue identified in the cleaner tests was the presence of talc-like mineralization (phyllosilicates) in the first cleaner concentrate. This would have to be addressed in future tests by the addition of silicate dispersants. A regrind in the cleaners would be included in further tests with the aim of improving cleaner concentrate grades.

Tests F8 and F9 incorporated the new flowsheet and reagent changes. Both tests had a lower fuel oil dosage of 45 g/t in the roughers, and an 8 minute regrind on the first cleaner concentrate with lime and NaCN to depress pyrite. Silicate dispersants were added to the second cleaner stage in both tests, with 10 g/t CMC added in F8 and 1000g/t  $\text{Na}_2\text{SiO}_3$  added in F9. Concentrate upgrading was assessed visually under microscope throughout the tests. The final molybdenum concentrates appeared to be dominated by platy molybdenum clusters with no liberated silicates, and a very small fraction of finely dispersed pyrite grains. Test F8 final concentrate graded 55% Mo with a 50% molybdenum recovery. Test F9 final concentrate graded 56% Mo with a 64% molybdenum recovery. The lower molybdenum recovery in F8 is likely attributable to CMC, which has a tendency to depress molybdenum. This is evident in the second cleaner stage (where the CMC was added) which has 22% of the molybdenum reporting to the second cleaner tailings. The second cleaner tailings in F9 (with no CMC) only had 7% of the molybdenum reporting to it. The other change made to F8 and F9 was that the cleaner stage times were shortened, which also would have contributed in improving concentrate grades.

At this point in the testwork program, it was demonstrated that a saleable molybdenum concentrate could be produced from the ore. It was also noted that the combined concentrate  $P_{80}$  of test F9 was 18µm. With such a fine particle size in the first cleaner concentrate regrind product, it is possible that this resulted in lower stage recoveries of molybdenum in the cleaners. To address this issue, stage grinding of the rougher feed was implemented. Stage grinding in this case was comprised of a sequence of 5 minute grinds in the 10kg rod mill, in which the mill

product was wet screened over 65 mesh. The grind cycles continued until the plus 65 mesh weight distribution equated to that of the distributions in tests F8 and F9. After that, a rougher float was performed. A regrind was then applied to the rougher concentrates, rather than on the first cleaner concentrate. In F5 and F6, molybdenum loss to the 1<sup>st</sup> cleaner tailings was likely due to unliberated molybdenum in the form of middlings.

The objective of test F10 was to investigate the effectiveness of stage grinding on molybdenum recovery and to improve upon F8 and F9 (although at a saleable grade). Lime and NaCN were used to depress pyrite, and were adjusted as needed on a visual basis. Sodium silicate was added in the first cleaner at a lower dosage of 200 g/t which was just enough to disperse the talc-like minerals in the pulp (no silicates visible in froth). The final concentrate graded 45% Mo, with a 76% molybdenum recovery.

Test F11 investigated the use of lime only to depress pyrite, with slightly higher lime adjusted pH levels in the cleaners. The final concentrate graded at 48% Mo, with a 73% molybdenum recovery. The performance of tests F10 and F11 demonstrated improved molybdenum recovery, but did not attain a saleable concentrate grade.

Test F12 was conducted to investigate the use of NaHS as a substitute for NaCN in depressing pyrite. The NaHS was adjusted over the test based on examinations of froth sample under microscope. In addition to this, the Na<sub>2</sub>SiO<sub>3</sub> dosage was brought back up to 1000 g/t as in test F9. It was suspected that the lower Na<sub>2</sub>SiO<sub>3</sub> dosage in tests F10 and F11 had an impact on the final concentrate grades. The final concentrate of F12 graded 56% Mo with a 51% molybdenum recovery, which is closer the metallurgical performance of tests F8 and F9. This appeared to confirm the suspicion of Na<sub>2</sub>SiO<sub>3</sub> influence on metallurgical performance.

Test F13 was conducted by using only 200 g/t sodium silicate in the regrind on the rougher concentrate, and utilizing the conventional lime/NaCN scheme to depress pyrite. A fuel oil surfactant, OP6, was added in the primary grind at 25 g/t to investigate its effect on rougher Mo recovery. Rougher Mo recovery was 91%, showing no improvement over rougher recoveries in the other cleaner tests. A second regrind on the fourth cleaner concentrate was implemented with an additional 100 g/t sodium silicate. A final concentrate grade of 57% Mo with 78% recovery was achieved in F13. This was a 13% improvement in recovery over the next best test, F9. The first dosage of Na<sub>2</sub>SiO<sub>3</sub> was sufficient to disperse talc-like mineralization in the pulp without



depressing the molybdenite/silicate middlings. The molybdenum concentrate was successively cleaned through to the fourth cleaner stage, after which the second regrind liberated more molybdenum from the silicates. An additional 100g/t of  $\text{Na}_2\text{SiO}_3$  was added in the second regrind for further dispersion of liberated insolubles. The results of the cleaner tests are presented graphically in Figure 5. The open-circuit configuration for test F13 is presented in Figure 6.

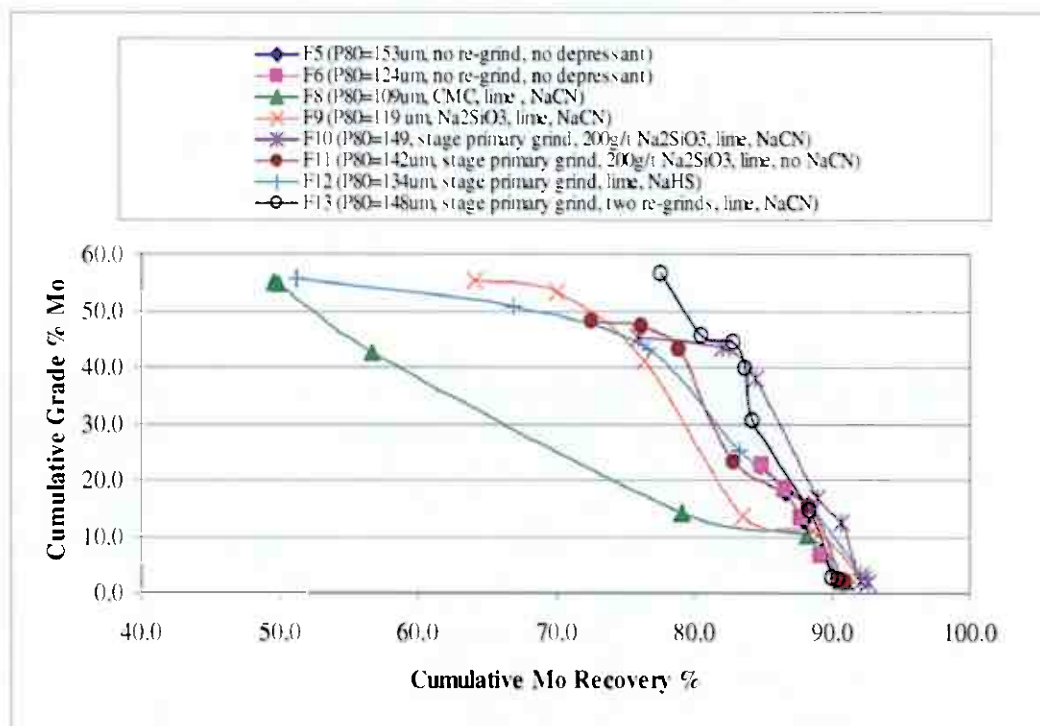


Figure 5. Mo Grade-Recovery Curves for Cleaner Tests

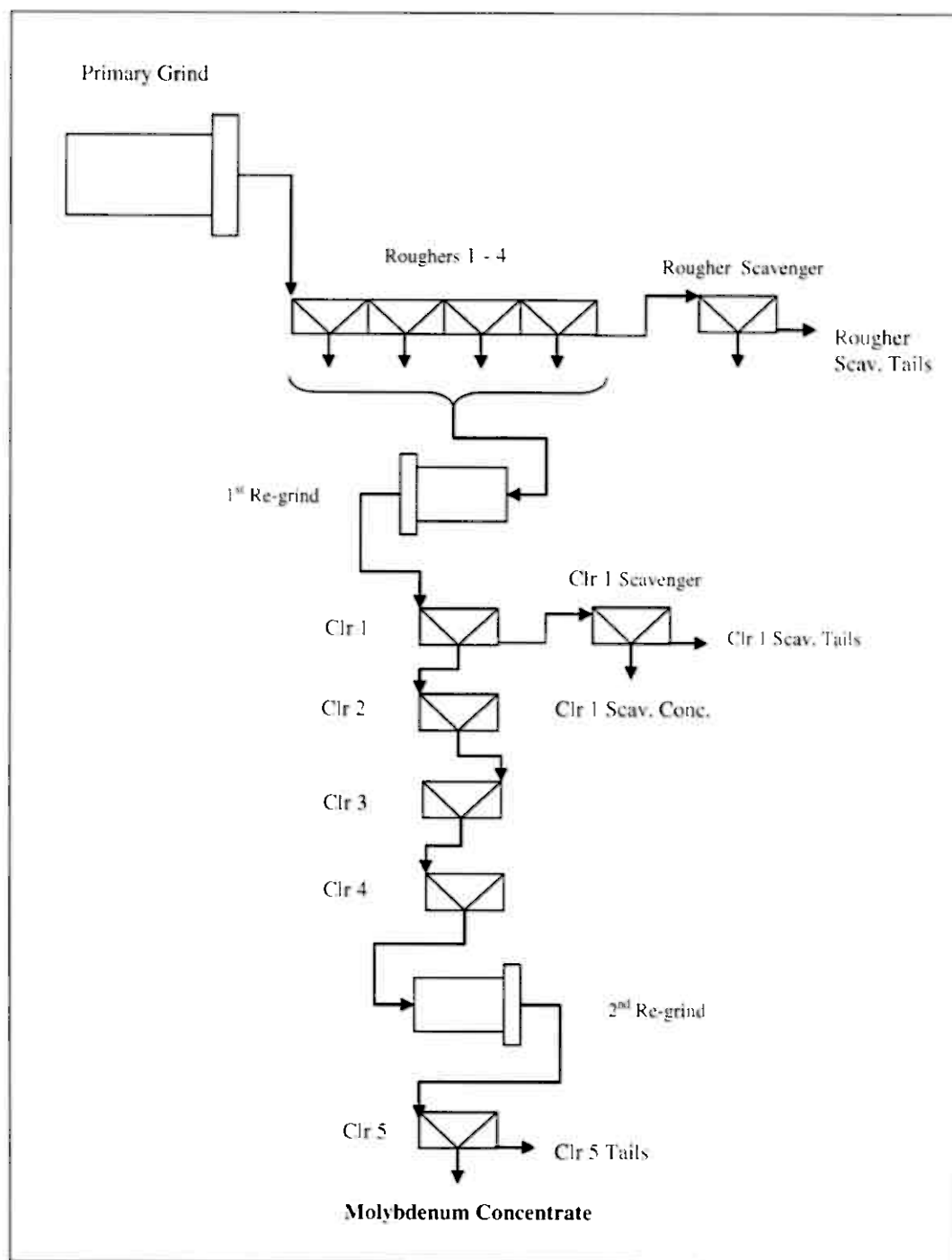


Figure 6. Open-Circuit Flowsheet of Cleaner Test F13

#### **4.3. Summary of Cleaner Results**

Poor final concentrate grades in tests F4 and F5 were attributable to a combination of too high a fuel oil dosage, and the use of pine oil as a frother. Subsequent testing used a lower fuel oil dosage of 45g/t of fuel oil in the roughers, and MIBC as a frother. Less free silicates were observed in the cleaner concentrate stages as a result.

Phyllosilicate dispersants are required to minimize phyllosilicates reporting to the froth. Sodium silicate is highly recommended for this purpose. It does not have as adverse an impact on molybdenum recovery as CMC.

It was observed that  $\text{Na}_2\text{SiO}_3$  dosage has an impact on molybdenum concentrate grade and recovery. As the  $\text{Na}_2\text{SiO}_3$  dosage increased, the concentrate grades increased, but at the expense of molybdenum recovery. This is likely due to the higher  $\text{Na}_2\text{SiO}_3$  dosages depressing molybdenum-silicate middlings which would otherwise report to the concentrate at much lower dosage.

At the low dosage of 200g/t  $\text{Na}_2\text{SiO}_3$  in the rougher concentrate regrind, in tests F10 and F11, final concentrate grades fell just short of 50% Mo.

When the  $\text{Na}_2\text{SiO}_3$  dosage was increased to 1000g/t in F12, final concentrate grade exceeded 50% Mo.

Due to the impact that  $\text{Na}_2\text{SiO}_3$  dosage has on Mo metallurgy, the effects of stage grinding and NaHS on Mo metallurgy, remain inconclusive.

The use of a fuel oil surfactant, OP6, did not improve molybdenum rougher recovery over that of earlier tests.

The addition of a second regrind in the cleaner circuit was demonstrated to improve concentrate grade, and significantly improve Mo recovery, with a  $\text{Na}_2\text{SiO}_3$  dosage of 300g/t.

Based on the results of test F13, it would be anticipated that in a locked cycle test, Mo recovery in a final concentrate would be in the range of 85-90%.

### **5. QEMSCAN Characterization**

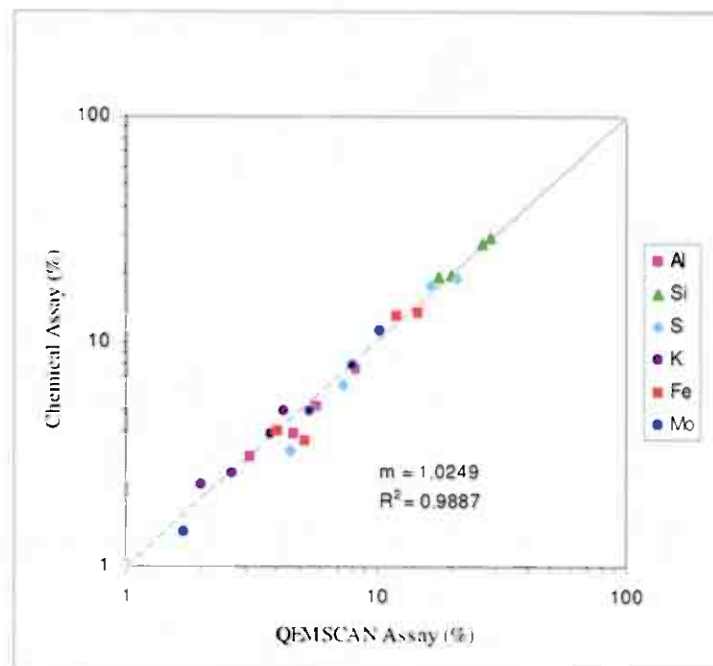
Mineralogical investigations were conducted on four size fractions (-300/+106 $\mu\text{m}$ , -106/+53 $\mu\text{m}$ , -53/+20 $\mu\text{m}$ , -20/+3 $\mu\text{m}$ ) of a rougher concentrate (test F7), using QEMSCAN<sup>TM</sup> (Quantitative Evaluation of Materials by Scanning Electron Microscopy) technology. A more detailed description of this process and its operating modes is provided in Appendix E.

Four graphite-impregnated 30mm polished sections were prepared, and the coarsest fraction was submitted for XRD analysis. Each size fraction was also submitted for chemical analysis. The polished sections were carbon coated and analysed using the QEMSCAN Particle Mapping Analysis (PMA) mode. PMA is a two-dimensional mapping analysis aimed at resolving liberation and locking characteristics of a generic set of particles. A pre-defined number of particles are mapped at a point spacing selected in order to spatially resolve and describe mineral textures and associations. The operating statistics for the PMA mode are given in Table 4.

**Table 4. Operating Statistics for PMA**

QEM Size Fraction	Weight (g)	Weight %	Sections No.	Pixel Size (µm)	Particle No.	Points No.
-300µm +106µm	50	16.5	1	5	2749	2852837
-106 µm +53 µm	22.2	7.3	1	4	5011	1582329
-53 µm +20 µm	19	6.3	1	2	5000	922188
-20µm -3µm	212	69.9	1	2	30059	267988
<b>Total</b>	<b>303.2</b>	<b>100</b>				

Key QEMSCAN™ mineralogical assays have been regressed with chemical assays and this is presented in Figure 7. The overall correlation, as measured by R-squared criteria, was 0.989. This is considered to be acceptable. Full QEMSCAN™ and direct chemical assays are presented in Appendix E.



**Figure 7. QEMSCAN and Direct Assay Reconciliation**

### 5.1. Modal Analysis and Grain Size Distribution

Bulk modal analysis results, presented in Appendix E, indicate mineral distributions in the rougher concentrate for each of the size fractions. The main value mineral in the rougher concentrate is molybdenite, which comprises 5.7% of the concentrate. Pyrite is the predominant sulphide gangue accounting for 10% of the concentrate. Other sulphide minerals account for 1.4% of the concentrate. Quartz, feldspars, and micas/phyllsilicates make up the bulk of the non-sulphide gangue (NSG). These three NSG minerals account for 78% of the rougher concentrate mass. The -106/+53  $\mu\text{m}$  fraction of the rougher concentrate contained the highest proportion of molybdenite, at 17% of the size fraction weight. This is shown in the graphs in Appendix E. An XRD scan was performed on the fraction, with the relative proportions of minerals classified into abundance categories of: major, moderate, minor, and trace. Table 5 lists the crystalline phase identification from the XRD analysis.

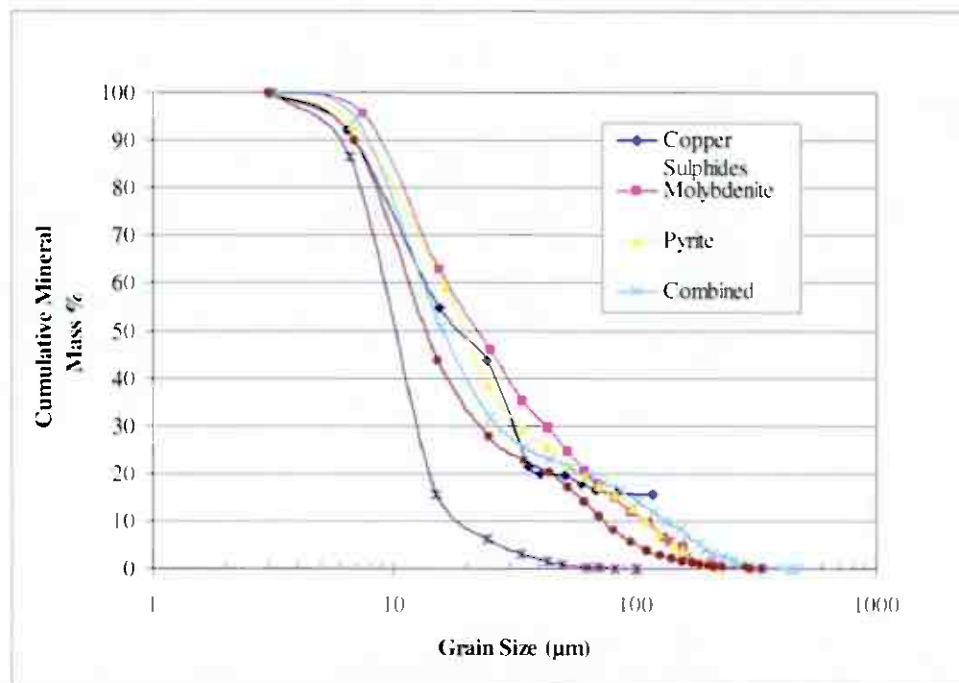
**Table 5. XRD Identification of Crystalline Phases in the -106/+53  $\mu\text{m}$  fraction**

Sample	Crystalline Mineral Assemblage (relative proportions based on peak height)			
	Major	Moderate	Minor	Trace
F7 Mo Conc -106/+53 $\mu\text{m}$	quartz	molybdenite plagioclase	potassium-feldspar pyrite	*dolomite, *mica *magnesite *pyroxene *pyrrhotite *tetrahedrite

\*Tentative identification due to low concentrations, diffraction line overlap, or poor crystallinity

The cumulative grain size distributions of molybdenite, pyrite, copper sulphides, and silicates are depicted in Figure 8. Molybdenite appears to be the coarsest mineral in the series with a  $P_{80}$  of approximately 60 $\mu\text{m}$ . The next coarsest mineral appears to be pyrite with a  $P_{80}$  between 55 and 60  $\mu\text{m}$ . Above 60  $\mu\text{m}$ , the size distributions of pyrite and molybdenite appear to overlap one another, implying that the two are closely associated with one another in this size range. This implication will be discussed in further detail in the liberation and association section of this text.

The finest mineral group in the series is the phyllosilicate group. This group consists of micas, chlorite, talc, serpentine, and clay minerals. Because of the fine size distribution of this mineral group, it may consist of a soft mineral such as talc. This assumption is strengthened by the appearance of talc-like mineralization of the froth in the cleaner tests.



**Figure 8. Average Grain Size Distribution of Minerals in Rougher Concentrate**

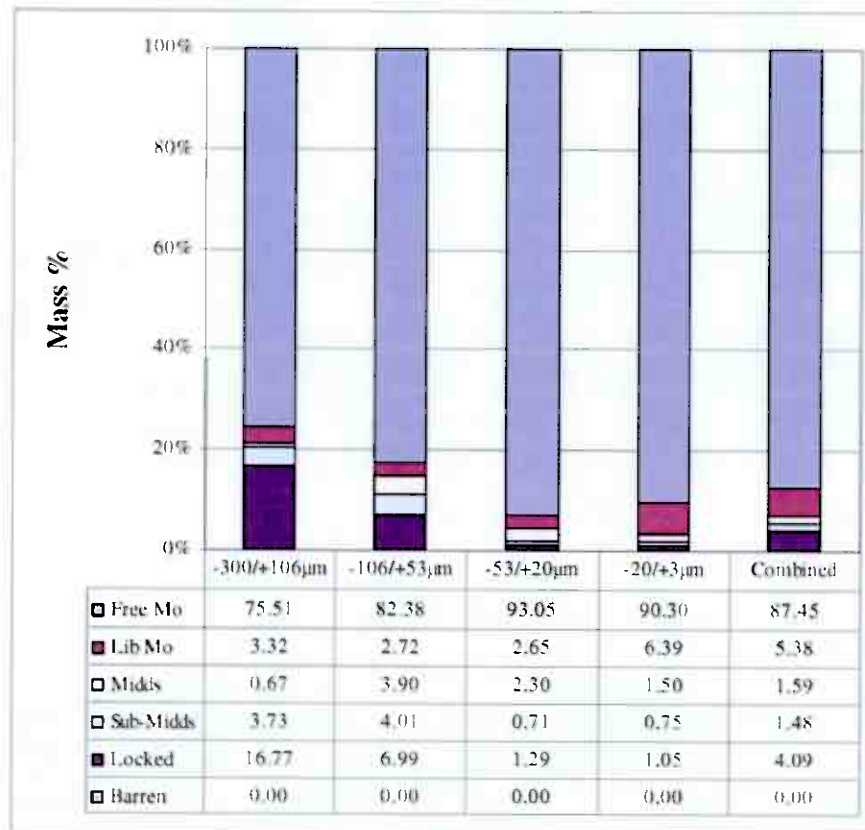
## 5.2. Mineral Liberation

For the purpose of this analysis, particle liberation is defined based on 2D particle area percent. Particles are classified into the following groups based on the mineral area percent (in the order of decreased % area liberation): free, liberated, sub-middling, middling, and locked. The criteria for these categories is listed in Table 6.

**Table 6. Criteria for Liberation Classification**

Free	Area % $\geq 95$
Liberated	Area % $< 95\%$ & $\geq 80\%$
Middlings	Area % $< 80\%$ & $\geq 50\%$
Sub-Middlings	Area % $< 50\%$ & $\geq 20\%$
Locked	Area % $< 20$

Combined and size-by-size distributions of molybdenite are presented in Figure 9. Molybdenum occurs as molybdenite throughout the entire sample.



**Figure 9. Rougher Concentrate Molybdenum Liberation Statistics**

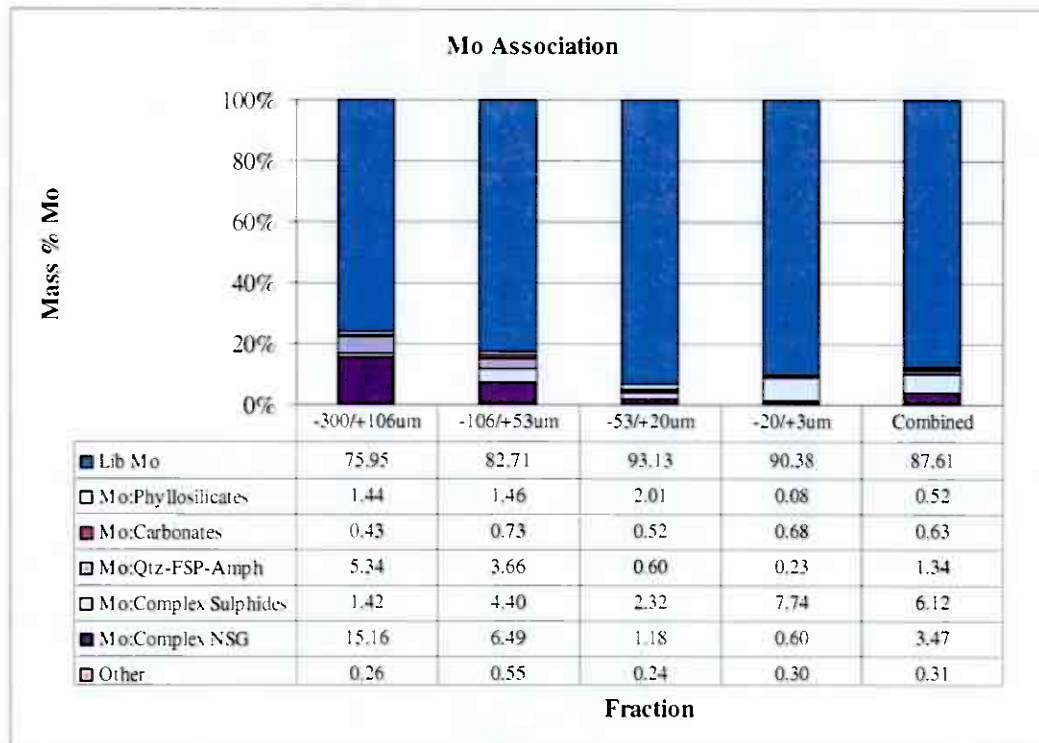
Free molybdenite for the global sample was 87%, with the highest proportion of free molybdenite occurring in the -53/+20µm fraction, at 93%. The highest proportion of locked molybdenite occurred in the -300/+106µm fraction at 17%, and correspondingly it had the lowest proportion of free molybdenite at 76%. A molybdenite liberation map is included in Appendix E.

### 5.3. Mineral Association

The chart for mineral associations with molybdenite is presented in Figure 10. In order to provide some clarification on some of the mineral groups, the Complex Sulphides category consists of complex combinations: pyrite, chalcopyrite, sphalerite, pyrrhotite and other copper sulphides. The Complex NSG category consists of complex combinations of: rutile, carbonates, micas/phyllsilicates, and quartz. Digital output of the mineral association textures is presented in Appendix E for more of a visual representation of the mineral associations found in the sample.



The mineral association analysis indicated that in the global sample, the largest association of locked molybdenite was with the complex sulphides group of minerals, at 6% of the sample weight. In the -300/+106 $\mu$ m fraction, the largest association with molybdenite was with complex NSG, at 15% of the sample weight. In the -20/+3 $\mu$ m fraction, the largest association of molybdenite was with the complex sulphides group, at almost 8% of the sample weight.



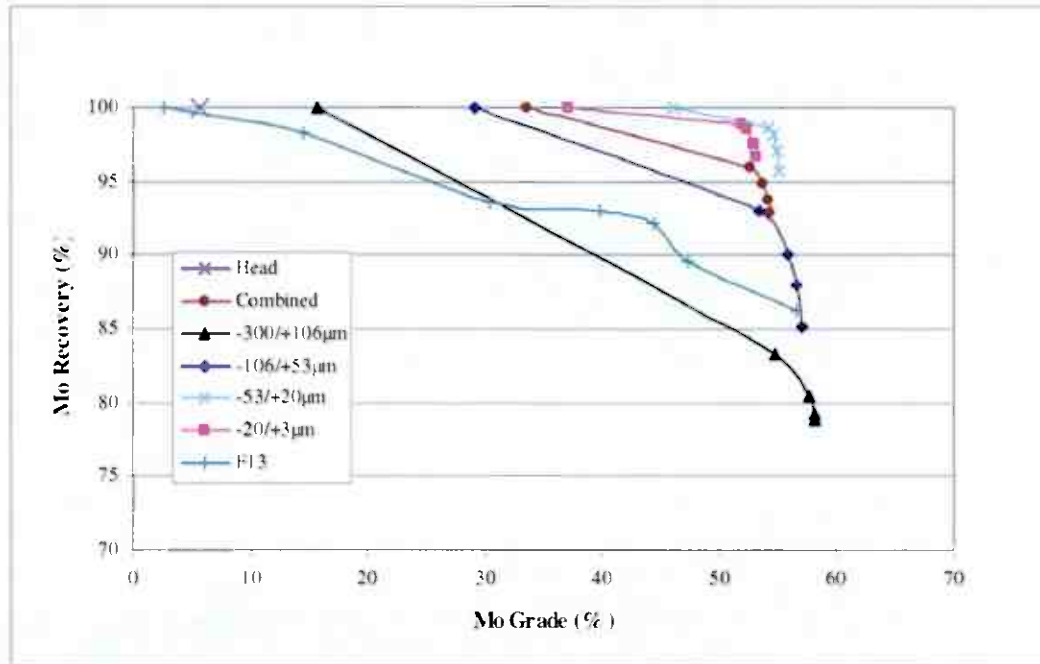
**Figure 10. Molybdenum Association Statistics**

#### 5.4. Determinative Mineralogy

Figure 11 illustrates the mineralogically limiting copper grade-recovery curves for the rougher concentrate sample. This analysis provides an indication of the maximum achievable molybdenum grade by recovery based on individual particle liberation and grade. These results, of course, do not reflect gangue activation and entrainment, or other factors that could occur in the actual metallurgical process. The plots in Figure 11 indicate that metallurgical performance improves (grade-recovery curves shift upward and to the right) in the finer fractions. The coarser the fractions become, the metallurgical response becomes more limited. This is due to the poor liberation of molybdenite. The combined size fraction plot in Figure 15 predicts that a final concentrate grade of 54% Mo with 93% recovery is



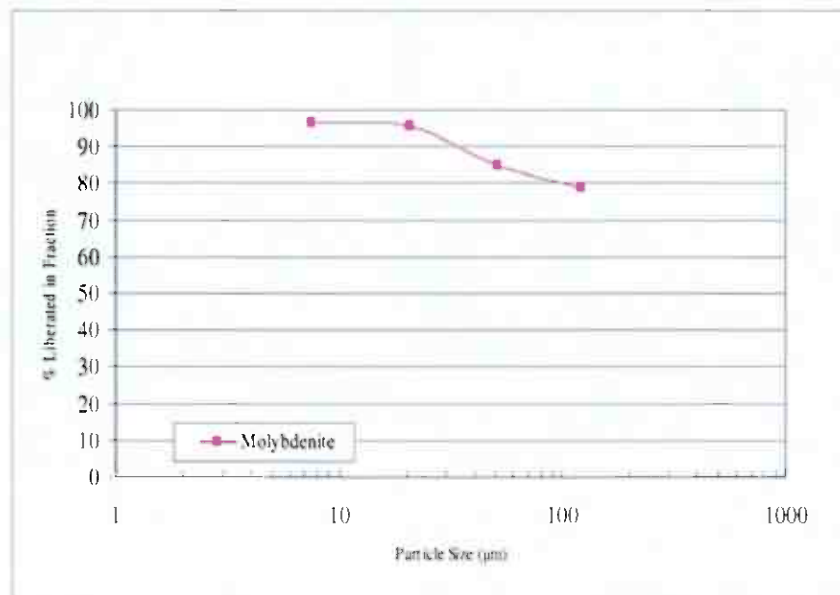
achievable with the Hurdal ore. Figure 11 also shows the metallurgical performance of test F13 relative to the theoretical curves.



**Figure 11. Theoretical Size-Limiting Grade-Recovery Curves**

The plot for F13 in Figure 11 has recoveries normalized to the Mo content of the rougher concentrate going into the cleaner circuit (i.e. F13 is expressed as a stage-recovery plot).

The theoretical mineral release curve for molybdenite in Figure 12 is essentially a re-iteration of the liberation data discussed earlier, presented in a different graphical format. The graph shows that molybdenite is already well liberated in the -300/+150 µm ( $P_{80} = 122\mu\text{m}$ ) at 79% Mo liberation. The minimum particle size for a regrind would appear to be at 20µm with 96% Mo liberation at this grind. In the cleaner tests, the reground rougher concentrates sized between  $P_{80} = 18\text{-}24\mu\text{m}$ .



**Figure 12. Theoretical Molybdenite Liberation Curve**

## 6. Conclusions and Recommendations

The conclusions that can be drawn from the testwork can be summarized as follows:

- Based on the mineralogical characterization of the ore and results of the metallurgical testwork, the Hurdal ore does not appear to be highly refractory in nature. Gangue minerals of significance were phyllosilicate minerals and pyrite. The phyllosilicate minerals were controlled with the addition of  $\text{Na}_2\text{SiO}_3$  dispersant. Pyrite was depressed by a combination of lime, higher pH, and NaCN depressant. Depending on reagent additions, saleable molybdenum concentrates can be produced with as few as 4 or 5 cleaning stages because of the nature of the ore.
- Sodium silicate dosage appeared to have the greatest influence on molybdenum cleaner circuit metallurgy. As dosage increased, concentrate grade improved, but with a much lower molybdenum recovery associated with it.
- The effect of stage grinding of the rougher flotation feed appeared to have no effect on molybdenum metallurgy.
- The addition of OP6 fuel oil surfactant appeared to have no effect on rougher molybdenum recovery.
- The effect of NaHS on depressing pyrite in one of the tests could not be determined, due to the masking effect of the high  $\text{Na}_2\text{SiO}_3$  dosage.
- The introduction of a second regrind in the cleaner circuit was beneficial in upgrading the molybdenum concentrate, without excessive use of sodium silicate. Molybdenum stage recovery was also significantly improved with this flowsheet option.

Recommendations for future work include:

1. Further tests should be conducted for flowsheet optimization. Using lime only in the cleaners, or use of NaHS as a substitute for NaCN, has the potential to produce a saleable molybdenum concentrate with further optimization.
2. A variability flotation study is an option to be considered to assess the metallurgical response of different zones of the Hurdal ore body.
3. A grindability study is recommended to determine grinding equipment requirements and variability in ore hardness.
4. A study on the environmental impact of flotation tailings material is also recommended.

## ***Appendix A – Drill Core Inventory List***

## Hurdal - Intervals for test work

## Crew cores

Drill hole	From	To	Sample no	MoS <sub>2</sub> %	Client Measured Weight (kg)	SGS Measured Weight (kg)
Dh 02	370	375	43313	0.157	6.7	6.7
Dh 02	385	390	43317	0.165	6.9	6.9
Dh 02	395	400	43320	0.180	7.6	7.6
Dh 02	410	415	43323	0.222	3.1	3.1
Dh 02	415	420	43325	0.248	6.8	6.8
Dh 02	430	435	43328	0.171	7.2	7.2
Dh 02	470	475	43336	0.317	7.6	7.7
Dh 02	635	640	43376	0.180	6.6	6.7
Dh 02	640	645	43377	0.181	7.1	7.2
Dh 02	655	660	43379	0.186	6.9	7.0
Dh 02	660	665	43380	0.225	7.2	7.3
Dh 02	755	760	43405	0.241	7.1	7.3
Dh 03	560	565	43433	0.293	6.9	7.0
Dh 03	580	585	43439	0.215	7.9	7.9
Dh 03	590	595	43441	0.159	7.5	7.6
Total					103.1	102.9

SGS weight includes bag weight

## Hydro cores

Drill hole	From	To	Sample no	MoS <sub>2</sub> %	Client Measured Weight (kg)	SGS Measured Weight (kg)
BH 7	330	335		0.180	4.5	4.5
BH 7	335	340		0.234	4.4	4.4
BH 7	340	345		0.351	4.4	4.4
BH 7	355	360		0.218	4.6	4.7
BH 7	360	365		0.231	4	4.1
BH 7	365	370		0.151	4.3	4.4
BH 7	370	375		0.168	4.5	4.6
BH 7	375	380		0.185	4.4	4.5
BH 7	390	395		0.223	4.1	4.3
BH 7	395	400		0.184	4.2	4.3
Total					43.4	44.2

SGS weight includes bag weight

## ***Appendix B – Bond Work Index Data and Calculations***

## SGS Minerals Services

## Standard Bond Ball Mill Grindability Test

Project No.: 11656-001    Product: Minus 6 Mesh    Date: Jan 29 2008

Sample.: Ore Drill Core

Purpose: To determine the ball mill grindability of the sample in terms of a Bond work index number.

Procedure: The equipment and procedure duplicate the Bond method for determining ball mill work indices.

Test Conditions: Mesh of grind: 100 mesh  
 Test feed weight (700 mL): 1230 grams  
 Equivalent to : 1757 kg/m<sup>3</sup> at Minus 6 mesh  
 Weight % of the undersize material in the ball mill feed: 13.0 %  
 Weight of undersize product for 250% circulating load: 351 grams

Results: Average for Last Three Stages = 1.75g.    247% Circulation load

## CALCULATION OF A BOND WORK INDEX

$$BW I = \frac{44.5}{P I^{0.23} \times G r p^{0.82} \times \left\{ \frac{10}{\sqrt{P}} - \frac{10}{\sqrt{F}} \right\}}$$

PI = 100% passing size of the product    150 microns  
 Grp = Grams per revolution    1.75 grams  
 P80 = 80% passing size of product    127 microns  
 F80 = 80% passing size of the feed    2039 microns

BW I = 13.4 (imperial)

BW I = 14.7 (metric)

## Grindability Test Data

Project No.: 11656-001

Test No.: Ore Drill Core

Stage No.	Revs	New Feed (grams)	Undersize		U'Size In Product (grams)	Undersize Product	
			In Feed (grams)	To Be Ground (grams)		Total (grams)	Per Mill Rev (grams)
1	100	1,230	159	192	299	140	1.40
2	224	299	39	313	363	324	1.45
3	210	363	47	304	377	330	1.57
4	193	377	49	303	381	332	1.72
5	176	381	49	302	351	302	1.71
6	179	351	45	306	361	316	1.76
7	173	361	47	305	351	304	1.76

Average for Last Three Stages = 354g.

1.75g.

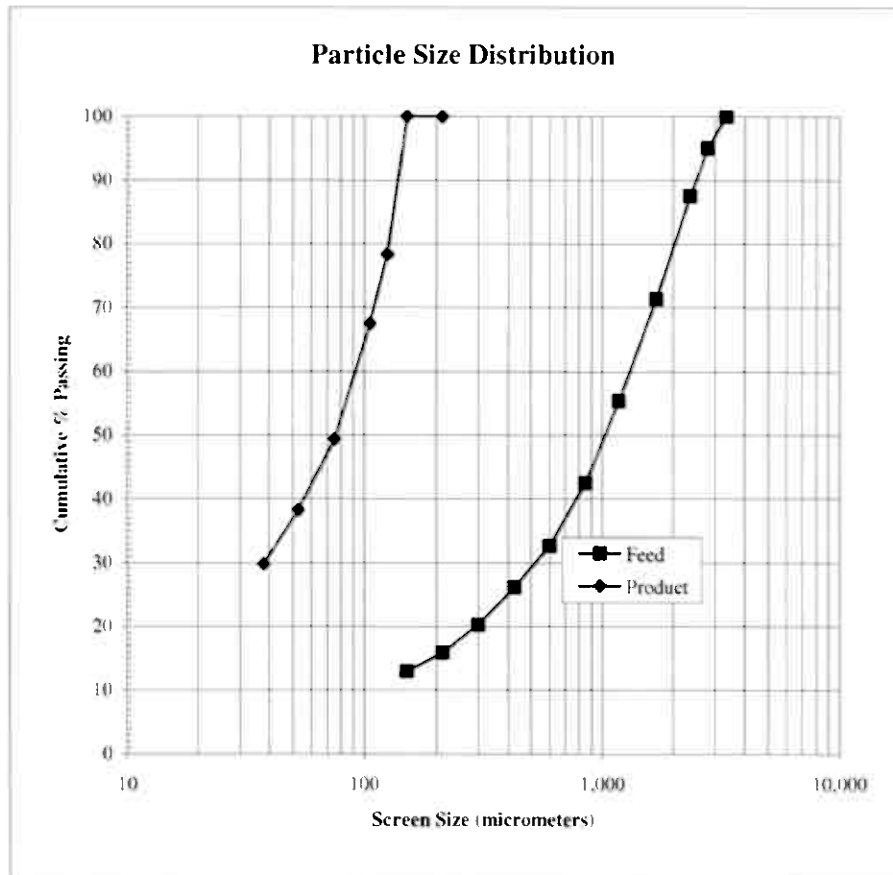
Feed K80						
Mesh	Size	Weight grams	% Retained		% Passing	
	µm		Individual	Cumulative	Cumulative	
6	3,360	0.0	0.0	0.0	100.0	
7	2,800	41.5	5.0	5.0	95.0	
8	2,360	61.6	7.5	12.5	87.5	
10	1,700	133.3	16.2	28.7	71.3	
14	1,180	131.3	15.9	44.6	55.4	
20	850	106.7	13.0	57.6	42.4	
28	600	80.3	9.7	67.3	32.7	
35	425	54.2	6.6	73.9	26.1	
48	300	48.2	5.9	79.8	20.2	
65	212	36.0	4.4	84.1	15.9	
100	150	24.0	2.9	87.0	13.0	
Pan	-150	106.7	13.0	100.0	0.0	
<b>Total</b>	-	<b>823.8</b>	<b>100.0</b>	-	-	
<b>K80</b>	<b>2,039</b>					

Product K80						
Mesh	Size	Weight grams	% Retained		% Passing	
	µm		Individual	Cumulative	Cumulative	
65	212	0.0	0.0	0.0	100.0	
100	150	0.0	0.0	0.0	100.0	
115	125	33.4	21.7	21.7	78.3	
150	106	16.7	10.8	32.5	67.5	
200	75	27.9	18.1	50.6	49.4	
270	53	17.1	11.1	61.7	38.3	
400	38	13.1	8.5	70.2	29.8	
Pan	-38	45.9	29.8	100.0	0.0	
<b>Total</b>	-	<b>154.1</b>	<b>100.0</b>	-	-	
<b>K80</b>	<b>127</b>					



Project No.: 11656-001

Test No.: Ore Drill Core



## **Appendix C – Rougher Kinetics Test Sheets**

Test No.: FI Project No.: 11656-001 Operator: PSM  
Date: Sept. 27/2007

Purpose: Initial Rougher Kinetics Scoping Test

Procedure: As outlined below.

Feed: 10kg of Hurdal ore composite

Grind: 25 minutes, Laboratory 10kg SS Rod Mill, 65 % solids.

Notes: - pull rate every 10 seconds over entire test  
- stopped test after 3 rougher stages as froth was barren

Stage	Reagents added, grams per tonne					Time, minutes			
	Diesel Fuel	Pine Oil				Grind	Cond.	Froth	pH
Grind	40					25			
Condition		50					1		Nat
Mo rougher 1								2	8.3
Mo rougher 2								4	
Mo rougher 3								4	
Mo Ro Scav	15						5	4	
Total	55	50					6	14	

Stage	Rougher 1-Scav
Flotation Cell	10 kg
Speed, rpm	50% setting

#### Metallurgical Balance

Product	Weight		Assays, %		% Distribution	
	g	%	Mo	S	Mo	S
Mo Ro Conc 1	105.8	1.1	9.26	7.09	75.1	32.4
Mo Ro Conc 2	74.7	0.7	1.72	1.87	9.9	6.0
Mo Ro Conc 3	35.6	0.4	0.36	0.82	1.0	1.3
Mo Ro Scav Conc	49.1	0.5	0.56	0.69	2.1	1.5
Ro Tls	9734.8	97.3	0.016	0.14	11.9	55.9
Head (calc.)	10000	100	0.13	0.23	100.0	100.0
(direct)			0.12	0.79		

#### Combined Products

Product	Weight		Assays, %		% Distribution	
	g	%	Mo	S	Mo	S
Mo Ro Conc 1	105.80	1.1	9.3	0.8	75.1	32.4
Mo Ro Conc 1-2	180.50	1.8	6.1	1.4	85.0	38.4
Mo Ro Conc 1-3	216.10	2.2	5.2	1.8	85.9	39.7
Mo Ro Scav Conc + Ro Conc 1-3	265.20	2.7	4.3	2.2	88.1	41.1

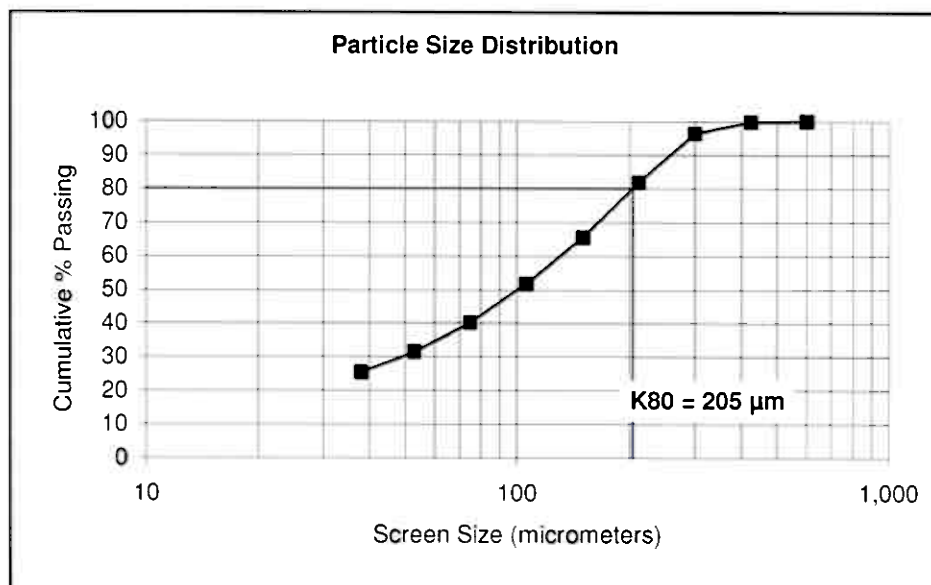
**SGS Minerals Services  
Size Distribution Analysis**

Project No.  
**11656-001**

Sample: **Ro Tls Sub**

Test No.: **F1**

Mesh	Size	Weight grams	% Retained		% Passing Cumulative
	µm		Individual	Cumulative	
28	600	0.0	0.0	0.0	100.0
35	425	0.3	0.2	0.2	99.8
48	300	6.8	3.5	3.6	96.4
65	212	28.7	14.6	18.2	81.8
100	150	32.1	16.3	34.5	65.5
150	106	27.1	13.8	48.3	51.7
200	75	22.9	11.6	59.9	40.1
270	53	17.0	8.6	68.5	31.5
400	38	12.2	6.2	74.7	25.3
Pan	-38	49.7	25.3	100.0	0.0
<b>Total</b>	-	<b>196.8</b>	100.0	-	-
<b>K80</b>	<b>205</b>				



Test No.:  
F2

Project No.: 11656-001

Operator: PSM  
Date: Oct.11/2007

Purpose: 2nd Rougher Kinetics Scoping Test

Procedure: As outlined below.

Feed: 10kg of Hurdal ore composite

Grind: 35 minutes, Laboratory 10kg SS Rod Mill, 65 % solids,

Notes: - pull rate every 10 seconds over entire test

Conditions:

K80 (grind): 150 (estimated)

Stage	Reagents added, grams per tonne				Time, minutes			
	Diesel Fuel	Pine Oil			Grind	Cond.	Froth	pH
Grind	60				35			
Condition		50				1		Nat
Mo rougher 1							2	8.3
Mo rougher 2							4	
Mo rougher 3							4	
Condition	10					5		
Mo rougher 4							4	
Mo Ro Scav	10					5	6	
Total	80	50				11	20	

Stage	Rougher 1-Scav
Flotation Cell	10 kg
Speed, rpm	50% setting

#### Metallurgical Balance

Product	Weight		Assays, %		% Distribution	
	g	%	Mo	S	Mo	S
Mo Ro Conc 1	112	1.1	8.67	9.18	77.0	18.7
Mo Ro Conc 2	96.8	1.0	1.29	2.29	9.9	4.0
Mo Ro Conc 3	67.4	0.7	0.37	0.82	2.0	1.0
Mo Ro Conc 4	38.5	0.4	0.19	0.53	0.6	0.4
Mo Ro Scav Conc	50.3	0.5	0.15	0.51	0.6	0.5
Ro Tls	9635	96.4	0.013	0.43	9.9	75.4
Head (calc.)	10000	100	0.13	0.55	100.0	100.0
(direct)			0.12	0.79		

#### Combined Products

Product	Weight		Assays, %		% Distribution	
	g	%	Mo	S	Mo	S
Mo Ro Conc 1	112.0	1.1	8.7	1.2	77.0	18.7
Mo Ro Conc 1-2	208.8	2.1	5.2	2.4	86.9	22.7
Mo Ro Conc 1-3	276.2	2.8	4.1	3.2	88.9	23.8
Mo Ro Conc 1-4	314.7	3.1	3.6	3.7	89.5	24.1
Mo Ro Scav Conc + Ro Conc 1-4	365.0	3.7	3.1	4.3	90.1	24.6

Test No.: **F3** Project No.: **11656-001** Operator: **PSM**  
Date: **Oct.11/2007**

**Purpose:** 3rd Rougher Kinetics: Scooping Test

**Procedure:** As outlined below.

**Feed:** 10kg of Hurdal ore composite

**Grind:** 45 minutes, Laboratory 10kg SS Rod Mill, 65 % solids,

**Notes:** - pull rate every 10 seconds over entire test

**Conditions:**

K80 (grind): 114

Stage	Reagents added, grams per tonne				Time, minutes			
	Diesel Fuel	Pine Oil			Grind	Cond.	Froth	pH
Grind	60				45			
Condition		50				1		Nat
Mo rougher 1							2	8.3
Mo rougher 2							4	
Mo rougher 3							4	
Condition	10					5		
Mo rougher 4							4	
Mo Ro Scav	10					5	6	
Total	80	50				11	20	

Stage	Rougher 1-Scav
Flotation Cell	10 kg
Speed, rpm	50% setting

#### Metallurgical Balance

Product	Weight		Assays, %		% Distribution	
	g	%	Mo	S	Mo	S
Mo Ro Conc 1	181.1	1.8	4.99	6.81	70.0	21.6
Mo Ro Conc 2	93	0.9	2.34	2.99	16.8	4.9
Mo Ro Conc 3	49.5	0.5	0.90	1.35	3.4	1.2
Mo Ro Conc 4	63.8	0.6	0.23	1.30	1.1	1.5
Mo Ro Scav Conc	45.9	0.5	0.13	0.75	0.5	0.6
Ro Tls	9566.7	95.7	0.011	0.42	8.1	70.3
Head (calc.)	10000	100	0.13	0.57	100.0	100.0
(direct)			0.12	0.79		

#### Combined Products

Product	Weight		Assays, %		% Distribution	
	g	%	Mo	S	Mo	S
Mo Ro Conc 1	181.1	1.8	5.0	2.5	70.0	21.6
Mo Ro Conc 1-2	274.1	2.7	4.1	3.7	86.8	26.5
Mo Ro Conc 1-3	323.6	3.2	3.6	4.4	90.3	27.6
Mo Ro Conc 1-4	387.4	3.9	3.0	5.5	91.4	29.1
Mo Ro Scav Conc + Ro Conc 1-4	433.3	4.3	2.7	6.2	91.9	29.7

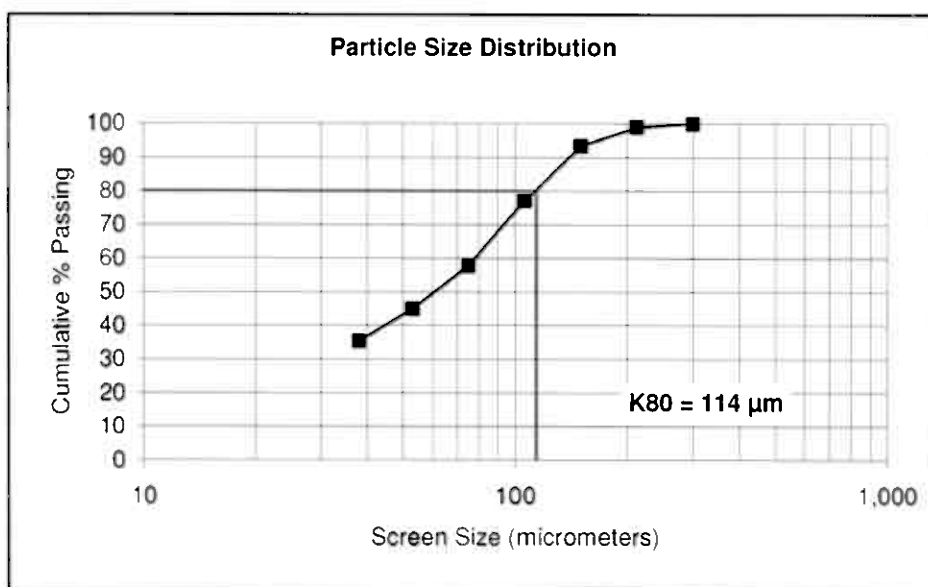
**SGS Minerals Services  
Size Distribution Analysis**

Project No.  
**11656-001**

Sample: **Ro Sc Tails**

Test No.: **F3**

Mesh	Size	Weight grams	% Retained		% Passing Cumulative
	µm		Individual	Cumulative	
48	300	0.2	0.1	0.1	99.9
65	212	1.5	1.0	1.1	98.9
100	150	8.4	5.6	6.7	93.3
150	106	24.5	16.3	23.0	77.0
200	75	29.1	19.3	42.3	57.7
270	53	19.3	12.8	55.1	44.9
400	38	14.4	9.6	64.7	35.3
Pan	-38	53.2	35.3	100.0	0.0
<b>Total</b>	-	<b>150.6</b>	<b>100.0</b>	-	-
<b>K80</b>	<b>114</b>				



Test No.:  
F4

Project No.: 11656-001

Operator: PSM  
Date: Oct.11/2007

Purpose: 4th Rougher Kinetics Scoping Test

Procedure: As outlined below.

Feed: 10kg of Hurdal ore composite

Grind: 25 minutes, Laboratory 10kg SS Rod Mill, 65 % solids,

Notes: - pull rate every 10 seconds over entire test

Conditions:

K80 (grind): 202 um

Stage	Reagents added, grams per tonne				Time, minutes			
	Diesel Fuel	Pine Oil			Grind	Cond.	Froth	pH
Grind	40				25			
Condition		50				1		Nat
Mo rougher 1							2	8.3
Mo rougher 2							4	
Mo rougher 3							4	
Condition	10					5		
Mo rougher 4							4	
Mo Ro Scav	10					5	6	
Total	60	50				11	20	

Stage	Rougher 1-Scav
Flotation Cell	10 kg
Speed, rpm	50% setting

#### Metallurgical Balance

Product	Weight		Assays, %		% Distribution	
	g	%	Mo	S	Mo	S
Mo Ro Conc 1	115.9	1.2	7.5	6.81	68.0	15.1
Mo Ro Conc 2	67.5	0.7	2.28	2.99	12.0	3.9
Mo Ro Conc 3	57.5	0.6	0.99	1.35	4.5	1.5
Mo Ro Conc 4	36.0	0.4	0.89	1.30	2.5	0.9
Mo Ro Scav Conc	45.2	0.5	0.25	0.75	0.9	0.7
Ro Tls	9677.9	96.8	0.016	0.42	12.1	78.0
Head (calc.)	10000	100	0.13	0.52	100.0	100.0
(direct)			0.12	0.79		

#### Combined Products

Product	Weight		Assays, %		% Distribution	
	g	%	Mo	S	Mo	S
Mo Ro Conc 1	115.9	1.2	7.5	1.1	68.0	15.1
Mo Ro Conc 1-2	183.4	1.8	5.6	1.8	80.0	19.0
Mo Ro Conc 1-3	240.9	2.4	4.5	2.4	84.5	20.5
Mo Ro Conc 1-4	276.9	2.8	4.0	2.8	87.0	21.4
Mo Ro Scav Conc + Ro Conc 1-4	322.1	3.2	3.5	3.3	87.9	22.0

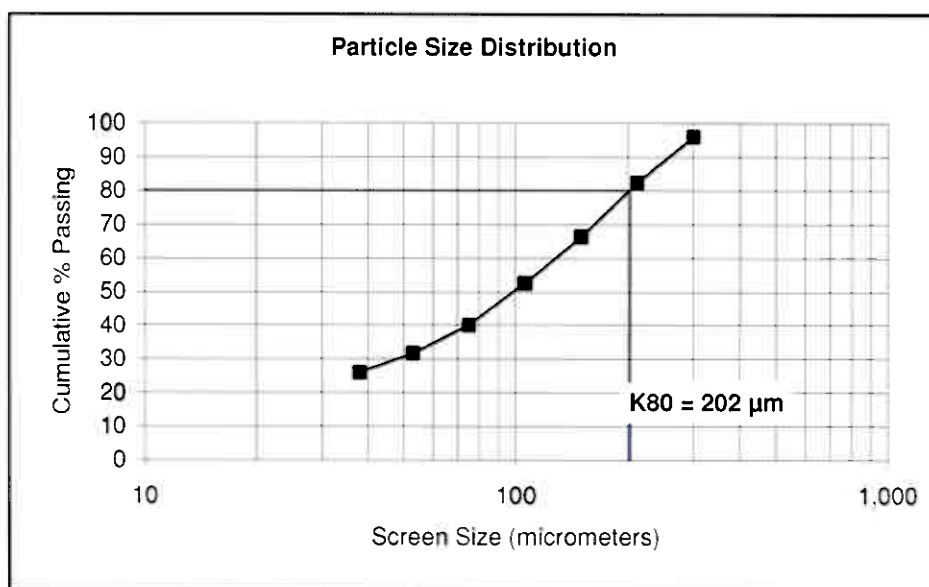


**SGS Minerals Services  
Size Distribution Analysis**

Project No.

**11656-001**Sample: **Ro Sc Tails**Test No.: **F4**

Mesh	Size	Weight grams	% Retained		% Passing Cumulative
	µm		Individual	Cumulative	
48	300	6.1	4.1	4.1	95.9
65	212	20.4	13.6	17.6	82.4
100	150	24.1	16.0	33.7	66.3
150	106	20.7	13.8	47.5	52.5
200	75	18.8	12.5	60.0	40.0
270	53	12.6	8.4	68.4	31.6
400	38	8.4	5.6	74.0	26.0
Pan	-38	39.1	26.0	100.0	0.0
<b>Total</b>	<b>-</b>	<b>150.2</b>	<b>100.0</b>	<b>-</b>	<b>-</b>
<b>K80</b>	<b>202</b>				



## ***Appendix D – Batch Cleaner Test Sheets***

Test No.:  
F5

Project No.: 11656-001

Operator: PSM  
Date: Nov. 19/2007

Purpose: 1st cleaner test using 1/2 rougher conditions

Procedure: As outlined below.

Feed: 10kg of Hurdal ore composite

Grind: 35 minutes, Laboratory 10kg SS Rod Mill, 65 % solids.

Notes:  
- pull rate every 10 seconds over entire test  
- 10 kg float machine has new impeller  
- Used machine #6 for cleaners

#### Conditions:

KSD (grind): 153

Stage	Reagents added, grams per tonne				Time, minutes			pH	Redox
	Diesel Fuel	Pine Oil			Grind	Cond.	Froth		
Grind	60				35				
Condition		50				1		Nat	
Mo rougher 1							2	9.5	
Mo rougher 2							4	9.3	
Mo rougher 3							4	9.6	
Condition	10					5			
Mo rougher 4							4	9.0	
Mo Ro Scav	10					5	6	8.3	
Cleaners									
		as needed							
Cleaner1		--					13	8.1	180
Cleaner2		--					10	8.0	180
Cleaner3		--					8	7.8	150
Cleaner4		--					6	7.7	120
Total	80	50					57		

Stage	Rougher 1-Scav	Cleaner1	Cleaner2	Cleaner 3-4
Flotation Cell	10 kg	D1 - 1000g	D1 - 500 g	D1 - 250g
Speed, rpm	50% setting	1800	1500	1200

#### Metallurgical Balance

Product	Weight		Assays, Gt		% Distribution	
	g	%	Mo	S	Mo	S
Mo Clr 4 Conc	45.8	0.5	22.6	18.3	84.8	15.1
Mo Clr 4 Tls	14.2	0.1	1.64	1.85	1.9	0.5
Mo Clr 3 Tls	23.3	0.2	0.65	1.45	1.2	0.6
Mo Clr 2 Tls	73.1	0.7	0.21	0.79	1.3	1.0
Mo Clr 1 Tls	536.4	5.4	0.038	0.44	1.7	4.2
Mo Ro Tls	9307.2	93.1	0.012	0.47	9.1	78.6
Head (calc.)	10000	100	0.12	0.56	100.0	100.0
(direct)			0.12	0.79		

#### Combined Products

Product	Weight		Assays, Gt		% Distribution	
	g	%	Mo	S	Mo	S
Mo Clr 4 Conc	45.8	0.5	22.6	18.3	84.8	15.1
Mo Clr 3 Conc	60.0	0.6	17.6	14.4	86.7	15.5
Mo Clr 2 Conc	83.3	0.8	12.9	10.8	87.9	16.1
Mo Clr 1 Conc	156.4	1.6	7.0	6.1	89.2	17.2
Mo Ro Conc	692.8	6.9	1.8	8.0	90.9	21.4

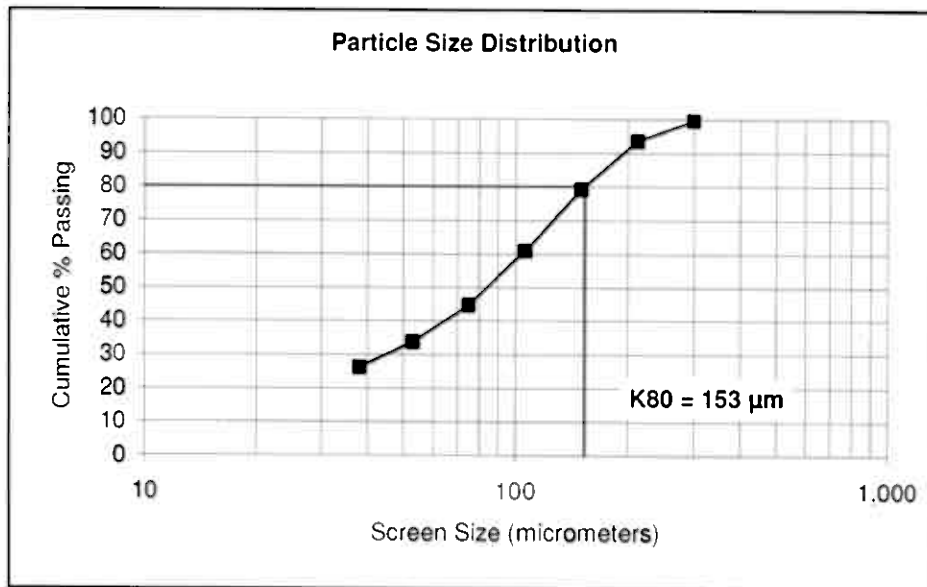
**SGS Minerals Services**  
**Size Distribution Analysis**

Project No.  
**11656-001**

Sample: **Ro TI Sub**

Test No.: **F5**

Mesh	Size	Weight grams	% Retained		% Passing Cumulative
	µm		Individual	Cumulative	
48	300	0.7	0.4	0.4	99.6
65	212	8.9	6.0	6.5	93.5
100	150	21.1	14.3	20.8	79.2
150	106	26.8	18.3	39.1	60.9
200	75	23.9	16.3	55.4	44.6
270	53	15.9	10.9	66.3	33.7
400	38	11.1	7.6	73.8	26.2
Pan	-38	38.4	26.2	100.0	0.0
<b>Total</b>	-	<b>146.7</b>	<b>100.0</b>	-	-
<b>K80</b>	<b>153</b>				



Test No.:  
F6

Project No.: 11656-001

Operator: PSM  
Date: Nov.19/2007

Purpose: 2nd cleaner test using F3 rougher conditions

Procedure: As outlined below.

Feed: 10kg of Hurdal ore composite

Grind: 45 minutes, Laboratory 10kg SS Rod Mill, 65 % solids.

Notes:  
- Rougher pull rate every 10 seconds  
- Weight of rod mill charge may have changed based on grind K50  
- Used machine #6 for cleaners  
- 10 kg float machine has new impeller

Stage	Reagents added, grams per tonne				Time, minutes			pH	Redox
	Diesel Fuel	Pine Oil			Grind	Cond.	Froth		
Grind	60				45				
Roughers									
Condition		50				1		Nat	
Mo rougher 1							2	8.3	
Mo rougher 2							4		
Mo rougher 3							4		
Condition	10					5			
Mo rougher 4							4		
Mo Ro Scav	10					5	6		
Cleaners									
Condition									
Cleaner1		as needed					13	8.2	180
Cleaner2							13	8.0	180
Cleaner3							8	8.0	150
Cleaner4							6	7.9	100
Total	20						60		

Stage	Rougher 1-Scav	Cleaner1	Cleaner2	Cleaner 3-4
Flotation Cell	10 kg	D1 - 1000g	D1 - 500 g	D1 - 250g
Speed, rpm	50% setting	1800	1500	1200

#### Metallurgical Balance

Product	Weight		Assays, %		% Distribution	
	g	%	Mo	S	Mo	S
Mo Ctr 4 Conc	45.5	0.5	22.6	20.4	84.9	17.7
Mo Ctr 4 Tls	11.6	0.1	1.64	3.85	1.6	0.9
Mo Ctr 3 Tls	22.5	0.2	0.65	1.76	1.2	0.5
Mo Ctr 2 Tls	81.4	0.8	0.21	0.91	1.4	1.4
Mo Ctr 1 Tls	517.5	5.2	0.038	0.29	1.6	2.9
Mo Ro Tls	9321.2	93.2	0.012	0.43	9.2	26.4
Head (calc.)	10000	100.0	0.12	0.52	100.0	100.0
(direct)			0.12	0.79		

#### Combined Products

Product	Weight		Assays, %		% Distribution	
	g	%	Mo	S	Mo	S
Mo Ctr 4 Conc	45.5	0.5	22.6	20.4	84.9	17.7
Mo Ctr 3 Conc	57.1	0.6	18.3	17.0	55.5	18.5
Mo Ctr 2 Conc	79.6	0.8	13.3	12.7	87.7	19.3
Mo Ctr 1 Conc	161.0	1.6	6.70	6.75	89.1	20.7
Mo Ro Conc	678.8	6.5	1.78	7.73	90.8	23.6

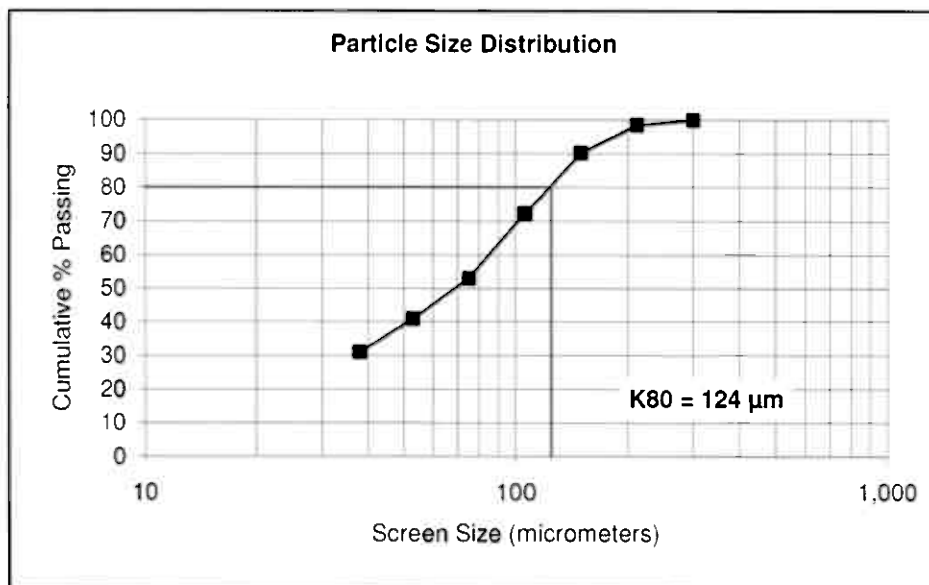
**SGS Minerals Services**  
**Size Distribution Analysis**

Project No.  
**11656-001**

Sample: **Ro TI Sub**

Test No.: **F6**

Mesh	Size	Weight grams	% Retained		% Passing Cumulative
	µm		Individual	Cumulative	
48	300	0.1	0.1	0.1	99.9
65	212	2.2	1.5	1.6	98.4
100	150	12.3	8.3	9.8	90.2
150	106	26.8	18.0	27.8	72.2
200	75	28.6	19.3	47.1	52.9
270	53	17.8	12.0	59.1	40.9
400	38	15.0	10.1	69.2	30.8
Pan	-38	45.8	30.8	100.0	0.0
<b>Total</b>	-	<b>148.6</b>	100.0	-	-
<b>K80</b>	<b>124</b>				



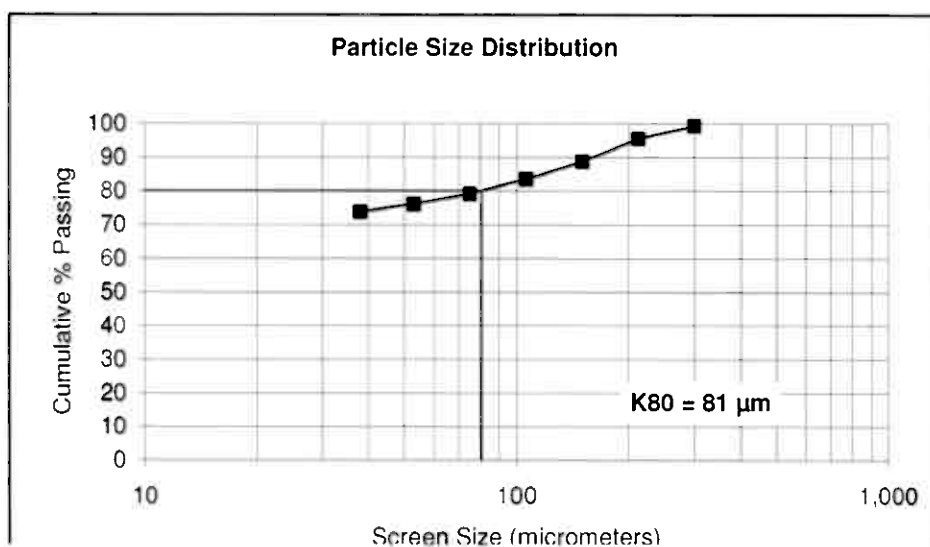
**SGS Minerals Services  
Size Distribution Analysis**

Project No.  
**11656-001**

Sample: **Ro Con**

Test No.: **F7**

Mesh	Size	Weight grams	% Retained		% Passing Cumulative
	µm		Individual	Cumulative	
48	300	2.1	0.7	0.7	99.3
65	212	11.6	3.8	4.5	95.5
100	150	20.5	6.8	11.3	88.7
150	106	15.8	5.2	16.5	83.5
200	75	13.3	4.4	20.9	79.1
270	53	8.9	2.9	23.8	76.2
400	38	7.3	2.4	26.2	73.8
Pan	-38	223.7	73.8	100.0	0.0
<b>Total</b>	-	<b>303.3</b>	100.0	-	-
<b>K80</b>	<b>81</b>				



Test No.: **FB** Project No.: **11656-001** Operator: **PSM**  
Date: **Dec. 5/2007**

**Purpose:** Cleaner test to observe effect of less fuel oil in roughers, re-grind on 1st Cleaner concentrate, and addition of cyanide and lime to depress pyrite.  
Achieve grade of 50% Mo in 4th cleaner concentrate.  
CMC added in Clr 2 to depress talc.

**Procedures:** As outlined below.

**Feed:** 10kg of Hurdal ore composite

**Grind:** 45 minutes, Laboratory 10kg SS Rod Mill, 65 % solids.  
8 minutes re-grind in pebble mill

**Notes:** - Rougher pull rate every 10 seconds in Ro 1-3 **K80 (grind): 109**  
- Pull rate in Ro 4,5 every 15 seconds **K80 (re-grind): N/A**

**Conditions:**

Stage	Reagents added, grams per tonne					Time, minutes			pH	Redox
	Diesel Fuel	MIBC	NaCN	Lime	CMC	Grind	Cond.	Froth		
Grind	40					45				
Roughers										
Condition		50					1		Nat	
Mo Rougher 1								2	8.3	
Mo Rougher 2								4		
Mo Rougher 3								4		
Condition	2.5						5			
Mo Rougher 4								5		
Condition	2.5						5			
Mo rougher 5								5		
Condition										
Mo Ro Scav (See Conc 1)	10						5	6		
Cleaners										
Ro Conc 1-3										
Condition										
		as needed								
Cleaner1								4	8.21	
Cleaner1 Scav								6	8.09	
Re-grind Clr 1 Conc			20	100		8			11.55	-100
Cleaner2	2	2.5	10		10			4	10.14	-90
Cleaner3			10					3	9.71	-85
Cleaner4	0.5		10					2	9.70	-80
Total	17.5	52.5	50	100	10			45		

Stage	Rougher 1-Scav	Cleaner1	Cleaner2	Cleaner 3-4
Flotation Cell	10 kg	D1 - 1000g	D1 - 500g	D1 - 250g
Speed, rpm	50% setting	1800	1500	1200

**Metallurgical Balance**

Product	Weight		Assays, %		% Distribution	
	g	%	Mo	S	Mo	S
Mo Clr 4 Conc	9.5	0.1	55.1	35.3	49.6	6.9
Mo Clr 4 Tls	0.1	0.001	38.1	23.2	0.4	0.05
Mo Clr 3 Tls	4.5	0.045	16.0	11.4	6.8	1.1
Mo Clr 2 Tls	44.9	0.4	5.3	6.41	22.4	5.9
Mo Clr 1 Scav Conc	33.8	0.3	2.83	3.13	9.1	2.2
Mo Clr 1 Scav Tls	309.0	3.1	0.083	0.42	2.4	2.7
Mo Ro Scav Conc	95.0	1.0	0.040	0.33	0.4	0.6
Mo Ro Tls	9503.2	95.0	0.010	0.410	9.0	89.5
Head (calc.)	10000	100.0	0.11	0.48	100.0	100.0
(direct)			0.12	0.79		

**Note:** Insufficient sample for Cleaner 4 tailings, used assays from F9 as approximations

**Combined Products**

Product	Weight		Assays, %		% Distribution	
	g	%	Mo	S	Mo	S
Mo Clr 4 Conc	9.5	0.1	55.1	35.3	49.6	6.9
Mo Clr 3 Conc	9.6	0.1	54.9	35.2	50.0	7.0
Mo Clr 2 Conc	14.1	0.1	42.5	27.6	56.8	8.0
Mo Clr 1 Conc	59.0	0.6	14.16	11.47	79.1	14.0
Mo Clr 1 Conc + Clr 1 Scav Conc	62.8	0.9	10.03	8.43	83.2	16.2
Mo Ro Conc	201.5	4.0	2.38	2.27	90.6	15.9
Mo Ro Conc + Ro Scav Conc	496.8	5.0	1.93	1.90	91.0	19.5



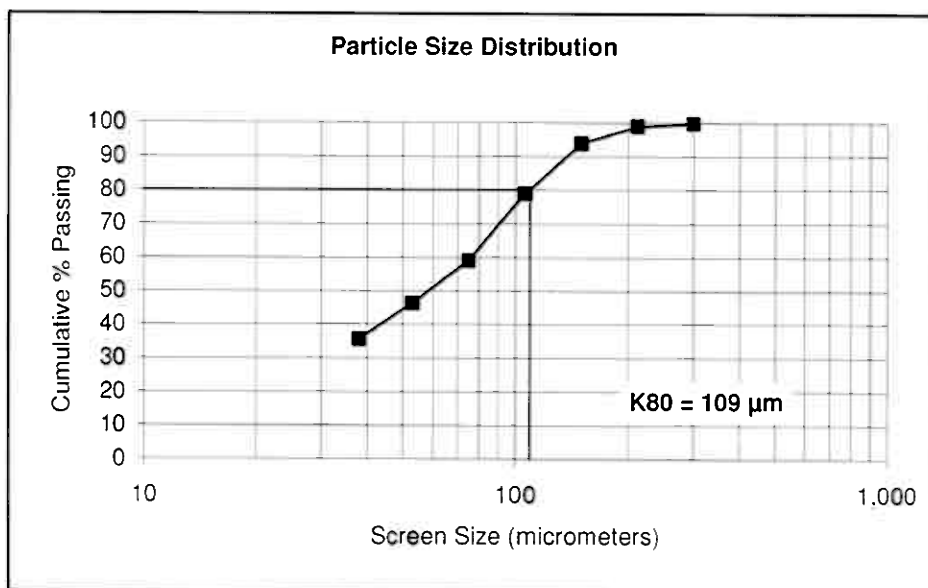
**SGS Minerals Services  
Size Distribution Analysis**

Project No.  
**11656-001**

Sample: **Ro Sc TI Sub**

Test No.: **F8**

Mesh	Size	Weight grams	% Retained		% Passing Cumulative
	µm		Individual	Cumulative	
48	300	0.4	0.3	0.3	99.7
65	212	1.3	0.9	1.2	98.8
100	150	7.1	4.9	6.1	93.9
150	106	21.5	15.0	21.1	78.9
200	75	28.5	19.9	41.0	59.0
270	53	18.3	12.7	53.7	46.3
400	38	15.3	10.7	64.4	35.6
Pan	-38	51.1	35.6	100.0	0.0
<b>Total</b>	-	<b>143.4</b>	100.0	-	-
<b>K80</b>	<b>109</b>				



Test No.:  
F9

Project No.: 11656-001

Operator: PSM  
Date: Dec. 6/2007

**Purpose:** Cleaner test to observe effect of less fuel oil in roughers, re-grind on 1st Cleaner concentrate, and addition of cyanide and lime to depress pyrite.  
Achieve grade of 50% Mo in 4th cleaner concentrate.  
Sodium silicate added to depress talc in Clr 2.  
As outlined below.

**Feed:** 10kg of Hurdal ore composite

**Grind:** 45 minutes, Laboratory 10kg SS Rod Mill, 65 % solids.  
5 minutes re-grind in pebble mill

**Notes:** - Rougher pull rate every 10 seconds for first 10 minutes  
- Rougher pull rate every 15 seconds after 10 minutes

K80 (primary grind): 119  
K80 (re-grind): 18

**Conditions:**

Stage	Reagents added, grams per tonne					Time, minutes			pH	Redox
	Diesel Fuel	MIBC	NaCN	Lime	Sod Sil	Grind	Cond.	Froth		
Grind	40					45				
Roughers										
Condition		40					1		Nat	
Mo Rougher 1								2	5.3	
Mo Rougher 2								4		
Mo Rougher 3								4		
Condition	2.5						5			
Mo Rougher 4								5		
Condition	2.5						5			
Mo rougher 5								5		
Condition										
Mo Ro Scav (Sep. Conc.)	10						5	5		
Cleaners										
Ro Conc F-5										
Condition										
		as needed								
Cleaner1								4	8.3	+180
Cleaner1 Scav								6	8.1	+120
Re-grind Clr1 Conc			20	100		5			12.4	-220
Cleaner2	1	2.5	10		1000			4	12.3	-210
Cleaner3			10					3	12.0	-200
Cleaner4								2	11.2	-100
Total	56	42.5	40	100	1000			45		

Stage	Rougher 1-Scav	Cleaner1	Cleaner2	Cleaner 3-4
Flotation Cell	10 kg	101 - 1000g	101 - 500 g	101 - 250g
Speed, rpm	50% setting	1800	1500	1200

#### Metallurgical Balance

Product	Weight		Assays, %		% Distribution	
	g	%	Mo	S	Mo	S
Mo Clr 4 Conc	11.5	0.1	55.5	34.4	64.1	6.8
Mo Clr 4 Tls	1.6	0.02	38.1	23.2	6.0	0.6
Mo Clr 3 Tls	5.5	0.1	11.7	8.21	6.3	0.8
Mo Clr 2 Tls	43.6	0.4	1.67	2.95	7.1	2.2
Mo Clr 1 Scav Conc	19.1	0.2	2.73	2.64	5.1	0.3
Mo Clr 1 Scav Tls	207.5	2.1	0.17	0.890	3.5	9.2
Mo Ro Scav Conc	54	0.5	0.064	0.410	0.3	0.4
Mo Ro Tls	9656.9	96.6	0.008	0.490	3.6	79.7
Head (calc.)	10000	100.0	0.102	0.594	100.0	100.0
(direct)			0.120	0.790		

#### Combined Products

Product	Weight		Assays, %		% Distribution	
	g	%	Mo	S	Mo	S
Mo Clr 4 Conc	11.5	0.1	55.5	34.4	64.1	6.8
Mo Clr 3 Conc	13.4	0.1	53.4	33.1	70.1	7.5
Mo Clr 2 Conc	18.9	0.2	41.3	25.5	76.4	8.2
Mo Clr 1 Conc	42.5	0.6	13.65	9.87	83.5	10.4
Mo Clr 1 Conc + Clr 1 Scav Conc	81.6	0.8	11.09	7.77	85.6	10.7
Mo Ro Conc	280.1	2.9	3.25	4.09	92.1	19.9
Mo Ro Conc + Ro Scav Conc	343.1	3.4	2.76	3.51	92.4	20.3

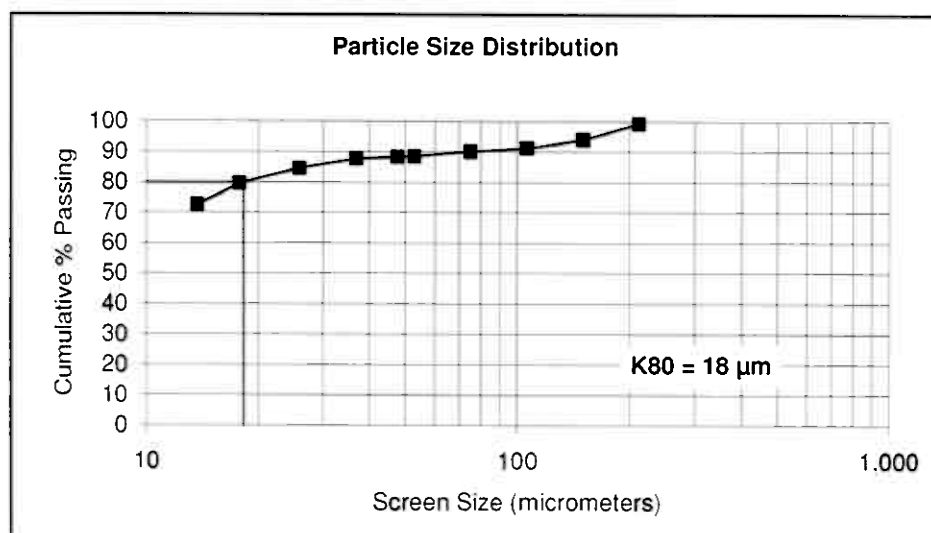
**SGS Minerals Services**  
**Size Distribution Analysis**

Project No.  
**11656-001**

Sample: **Comb Prod**

Test No.: **F-9**

Dry Solids S.G.= <b>2.63</b>		Water Temperature = <b>4.00 C°</b>			
Size		Weight grams	% Retained		% Passing Cumulative
Mesh	µm		Individual	Cumulative	
65	212	0.4	0.8	0.8	99.2
100	150	2.6	5.2	6.0	94.0
150	106	1.5	2.9	8.9	91.1
200	75	0.5	1.1	10.0	90.0
270	53	0.8	1.5	11.5	88.5
	48	0.1	0.2	11.7	88.3
	37	0.3	0.5	12.2	87.8
	26	1.6	3.1	15.4	84.6
	18	2.5	5.0	20.4	79.6
	14	3.5	7.0	27.5	72.5
	-14	36.3	72.5	100.0	0.0
<b>Total</b>	-	<b>50.0</b>	<b>100.0</b>	-	-
<b>K80</b>	<b>18</b>				



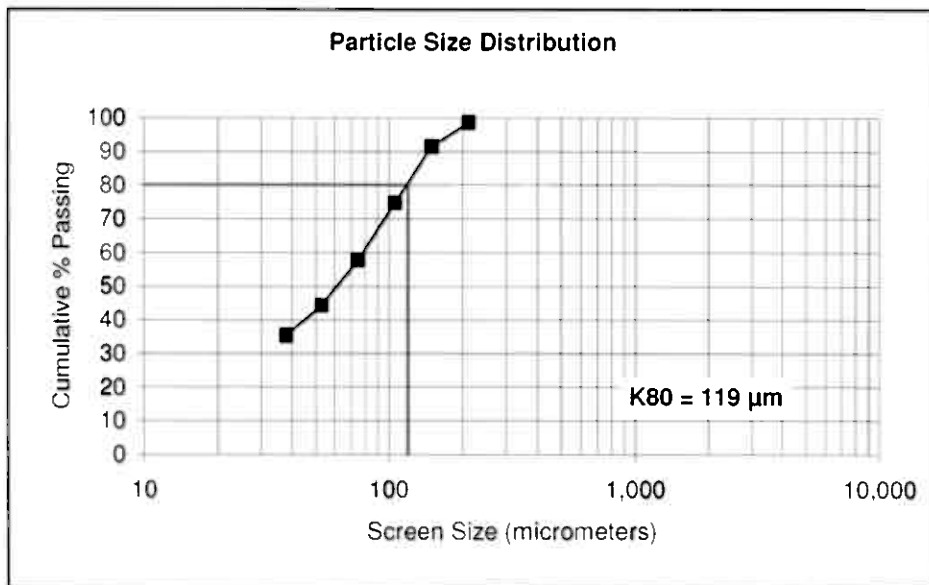
**SGS Minerals Services**  
**Size Distribution Analysis**

Project No.  
**11656-001**

Sample: **Ro Scav Tail**

Test No.: **F9**

Mesh	Size	Weight grams	% Retained		% Passing Cumulative
	µm		Individual	Cumulative	
65	212	2.0	1.4	1.4	98.6
100	150	10.3	7.1	8.5	91.5
150	106	24.2	16.8	25.3	74.7
200	75	24.6	17.0	42.3	57.7
270	53	19.5	13.5	55.8	44.2
400	38	12.7	8.8	64.6	35.4
Pan	-38	51.1	35.4	100.0	0.0
<b>Total</b>	-	<b>144.4</b>	<b>100.0</b>	-	-
<b>K80</b>	<b>119</b>				



Test No.:  
F10

Project No.: 11656-001

Operator: PSM  
Date:

**Purpose:**

Cleaner test to observe effect of stage grinding of Rougher feed to avoid over grinding of liberated Mo  
Re-grind on rougher concentrate, addition of cyanide and lime to depress pyrite.  
Sodium silicate added to depress talc in Clr 1  
Achieve grade of 50% Mo in 4th cleaner concentrate

**Procedure:**

Improve Mo recovery to final concentrate, above 1% and 1%  
As outlined below:

**Feed:**

10 kg of Hurdal ore composite

**Grind:**

Primary grind: *Stage at 3 minutes intervals* laboratory 10 kg SS Rod Mill, 65 % solids  
10 minutes Rougher concentrate re-grind in pebble mill

**Notes:**

- Rougher pull rate every 10 seconds for first 10 minutes K80 (primary grind): 14% µm  
- Rougher pull rate every 15 seconds after 10 minutes K80 (re-grind): 24 µm  
- measured pH levels in cleaners that differ from target pH levels are bracketed in red

**Conditions:**

Stage	Reagents added, grams per tonne					Time, minutes			pH	Redox
	Diesel Fuel	MIBC	NaCN	Lime	Sod Sil	Grind	Cond.	Froth		
Grind	40					Stage Gr.				
Roughers										
Condition		40					1		Nat	
Mo Rougher 1								2	< 3	
Mo Rougher 2								4		
Mo Rougher 3								4		
Condition	2.5						5			
Mo Rougher 4								5		
Condition	2.5						5			
Mo rougher 5		5						5		
Condition										
Mo Ro Scav (Sep. Conc.)	10						5	6		
Re-grind										
Ro Conc 1-5	0.5		20	as needed for pH 9.5 = 16 g/t	200	10			9.5	
Condition		as needed		as needed						
Cleaner1	1	2.5		12				4	10.0	-160
Cleaner1 Scav	1	1		0				6	10.0	-170
Cleaner2		2	10	0				4	10.5	-200
Cleaner3		1	10	25				3	11.0	-180
Cleaner4		—		25				2	11.5	180
Total	56.5	51.5	40	76	200			45		

Stage	Rougher 1-Scav	Cleaner1	Cleaner2	Cleaner 3-4
Flotation Cell	10 kg	D1 - 100 g	D1 - 50 g	D1 - 25 g
Speed, rpm	50% setting	1500	1500	1200

**Metallurgical Balance**

Product	Weight		Assays, %		% Distribution	
	g	%	Mo	S	Mo	S
Mo Clr 4 Conc.	16.7	0.2	45.1	32.1	76.0	8.6
Mo Clr 4 Tls.	2	0.02	30.4	27.3	6.1	0.9
Mo Clr 3 Tls.	3.4	0.0	7.11	11.7	2.4	0.6
Mo Clr 2 Tls.	30.1	0.3	1.450	3.110	4.4	1.5
Mo Clr 1 Scav Conc.	19.4	0.2	0.92	2.880	1.8	0.4
Mo Clr 1 Scav Tls.	349.2	3.5	0.041	1.240	1.4	16.1
Mo Ro Scav Conc.	79.2	0.8	0.068	0.490	0.5	0.6
Mo Ro Tls.	9500	95.0	0.0076	0.430	7.5	71.4
Head (calc.)	10000	100.0	0.099	0.626	100.0	100.0
(direct)			0.120	0.790		

**Combined Products**

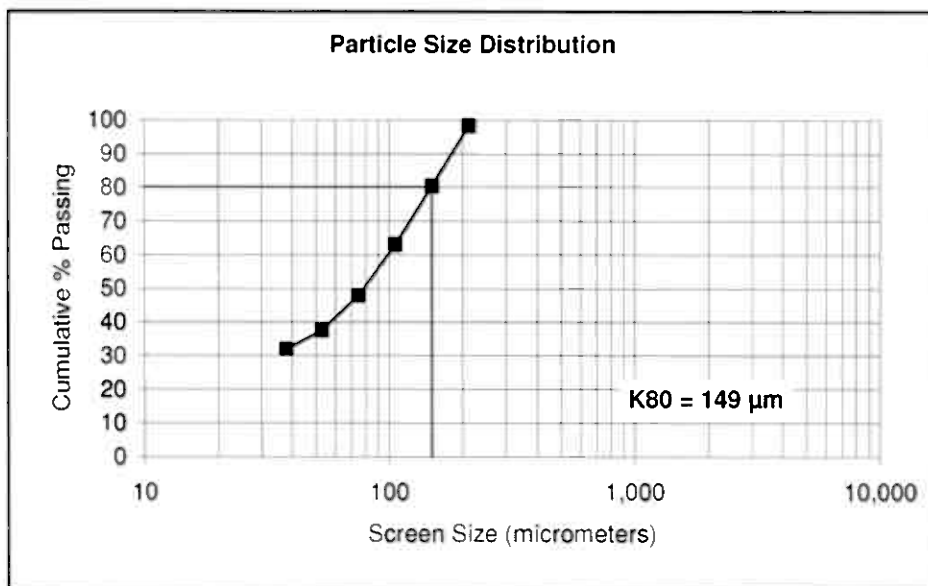
Product	Weight		Assays, %		% Distribution	
	g	%	Mo	S	Mo	S
Mo Clr 4 Conc.	16.7	0.2	45.1	32.1	76.0	8.6
Mo Clr 3 Conc.	15.7	0.2	43.5	31.6	82.1	9.4
Mo Clr 2 Conc.	22.1	0.2	37.9	28.5	84.5	10.1
Mo Clr 1 Conc.	52.2	0.5	16.89	13.87	85.9	11.6
Mo Clr 1 Conc. + Clr 1 Scav Conc.	71.6	0.7	12.56	10.45	90.7	12.0
Mo Ro Conc.	420.8	4.2	2.17	4.17	92.2	25.0
Mo Ro Conc. + Ro Scav Conc.	500	5.0	1.84	3.59	92.7	28.6

**SGS Minerals Services  
Size Distribution Analysis**

Project No.  
**11656-001**

Sample: **Ro Scav Tail sub**      Test No.: **F10**

Mesh	Size	Weight grams	% Retained		% Passing Cumulative
	µm		Individual	Cumulative	
65	212	1.9	1.7	1.7	98.3
100	150	19.7	17.8	19.5	80.5
150	106	19.4	17.5	37.0	63.0
200	75	16.8	15.1	52.1	47.9
270	53	11.5	10.4	62.5	37.5
400	38	6.2	5.6	68.1	31.9
Pan	-38	35.4	31.9	100.0	0.0
<b>Total</b>	-	<b>110.9</b>	<b>100.0</b>	-	-
<b>K80</b>	<b>149</b>				







Test No: F11 Project No: 11656-001 Operator: PSM  
Date:

**Purpose:** Cleaner test to depress pyrite with lime only  
Achieve grade of 50% Mo in 4th cleaner concentrate  
Sodium silicate added to depress sink in Clr 1  
Stage grinding of Rougher feed

**Procedure:** As outlined below.

**Feed:** 10kg of Hurdal ore composite

**Grind:** Stage grinding of flotation feed, laboratory 10kg SS Rod Mill, 65 % solids  
10 minutes re-grind in pebble mill

**Notes:** - Rougher pull rate every 10 seconds for first 10 minutes K80 (primary grind): 142 µm  
- Rougher pull rate every 15 seconds after 10 minutes K80 (re-grind): 23 µm  
- In Re-grind, lime added to pH 9.5 before s.d. Sil. Added

**Conditions:**

Stage	Reagents added, grams per tonne				Time, minutes			pH	Redox
	Diesel Fuel	MIBC	Lime	Sod Sil	Grind	Cond.	Froth		
Grind	40				Stage Gr.				
Roughers									
Condition		40				1		Nat	
Mo Rougher 1							2	8.2	
Mo Rougher 2							4		
Mo Rougher 3							4		
Condition	2.5					5			
Mo Rougher 4		5					6		
Condition	2.5					5			
Mo rougher 5							5		
Condition									
Mo Ro Scav (Sep. Conc.)	10					5	6		
Re-grind									
Re Conc 1-3	0.5		as needed for pH 9.5 = 16 g/t	200	10			9.5	-120
Condition		as needed	as needed						
Cleaner1		2.5	0				4	10 (11)	-180
Cleaner1 Scav		1	0				6	10.0	-150
Cleaner2		2	23				4	10.5	-200
Cleaner3		1	20				3	11.0	-180
Cleaner4		—	31				2	11.5	-120
Total	55.5	51.5	90	200			45		

Stage	Rougher 1-Scav	Cleaner1	Cleaner2	Cleaner 3-4
Flotation Cell	10 kg	D1 - 1000g	D1 - 500 g	D1 - 250g
Speed, rpm	50% setting	1800	1500	1200

**Metallurgical Balance**

Product	Weight		Assays, %		% Distribution	
	g	%	Mo	S	Mo	S
Mo Clr 4 Conc.	14.7	0.1	48.2	30.5	72.6	7.3
Mo Clr 4 Tls.	1	0.01	35.3	23.5	3.6	0.4
Mo Clr 2 Tls.	2.1	0.0	12.5	9.13	2.7	0.3
Mo Clr 2 Tls.	17.2	0.2	2.20	2.67	3.9	0.7
Mo Clr 1 Scav Conc.	21.4	0.2	2.53	2.93	5.5	0.3
Mo Clr 1 Scav Tls.	337.9	3.4	0.067	0.840	2.3	16.1
Mo Ro Scav Conc.	47.3	0.5	0.067	0.520	0.3	0.4
Mo Ro Tls	9555.4	95.6	0.0092	0.450	9.0	74.5
Head (calc.)	10000	100.0	0.065	0.616	100.0	100.0
(direct)			0.120	0.790		

**Combined Products**

Product	Weight		Assays, %		% Distribution	
	g	%	Mo	S	Mo	S
Mo Clr 4 Conc.	14.7	0.1	48.2	30.5	72.6	7.3
Mo Clr 3 Conc.	15.7	0.2	47.4	30.1	76.2	7.7
Mo Clr 2 Conc.	17.8	0.2	43.3	27.6	75.9	8.0
Mo Clr 1 Conc.	35.0	0.4	23.1	15.3	82.8	8.7
Mo Clr 1 Conc. + Clr 1 Scav. Conc.	56.4	0.6	15.28	9.54	88.3	9.0
Mo Ro Conc.	394.3	3.9	2.24	3.92	90.7	25.1
Mo Ro Conc + Ro Scav. Conc.	441.6	4.4	2.01	3.55	91.0	25.5



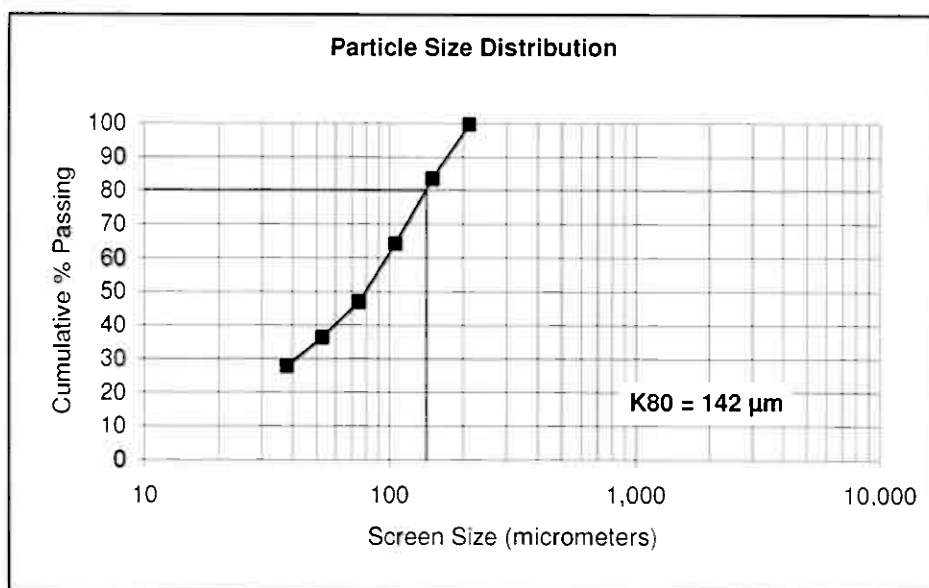
**SGS Minerals Services**  
**Size Distribution Analysis**

Project No.  
**11656-001**

Sample: **Ro Scav Tail sub**

Test No.: **F11**

Mesh	Size	Weight grams	% Retained		% Passing Cumulative
	µm		Individual	Cumulative	
65	212	0.6	0.5	0.5	99.5
100	150	19.7	16.0	16.5	83.5
150	106	23.8	19.3	35.9	64.1
200	75	21.3	17.3	53.2	46.8
270	53	13.0	10.6	63.7	36.3
400	38	10.4	8.5	72.2	27.8
Pan	-38	34.2	27.8	100.0	0.0
<b>Total</b>	-	<b>123.0</b>	<b>100.0</b>	-	-
<b>K80</b>	<b>142</b>				





# MASTERSIZER



## Result Analysis Report

Sample Name:  
11656-001 Comb Prod - Average  
Sample Source & type:  
Factory - F11  
Sample bulk lot ref:  
129-ABC

SOP Name:  
default  
Measured by:  
L. Hydrot  
Result Source:  
Averaged

Measured:  
Friday, January 16, 2008 8:46:11 AM  
Analysed:  
Friday, January 16, 2008 8:46:12 AM

Particle Name:  
Default  
Particle RI:  
1.520  
Dispersant Name:  
Water

Accessory Name:  
Hydro 2000G (A)  
Absorption:  
0.1  
Dispersant RI:  
1.333

Analysis model:  
General purpose  
Size range:  
0.020 to 2000.000  $\mu\text{m}$   
Weighted Residual:  
1.560 %

Sensitivity:  
Enhanced  
Obscuration:  
19.33 %  
Result Emulation:  
Off

Concentration:  
0.0192 %Vol

Span:  
4.145  
Surface Weighted Mean D(3.2):  
4.197  $\mu\text{m}$

Uniformity:  
1.53  
Vol Weighted Mean D(4.3):  
17.635  $\mu\text{m}$

Result units:  
Volume

d(0.1): 1.657  $\mu\text{m}$  d(0.5): 0.941  $\mu\text{m}$  D(0.80): 22.73  $\mu\text{m}$



0.010	0.020	0.030	0.040	0.050	0.060	0.070	0.080	0.090	0.100	0.120	0.150	0.200	0.250	0.300	0.350	0.400	0.450	0.500	0.600	0.700	0.800	0.900	1.000	1.200	1.500	2.000	2.500	3.000	4.000	5.000	6.000	8.000	10.000	12.000	15.000	20.000	25.000	30.000	40.000	50.000	60.000	80.000	100.000	120.000	150.000	200.000	250.000	300.000	400.000	500.000	600.000	800.000	1000.000	1200.000	1500.000	2000.000
0.010	0.020	0.030	0.040	0.050	0.060	0.070	0.080	0.090	0.100	0.120	0.150	0.200	0.250	0.300	0.350	0.400	0.450	0.500	0.600	0.700	0.800	0.900	1.000	1.200	1.500	2.000	2.500	3.000	4.000	5.000	6.000	8.000	10.000	12.000	15.000	20.000	25.000	30.000	40.000	50.000	60.000	80.000	100.000	120.000	150.000	200.000	250.000	300.000	400.000	500.000	600.000	800.000	1000.000	1200.000	1500.000	2000.000
0.010	0.020	0.030	0.040	0.050	0.060	0.070	0.080	0.090	0.100	0.120	0.150	0.200	0.250	0.300	0.350	0.400	0.450	0.500	0.600	0.700	0.800	0.900	1.000	1.200	1.500	2.000	2.500	3.000	4.000	5.000	6.000	8.000	10.000	12.000	15.000	20.000	25.000	30.000	40.000	50.000	60.000	80.000	100.000	120.000	150.000	200.000	250.000	300.000	400.000	500.000	600.000	800.000	1000.000	1200.000	1500.000	2000.000

Operator notes:

Test No.:  
F12

Project No.: 11656-001

Operator: PSM  
Date:

**Purpose:** Cleaner test to depress pyrite with NaHS and lime  
Achieve grade of 50% Mo in 4th cleaner concentrate  
Sodium silicate added to depress tale in Clr 1  
Stage grinding of Rougher feed

**Procedure:** As outlined below.

**Feed:** 10kg of Hurdal ore composite

**Grind:** Stage grinding of flotation feed, laboratory 10-g SS Rod Mill, 65 % solids  
10 minutes to grind in pebble mill

**Notes:**  
- Rougher pull rate every 10 seconds for first 10 minutes  
- Rougher pull rate every 15 seconds after 10 minutes  
- Measured pH levels in cleaners that differ from target pH levels are bracketed in red

K90 (primary grind): 134 µm  
K90 (re-grind): 23 µm

**Conditions:**

Stage	Reagents added, grams per tonne					Time, minutes			pH	Reflux
	Diesel Fuel	MIBC	NaHS	Lime	Sod Sil	Grind	Concl.	Froth		
Grind	40					Stage Gr.				
Rougher										
Condition		40					1		Nat	
Mo Rougher 1								2	8.7	
Mo Rougher 2								4	9.0	
Mo Rougher 3		5						4	8.6	
Condition	2.5						5			
Mo Rougher 4								5	8.5	
Condition	2.5						5			
Mo rougher 5								5	8.3	
Condition										
Mo Ro Scav (Sep. Conc.)	10						5	6		
Re-grind										
Re Conc 1-5	0.5		200	none	1000	10			9.5 (12.3 after adding NaOH 50g)	
Condition									12.0	-300
Cleaner1		as needed	as needed	as needed				4	10 (10)	-300
Cleaner1 Scav		2.5		0				6	10 (10)	-300
Cleaner2		1.5	50	0				4	10.5 (11.5)	-250
Cleaner3		1	50	0				3	11.0	-270
Cleaner4		--	10	20				3	11.5	-280
Total	55.5	50	300	20	1000			15		

Stage	Rougher 1 Scav	Cleaner1	Cleaner2	Cleaner 3-4
Flotation Cell	100kg	1000g	1000g	1000g
Speed, rpm	50% setting	1500	1500	1200

**Metallurgical Balance**

Product	Weight		Assays, %		% Distribution	
	g	%	Mo	S	Mo	S
Mo Clr 4 Conc.	9.5	0.1	55.6	36.2	51.3	5.9
Mo Clr 4 Tls.	4.1	0.04	39.6	28.6	15.8	2.0
Mo Clr 3 Tls.	4.7	0.0	21.2	16.8	9.7	1.3
Mo Clr 2 Tls.	15.6	0.2	4.32	4.10	6.5	1.1
Mo Clr 1 Scav Conc.	24	0.2	2.16	2.620	5.0	0.3
Mo Clr 1 Scav Tls.	217.8	2.2	0.18	0.720	3.8	9.8
Mo Ro Scav Conc.	59.3	0.9	0.05	0.370	0.4	0.6
Mo Ro Tls.	9635	98.4	0.008	0.480	7.5	79.1
Head (calc.)	10000	100.0	0.103	0.585	100.0	100.0
(direct)			0.120	0.790		

**Combined Products**

Product	Weight		Assays, %		% Distribution	
	g	%	Mo	S	Mo	S
Mo Clr 4 Conc.	9.5	0.1	55.6	36.2	51.3	5.9
Mo Clr 3 Conc.	13.6	0.1	50.8	33.9	67.0	7.9
Mo Clr 2 Conc.	15.3	0.2	43.2	29.5	76.7	9.2
Mo Clr 1 Conc.	35.9	0.3	25.30	17.82	83.2	10.3
Mo Clr 1 Conc. + Clr 1 Scav Conc.	57.9	0.6	15.71	10.73	58.3	10.6
Mo Ro Conc.	276.7	2.8	3.44	4.32	92.1	20.4
Mo Ro Conc. + Ro Scav Conc.	365	3.7	2.61	3.36	92.5	20.9

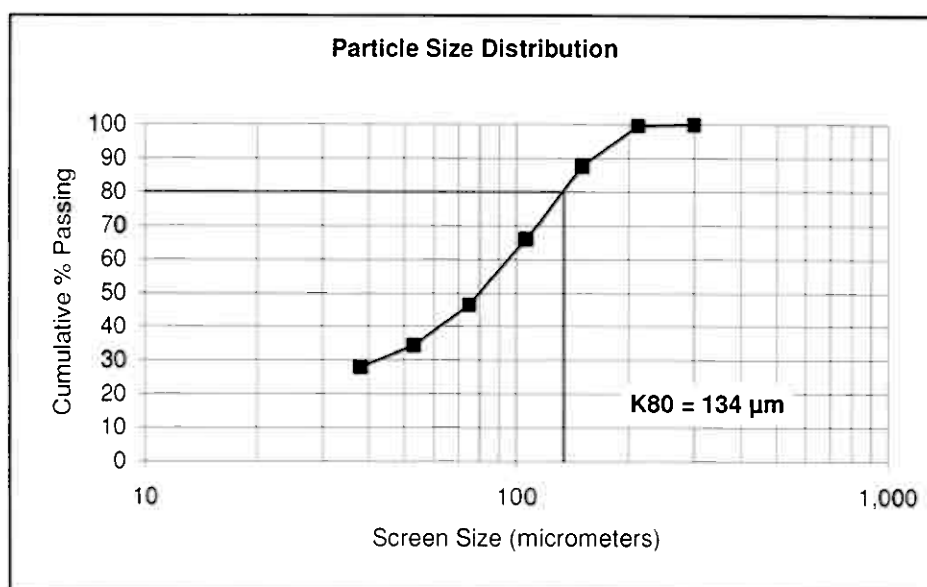
**SGS Minerals Services**  
**Size Distribution Analysis**

Project No.  
**11656-002**

Sample: **Ro Scav Tails Sub**

Test No.: **F12**

Mesh	Size	Weight grams	% Retained		% Passing Cumulative
	µm		Individual	Cumulative	
48	300	0.0	0.0	0.0	100.0
65	212	0.5	0.3	0.3	99.7
100	150	17.1	12.0	12.3	87.7
150	106	31.1	21.7	34.1	65.9
200	75	28.0	19.6	53.6	46.4
270	53	17.2	12.0	65.7	34.3
400	38	9.3	6.5	72.2	27.8
Pan	-38	39.8	27.8	100.0	0.0
<b>Total</b>	-	<b>143.0</b>	100.0	-	-
<b>K80</b>	<b>134</b>				





# MASTERSIZER 2000

## Result Analysis Report

Sample Name:  
11656-002 Comb Prod - Average  
Sample Source & type:  
Factory - F12  
Sample bulk for ref:  
123-ABC

SOP Name:  
default  
Measured by:  
L\_hydro1  
Result Source:  
Averaged

Measured:  
Tuesday, February 05, 2008 9:16:42 AM  
Analysis:  
Tuesday, February 05, 2008 9:16:43 AM

Particle Name:  
Default  
Particle ID:  
1.520  
Dispersant Name:  
Water

Accessory Name:  
Hydro 2000G (A)  
Absorption:  
0.1  
Dispersant RI:  
1.330

Analysis model:  
General purpose  
Size range:  
0.000 to 2000.000  $\mu\text{m}$   
Weighted Residual:  
1.579 %

Sensitivity:  
Enhanced  
Obscuration:  
16.26 %  
Resin Emulsion:  
Off

Concentration:  
0.0112 %Vol

Specs:  
4.203

Uniformity:  
1.43

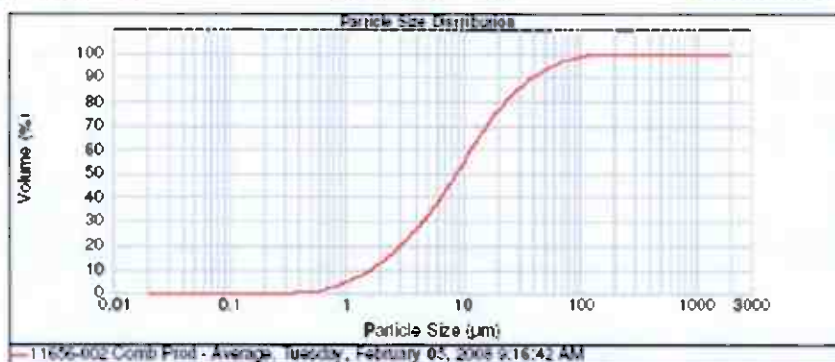
Result units:  
Volume

Specific Surface Area:  
1.43  $\text{m}^2/\text{g}$

Surface Weighted Mean D[3,2]:  
4.199  $\mu\text{m}$

Vol Weighted Mean D[4,3]:  
16.725  $\mu\text{m}$

d[0.1]: 1.660  $\mu\text{m}$  d[0.5]: 6.945  $\mu\text{m}$  D(0.80): 23.32  $\mu\text{m}$



Bin	Vol	Area	Bin	Vol	Area	Bin	Vol	Area	Bin	Vol	Area	Bin	Vol	Area	Bin	Vol	Area
0.000	0.00	0.00	0.000	0.00	0.00	0.000	0.00	0.00	0.000	0.00	0.00	0.000	0.00	0.00	0.000	0.00	0.00
0.001	0.00	0.00	0.001	0.00	0.00	0.001	0.00	0.00	0.001	0.00	0.00	0.001	0.00	0.00	0.001	0.00	0.00
0.002	0.00	0.00	0.002	0.00	0.00	0.002	0.00	0.00	0.002	0.00	0.00	0.002	0.00	0.00	0.002	0.00	0.00
0.003	0.00	0.00	0.003	0.00	0.00	0.003	0.00	0.00	0.003	0.00	0.00	0.003	0.00	0.00	0.003	0.00	0.00
0.004	0.00	0.00	0.004	0.00	0.00	0.004	0.00	0.00	0.004	0.00	0.00	0.004	0.00	0.00	0.004	0.00	0.00
0.005	0.00	0.00	0.005	0.00	0.00	0.005	0.00	0.00	0.005	0.00	0.00	0.005	0.00	0.00	0.005	0.00	0.00
0.006	0.00	0.00	0.006	0.00	0.00	0.006	0.00	0.00	0.006	0.00	0.00	0.006	0.00	0.00	0.006	0.00	0.00
0.007	0.00	0.00	0.007	0.00	0.00	0.007	0.00	0.00	0.007	0.00	0.00	0.007	0.00	0.00	0.007	0.00	0.00
0.008	0.00	0.00	0.008	0.00	0.00	0.008	0.00	0.00	0.008	0.00	0.00	0.008	0.00	0.00	0.008	0.00	0.00
0.009	0.00	0.00	0.009	0.00	0.00	0.009	0.00	0.00	0.009	0.00	0.00	0.009	0.00	0.00	0.009	0.00	0.00
0.010	0.00	0.00	0.010	0.00	0.00	0.010	0.00	0.00	0.010	0.00	0.00	0.010	0.00	0.00	0.010	0.00	0.00
0.011	0.00	0.00	0.011	0.00	0.00	0.011	0.00	0.00	0.011	0.00	0.00	0.011	0.00	0.00	0.011	0.00	0.00
0.012	0.00	0.00	0.012	0.00	0.00	0.012	0.00	0.00	0.012	0.00	0.00	0.012	0.00	0.00	0.012	0.00	0.00
0.013	0.00	0.00	0.013	0.00	0.00	0.013	0.00	0.00	0.013	0.00	0.00	0.013	0.00	0.00	0.013	0.00	0.00
0.014	0.00	0.00	0.014	0.00	0.00	0.014	0.00	0.00	0.014	0.00	0.00	0.014	0.00	0.00	0.014	0.00	0.00
0.015	0.00	0.00	0.015	0.00	0.00	0.015	0.00	0.00	0.015	0.00	0.00	0.015	0.00	0.00	0.015	0.00	0.00
0.016	0.00	0.00	0.016	0.00	0.00	0.016	0.00	0.00	0.016	0.00	0.00	0.016	0.00	0.00	0.016	0.00	0.00
0.017	0.00	0.00	0.017	0.00	0.00	0.017	0.00	0.00	0.017	0.00	0.00	0.017	0.00	0.00	0.017	0.00	0.00
0.018	0.00	0.00	0.018	0.00	0.00	0.018	0.00	0.00	0.018	0.00	0.00	0.018	0.00	0.00	0.018	0.00	0.00
0.019	0.00	0.00	0.019	0.00	0.00	0.019	0.00	0.00	0.019	0.00	0.00	0.019	0.00	0.00	0.019	0.00	0.00
0.020	0.00	0.00	0.020	0.00	0.00	0.020	0.00	0.00	0.020	0.00	0.00	0.020	0.00	0.00	0.020	0.00	0.00
0.021	0.00	0.00	0.021	0.00	0.00	0.021	0.00	0.00	0.021	0.00	0.00	0.021	0.00	0.00	0.021	0.00	0.00
0.022	0.00	0.00	0.022	0.00	0.00	0.022	0.00	0.00	0.022	0.00	0.00	0.022	0.00	0.00	0.022	0.00	0.00
0.023	0.00	0.00	0.023	0.00	0.00	0.023	0.00	0.00	0.023	0.00	0.00	0.023	0.00	0.00	0.023	0.00	0.00
0.024	0.00	0.00	0.024	0.00	0.00	0.024	0.00	0.00	0.024	0.00	0.00	0.024	0.00	0.00	0.024	0.00	0.00
0.025	0.00	0.00	0.025	0.00	0.00	0.025	0.00	0.00	0.025	0.00	0.00	0.025	0.00	0.00	0.025	0.00	0.00
0.026	0.00	0.00	0.026	0.00	0.00	0.026	0.00	0.00	0.026	0.00	0.00	0.026	0.00	0.00	0.026	0.00	0.00
0.027	0.00	0.00	0.027	0.00	0.00	0.027	0.00	0.00	0.027	0.00	0.00	0.027	0.00	0.00	0.027	0.00	0.00
0.028	0.00	0.00	0.028	0.00	0.00	0.028	0.00	0.00	0.028	0.00	0.00	0.028	0.00	0.00	0.028	0.00	0.00
0.029	0.00	0.00	0.029	0.00	0.00	0.029	0.00	0.00	0.029	0.00	0.00	0.029	0.00	0.00	0.029	0.00	0.00
0.030	0.00	0.00	0.030	0.00	0.00	0.030	0.00	0.00	0.030	0.00	0.00	0.030	0.00	0.00	0.030	0.00	0.00
0.031	0.00	0.00	0.031	0.00	0.00	0.031	0.00	0.00	0.031	0.00	0.00	0.031	0.00	0.00	0.031	0.00	0.00
0.032	0.00	0.00	0.032	0.00	0.00	0.032	0.00	0.00	0.032	0.00	0.00	0.032	0.00	0.00	0.032	0.00	0.00
0.033	0.00	0.00	0.033	0.00	0.00	0.033	0.00	0.00	0.033	0.00	0.00	0.033	0.00	0.00	0.033	0.00	0.00
0.034	0.00	0.00	0.034	0.00	0.00	0.034	0.00	0.00	0.034	0.00	0.00	0.034	0.00	0.00	0.034	0.00	0.00
0.035	0.00	0.00	0.035	0.00	0.00	0.035	0.00	0.00	0.035	0.00	0.00	0.035	0.00	0.00	0.035	0.00	0.00
0.036	0.00	0.00	0.036	0.00	0.00	0.036	0.00	0.00	0.036	0.00	0.00	0.036	0.00	0.00	0.036	0.00	0.00
0.037	0.00	0.00	0.037	0.00	0.00	0.037	0.00	0.00	0.037	0.00	0.00	0.037	0.00	0.00	0.037	0.00	0.00
0.038	0.00	0.00	0.038	0.00	0.00	0.038	0.00	0.00	0.038	0.00	0.00	0.038	0.00	0.00	0.038	0.00	0.00
0.039	0.00	0.00	0.039	0.00	0.00	0.039	0.00	0.00	0.039	0.00	0.00	0.039	0.00	0.00	0.039	0.00	0.00
0.040	0.00	0.00	0.040	0.00	0.00	0.040	0.00	0.00	0.040	0.00	0.00	0.040	0.00	0.00	0.040	0.00	0.00
0.041	0.00	0.00	0.041	0.00	0.00	0.041	0.00	0.00	0.041	0.00	0.00	0.041	0.00	0.00	0.041	0.00	0.00
0.042	0.00	0.00	0.042	0.00	0.00	0.042	0.00	0.00	0.042	0.00	0.00	0.042	0.00	0.00	0.042	0.00	0.00
0.043	0.00	0.00	0.043	0.00	0.00	0.043	0.00	0.00	0.043	0.00	0.00	0.043	0.00	0.00	0.043	0.00	0.00
0.044	0.00	0.00	0.044	0.00	0.00	0.044	0.00	0.00	0.044	0.00	0.00	0.044	0.00	0.00	0.044	0.00	0.00
0.045	0.00	0.00	0.045	0.00	0.00	0.045	0.00	0.00	0.045	0.00	0.00	0.045	0.00	0.00	0.045	0.00	0.00
0.046	0.00	0.00	0.046	0.00	0.00	0.046	0.00	0.00	0.046	0.00	0.00	0.046	0.00	0.00	0.046	0.00	0.00
0.047	0.00	0.00	0.047	0.00	0.00	0.047	0.00	0.00	0.047	0.00	0.00	0.047	0.00	0.00	0.047	0.00	0.00
0.048	0.00	0.00	0.048	0.00	0.00	0.048	0.00	0.00	0.048	0.00	0.00	0.048	0.00	0.00	0.048	0.00	0.00
0.049	0.00	0.00	0.049	0.00	0.00	0.049	0.00	0.00	0.049	0.00	0.00	0.049	0.00	0.00	0.049	0.00	0.00
0.050	0.00	0.00	0.050	0.00	0.00	0.050	0.00	0.00	0.050	0.00	0.00	0.050	0.00	0.00	0.050	0.00	0.00
0.051	0.00	0.00	0.051	0.00	0.00	0.051	0.00	0.00	0.051	0.00	0.00	0.051	0.00	0.00	0.051	0.00	0.00
0.052	0.00	0.00	0.052	0.00	0.00	0.052	0.00	0.00	0.052	0.00	0.00	0.052	0.00	0.00	0.052	0.00	0.00
0.053	0.00	0.00	0.053	0.00	0.00	0.053	0.00	0.00	0.053	0.00	0.00	0.053	0.00	0.00	0.053	0.00	0.00
0.054	0.00	0.00	0.054	0.00	0.00	0.054	0.00	0.00	0.054	0.00	0.00	0.054	0.00	0.00	0.054	0.00	0.00
0.055	0.00	0.00	0.055	0.00	0.00	0.055	0.00	0.00	0.055	0.00	0.00	0.055	0.00	0.00	0.055	0.00	0.00
0.056	0.00	0.00	0.056	0.00	0.00	0.056	0.00	0.00	0.056	0.00	0.00	0.056	0.00	0.00	0.056	0.00	0.00
0.057	0.00	0.00	0.057	0.00	0.00	0.057	0.00	0.00	0.057	0.00	0.00	0.057	0.00	0.00	0.057	0.00	0.00
0.058	0.00	0.00	0.058	0.00	0.00	0.058	0.00	0.00	0.058	0.00	0.00	0.058	0.00	0.00	0.058	0.00	0.00
0.059	0.00	0.00	0.059	0.00	0.00	0.059	0.00	0.00	0.059	0.00	0.00	0.059	0.00	0.00	0.059	0.00	0.00
0.060	0.00	0.00	0.060	0.00	0.00	0.060	0.00	0.00	0.060	0.00	0.00	0.060	0.00	0.00	0.060	0.00	0.00
0.061	0.00	0.00	0.061	0.00	0.00	0.061	0.00	0.00	0.061	0.00	0.00	0.061	0.00	0.00	0.061	0.00	0.00
0.062	0.00	0.00	0.062	0.00	0.00	0.062	0.00	0.00	0.062	0.00	0.00	0.062	0.00	0.00	0.062	0.00	0.00



Test No.:  
F13

Project No.: 11656-001

Operator:  
Date:

PSM

Purpose: Investigate effect of second re-grind in the cleaners on final conc.  
Investigate the use of fuel oil dispersant, OP6, in rougher

Procedure: As outlined below

Feed: 10kg of Hurdal ore composite

Grind: Stage Grinding of Flotation Feed, Laboratory 10kg SS Rod Mill, 65 % solids  
15 minutes first re-grind in pebble mill  
5 minutes second re-grind in pebble mill

Notes: - Rougher pull rate every 10 seconds for first 10 minutes K30 (primary grade) 148 µm  
- Rougher pull rate every 15 seconds after 10 minutes K30 (5th Clr Conc.) 18 µm  
- Some flotation feed spilled while emptying rod mill  
- Measured pH levels in cleaners that differ from target pH levels are bracketed in red

Stage	Reagents added, grams per tonne						Time, minutes			pH	Reflux
	Diesel Fuel	MIBC	NaCN	Lime	OP6	Sod Sil	Grind	Cond.	Proth		
Grind	40				25		Stage 1 & 2				
Roughers											
Condition		40						1		Nat	
Mo Rougher 1									2	9.5	
Mo Rougher 2									4		
Mo Rougher 3		2.5							4		
Condition	2.5							5			
Mo Rougher 4		2.5							5		
Condition	2.5							5			
Mo rougher 5									5		
Condition											
Mo Ro Scav (5th Clr Conc.)	10	2.5						5	6		
Re-grind											
Mo Conc 1-5	1		20	none	0.5	200	10			9.5 (11.8)	200
Condition		as needed									
Cleaner1		2.5		as needed					4	10 (11)	-80
Cleaner1 Scav	1	2.5							6	10 (10.5)	-20
Cleaner2		—	10	0					3	10.5	-100
Cleaner3		—	10	0					3	9.6	-10
Cleaner4		—		23					2	11.0	-80
Cleaner5		—							2	9.8	-20
Re-grind Clr 4 Conc.	1		20			100	5			11.5	-100
Cleaner5		2.5							2	11.5 (11.8)	-50
Total	56	55	60	23	25.5	300		47			

Stage	Rougher 1-Scav	Cleaner1	Cleaner2	Cleaner 3-5
Flotation Cell	10kg	D1 - 1000g	D1 - 500g	D1 - 250g
Speed rpm	50% setting	1800	1500	1200

## Metallurgical Balance

Product	Weight		Assays, %		% Distribution	
	g	%	Mn	S	Mn	S
Mo Clr 5 Conc.	13.6	0.14	56.8	37.0	77.6	10.0
Mo Clr 5 Th.	3.3	0.03	8.99	11.0	3.0	0.7
Mo Clr 4 Th.	1.6	0.02	14.3	15.1	2.1	0.2
Mo Clr 3 Th.	2.4	0.02	3.57	8.72	0.9	0.4
Mo Clr 2 Th.	6.6	0.07	0.810	6.47	0.5	0.9
Mo Clr 1 Scav Conc.	33.3	0.34	1.23	4.58	4.1	2.7
Mo Clr 1 Scav Th.	288.4	2.9	0.055	4.66	1.6	26.3
Mo Ro Scav Conc.	60.5	0.62	0.083	0.340	0.5	0.4
Mo Ro Th.	9405	95.5	0.010	0.310	9.5	55.1
Head (calc.)	9815	100.0	0.101	0.511	100.0	100.0
(direct)			0.120	0.790		

## Combined Products

Product	Weight		Assays, %		% Distribution	
	g	%	Mn	S	Mn	S
Mo Clr 5 Conc.	13.6	0.14	56.8	37.0	77.6	10.0
Mo Clr 4 Conc.	16.9	0.17	47.3	31.9	80.6	10.7
Mo Clr 3 Conc.	18.5	0.19	44.4	30.5	82.9	11.2
Mo Clr 2 Conc.	20.9	0.21	39.8	28.0	83.7	11.6
Mo Clr 1 Conc.	27.5	0.28	30.41	22.81	54.3	12.5
Mo Clr 1 Conc. + Clr 1 Scav. Conc.	60.5	0.62	14.43	12.54	88.4	15.2
Mo Ro Conc.	349.2	3.6	2.56	5.97	90.0	41.5
Mo Ro Conc. + Ro Scav. Conc.	409.7	4.2	2.19	5.14	90.5	41.9

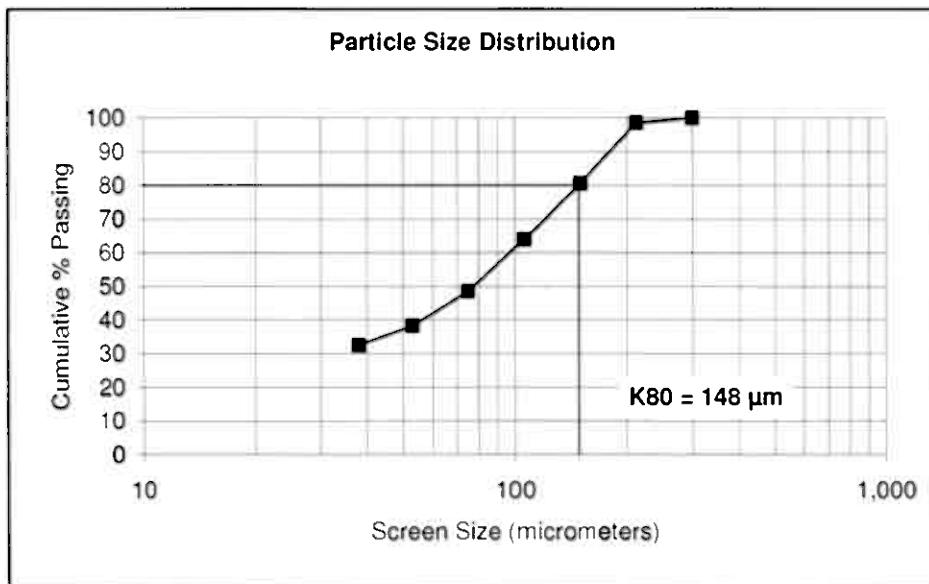
**SGS Minerals Services  
Size Distribution Analysis**

Project No.  
**11656-001**

Sample: **Ro Scav Tls**

Test No.: **F13**

Mesh	Size	Weight grams	% Retained		% Passing Cumulative
	µm		Individual	Cumulative	
48	300	0.0	0.0	0.0	100.0
65	212	2.3	1.5	1.5	98.5
100	150	26.5	17.8	19.4	80.6
150	106	24.8	16.7	36.1	63.9
200	75	22.9	15.4	51.5	48.5
270	53	15.3	10.3	61.8	38.2
400	38	8.5	5.7	67.5	32.5
Pan	-38	48.2	32.5	100.0	0.0
<b>Total</b>	-	<b>148.5</b>	<b>100.0</b>	-	-
<b>K80</b>	<b>148</b>				





Sample Name:  
11656-001 F13 Clrt Sc. Tls. - Average

Sample Source & type:  
Factory - Paris

Sample bulk lot ref:  
P3M

SOP Name:  
default

Measured by:  
Li\_hydro1

Result Source:  
Averaged

Measured:  
Wednesday, July 16, 2008 10:57:40 AM  
Analyse d:  
Wednesday, July 16, 2008 10:57:41 AM

Particle Name:  
DETAU1  
Particle R0:  
1.520  
Dispersant Name:  
Water

Accessory Name:  
Hydro 2000G (A)  
Absorption:  
0.1  
Dispersant Rt:  
1.230

Analysis model:  
General purpose  
Size range:  
0.020 to 2000.000 um  
Weighted residual:  
1.329 %

Sensitivity:  
Enhanced  
Obscuration:  
1221 %  
Result Emulation:  
Off

Concentration:  
0.0090 %Vol

Span :  
2.054

Surface Weighted Mean D[3,2]:  
4.260  $\mu\text{m}$

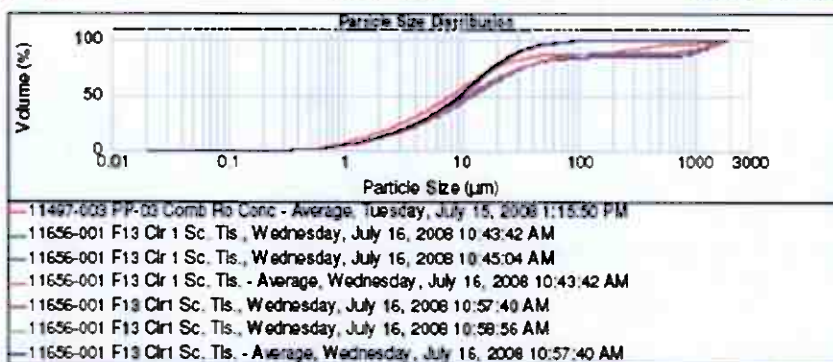
Uniformity:  
1.02  
Vol. Weighted Mean D[4.3]:  
14.242  $\mu\text{m}$

**Result units:**  
Volume

0.11 1.52 0.00

0.5 0.103 1.071

**D(0.80) : 21.23  $\mu$ m**



Year	Vol	Unit	%	Year	Vol	Unit	%	Year	Vol	Unit	%	Year	Vol	Unit	%
0.000	0.000	0.000	0.00	1.000	1.000	0.00	1.000	1.000	0.00	1.000	1.000	0.00	1.000	1.000	0.00
0.001	0.001	0.001	0.00	1.001	1.001	0.00	1.001	1.001	0.00	1.001	1.001	0.00	1.001	1.001	0.00
0.002	0.002	0.002	0.00	1.002	1.002	0.00	1.002	1.002	0.00	1.002	1.002	0.00	1.002	1.002	0.00
0.003	0.003	0.003	0.00	1.003	1.003	0.00	1.003	1.003	0.00	1.003	1.003	0.00	1.003	1.003	0.00
0.004	0.004	0.004	0.00	1.004	1.004	0.00	1.004	1.004	0.00	1.004	1.004	0.00	1.004	1.004	0.00
0.005	0.005	0.005	0.00	1.005	1.005	0.00	1.005	1.005	0.00	1.005	1.005	0.00	1.005	1.005	0.00
0.006	0.006	0.006	0.00	1.006	1.006	0.00	1.006	1.006	0.00	1.006	1.006	0.00	1.006	1.006	0.00
0.007	0.007	0.007	0.00	1.007	1.007	0.00	1.007	1.007	0.00	1.007	1.007	0.00	1.007	1.007	0.00
0.008	0.008	0.008	0.00	1.008	1.008	0.00	1.008	1.008	0.00	1.008	1.008	0.00	1.008	1.008	0.00
0.009	0.009	0.009	0.00	1.009	1.009	0.00	1.009	1.009	0.00	1.009	1.009	0.00	1.009	1.009	0.00
0.010	0.010	0.010	0.00	1.010	1.010	0.00	1.010	1.010	0.00	1.010	1.010	0.00	1.010	1.010	0.00
0.011	0.011	0.011	0.00	1.011	1.011	0.00	1.011	1.011	0.00	1.011	1.011	0.00	1.011	1.011	0.00
0.012	0.012	0.012	0.00	1.012	1.012	0.00	1.012	1.012	0.00	1.012	1.012	0.00	1.012	1.012	0.00
0.013	0.013	0.013	0.00	1.013	1.013	0.00	1.013	1.013	0.00	1.013	1.013	0.00	1.013	1.013	0.00
0.014	0.014	0.014	0.00	1.014	1.014	0.00	1.014	1.014	0.00	1.014	1.014	0.00	1.014	1.014	0.00
0.015	0.015	0.015	0.00	1.015	1.015	0.00	1.015	1.015	0.00	1.015	1.015	0.00	1.015	1.015	0.00
0.016	0.016	0.016	0.00	1.016	1.016	0.00	1.016	1.016	0.00	1.016	1.016	0.00	1.016	1.016	0.00
0.017	0.017	0.017	0.00	1.017	1.017	0.00	1.017	1.017	0.00	1.017	1.017	0.00	1.017	1.017	0.00
0.018	0.018	0.018	0.00	1.018	1.018	0.00	1.018	1.018	0.00	1.018	1.018	0.00	1.018	1.018	0.00
0.019	0.019	0.019	0.00	1.019	1.019	0.00	1.019	1.019	0.00	1.019	1.019	0.00	1.019	1.019	0.00
0.020	0.020	0.020	0.00	1.020	1.020	0.00	1.020	1.020	0.00	1.020	1.020	0.00	1.020	1.020	0.00

**Operator notes:**



## ***Appendix E – Mineralogy Data***

### ***DESCRIPTION of QEMSCAN***

Mineralogical testing can be an extremely powerful tool that compliments any flotation program. Such studies are useful in establishing performance limits and identifying possible areas for improvement. This can be accomplished by either an optical petrography study or QEMSCAN® mineralogical characterization to evaluate various flotation products. QEMSCAN® is an automated SEM that is capable of producing quantitative data to assess bulk modal analysis, liberation characteristics, and mineral associations. QEMSCAN is an acronym for Quantitative Evaluation of Materials by SCANNing electron microscopy, a system which differs from image analysis systems in that it is configured to measure mineralogical variability based on chemistry at the micrometer-scale. QEMSCAN® utilizes both the back-scattered electron (BSE) signal intensity as well as an Energy Dispersive X-ray Signal (EDS) at each measurement point. It thus makes no simplifications or assumptions of homogeneity based on the BSE intensity, as many mineral phases show BSE overlap. EDS signals are used to assign mineral identities to each measurement point by comparing the EDS spectrum against a mineral species identification program (SIP) or database. QEMSCAN® can map many thousands of particles in a polished section to obtain a detailed and statistically robust characterization of the ore liberation. QEMSCAN map the particles based on differences in chemical analyses and can differentiate amongst the various non-opaque gangues present in the ore body.

There are two general types of measurement: those using the linear intercept and those based on particle mapping. Bulk mineral analysis (BMA) is performed using the linear intercept method, while liberation is performed by particle mapping in particle analysis (PMA), specific mineral (SMS) and trace mineral search (TMS) modes. Specific details of the measurement modes are presented below.

Bulk Mineral Analysis, or BMA, is performed by the linear intercept method, in which the electron beam is rastered at a pre-defined point spacing (nominally 3 micrometers, but variable with particle size) along several lines per field, and covering the entire polished section at any given magnification. This provides a robust data set for determination of the bulk mineralogy, with mineral identities and proportions, along with grain size measurements. This would be performed on every section to accurately establish modal abundance. XRD analyses will be

performed to identify the significant crystalline phases present in the ore to support the QEMSCAN work.

The Specific Mineral Search (SMS) routine is a particle mapping method which uses BSE measurements to map only those particles which contain the constituents of interest. This provides a more statistically abundant analysis of the minerals of interest, and provides spatial information, allowing for full characterization of these minerals, including liberation, association and determinative mineralogical characteristics.

Each polished section prepared from an ore sample can be analyzed using the Particle Mineral Analysis (PMA) method. This ensures that the mineralogy of all minerals is captured. This method is a particle mapping mode of measurement which allows for complete analysis of the mineralogy of the sample. Like the BMA, it allows for a robust determination of the bulk mineralogy, with mineral identities and proportions, along with average grain size measurements. The PMA mode also provides an analysis of the spatial characteristics of minerals, including liberation, association and grain size distribution, and it allows for determinative mineralogical analyses such as grade vs. recovery curves and mineral release curves.

### Introduction

One F7 molybdenite concentrate containing four fractions was submitted for mineralogical analysis from Crew Minerals in December 2007. Four graphite-impregnated 30mm polished sections were prepared, and the coarsest fraction was submitted for XRD analysis. The polished sections were carbon coated and analysed using the QEMSCAN Particle Mapping Analysis (PMA) mode. The resulting data was processed to separate touching particles, resulting in the following particle counts:

Fraction ( $\mu\text{m}$ )	Sections No.	Particle No.
-300/+106	1	2749
-106/+53	1	5011
-53/+20	1	5000
-20/+3	1	30059

Reports included are as follows:

- XRD summary
- Operational statistics
- Assay reconciliation
- Modal data and distribution graphs
- Mo liberation and corresponding image grid
- Mo association and example textures
- Mo grade-recovery curves
- Mo release curves
- Cumulative grain size distribution curves

CALR-11656-001  
 MI5004-DEC07  
 Crew Minerals-Hurdal

XRD Summary

Sample	Crystalline Mineral Assemblage (relative proportions based on peak height)			
	Major	Moderate	Minor	Trace
<b>F7 Mo Conc -106+53µm</b>	quartz	molybdenite plagioclase	potassium-feldspar pyrite	*dolomite, *mica *magnesite *pyroxene *pyrrhotite *tetrahedrite

\*Tentative identification due to low concentrations, diffraction line overlap, or poor crystallinity

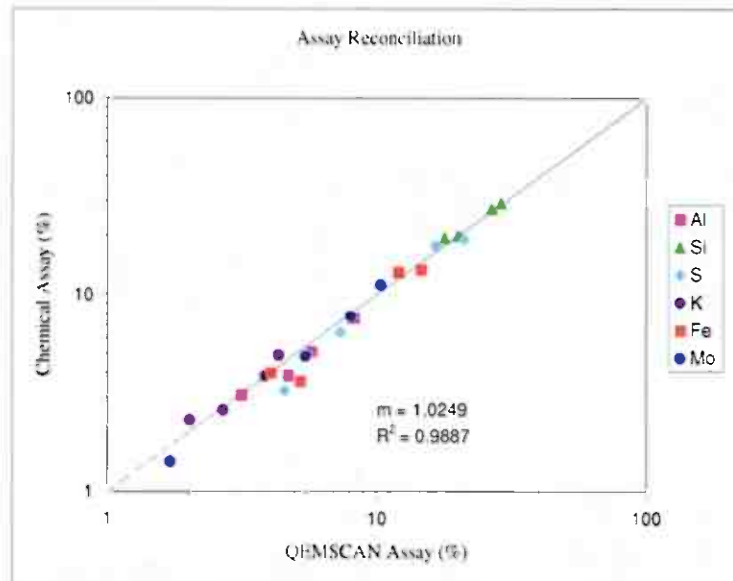
CALR-11656-001  
 MI5004-DEC07  
 Crew Minerals-Hurdal

Operational Statistics

Batch ID	MI5004-DEC07			
SIP ID	TONO			
Analysis Type	PMA			
Fraction ( $\mu\text{m}$ )	Sections No.	Pixel Size ( $\mu\text{m}$ )	Particle No.	Points No.
-300/+106 $\mu\text{m}$	1	5	2749	2852837
-106/+53 $\mu\text{m}$	1	4	5011	1582329
-53/+20 $\mu\text{m}$	1	2	5000	922188
-20/+3 $\mu\text{m}$	1	2	30059	267988

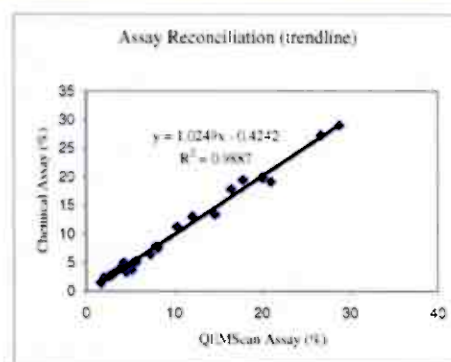
CALR-11656-001  
M15004-DHC07  
Crew Minerals-Hurdal

#### Assay Reconciliation



Fraction	Assays (%)												1:1 Line	
	Al		Si		S		K		Fe		Mo			
	QEM	Chem.	QEM	Chem.	QEM	Chem.	QEM	Chem.	QEM	Chem.	QEM	Chem.		
-300/+106µm	5.78	5.16	28.78	29.03	7.39	6.44	3.84	3.87	4.06	4.01	5.45	4.88	1	1
-106/+53µm	3.16	3.08	17.86	19.45	21.00	19.10	2.03	2.30	14.61	13.43	10.36	11.20	100	100
-53/+20µm	4.73	3.87	20.05	19.82	16.50	17.80	2.69	2.59	12.06	13.01	8.02	7.78		
-20/+3µm	8.27	7.62	26.63	27.25	4.56	3.26	4.34	4.94	5.24	3.62	1.72	1.42		

QEM	Chem.
5.78	5.16
3.16	3.08
4.73	3.87
8.27	7.62
28.78	29.03
17.86	19.45
20.05	19.82
26.63	27.25
7.39	6.44
21.00	19.10
16.50	17.80
4.56	3.26
3.84	3.87
2.03	2.30
2.69	2.59
4.34	4.94
4.06	4.01
14.61	13.43
12.06	13.01
5.24	3.62
5.45	4.88
10.36	11.20
8.02	7.78
1.72	1.42



CALR-11656-001  
M15004-DEC07  
Crew Minerals-Hurdal

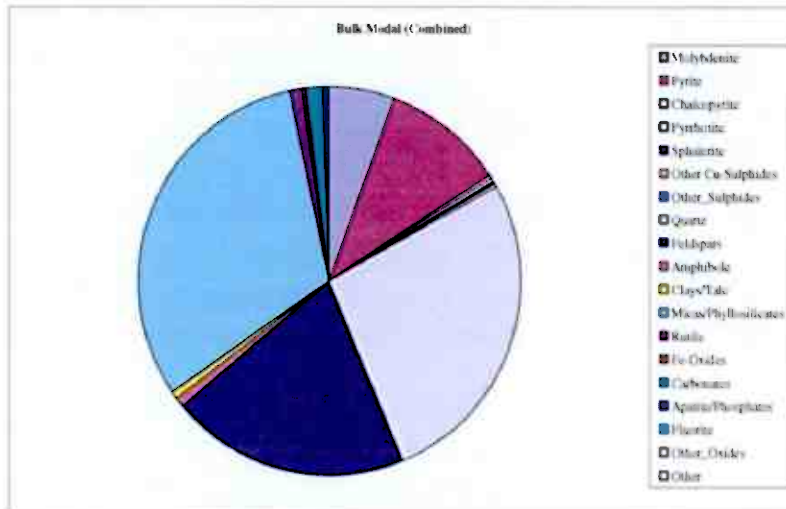
## Bulk Metal Analysis

Survey Sample Fraction	Name Id Name Name	Crew Minerals- Hurdal M15004-DEC07									
		17 Moly Con									
		Combined	-300/+106µm		-106/+53µm		-53/+20µm		-20/+3µm		
		Mass Size Distribution (%)	100.00	16.49	7.32	6.27	69.92				
	Particle Size (µm)	10	122	51	21	5					
		Combined	-300/+106µm		-106/+53µm		-53/+20µm		-20/+3µm		
		Sample	Sample	Fraction	Sample	Fraction	Sample	Fraction	Sample	Fraction	
Mineral Mass (%)	Molybdenite	5.66	1.51	9.14	1.28	17.48	0.85	13.57	2.02	2.89	
	Pyrite	10.04	1.29	7.80	2.14	29.19	1.48	23.65	5.14	7.35	
	Chalcopyrite	0.37	0.01	0.06	0.04	0.57	0.06	0.97	0.26	0.37	
	Pyrrhotite	0.41	0.02	0.15	0.07	1.01	0.03	0.44	0.29	0.41	
	Sphalerite	0.13	0.00	0.00	0.01	0.17	0.01	0.13	0.11	0.16	
	Other Cu-Sulphides	0.34	0.00	0.00	0.01	0.14	0.01	0.20	0.32	0.45	
	Other Sulphides	0.09	0.00	0.01	0.00	0.03	0.01	0.11	0.08	0.11	
	Quartz	26.51	4.98	30.22	1.60	21.87	1.25	19.91	18.68	26.71	
	Feldspars	20.26	6.63	40.18	1.42	19.33	1.57	25.10	10.65	15.23	
	Amphibole	0.91	0.06	0.34	0.04	0.59	0.04	0.63	0.77	1.11	
	Clays/Talc	0.49	0.11	0.65	0.04	0.53	0.03	0.46	0.32	0.45	
	Micas/Phyllosilicates	31.53	1.53	9.28	0.50	6.90	0.83	13.26	28.66	40.99	
	Rutile	1.12	0.06	0.38	0.03	0.42	0.02	0.30	1.01	1.44	
	Fe-Oxides	0.22	0.01	0.07	0.01	0.17	0.01	0.12	0.19	0.27	
	Carbonates	1.43	0.21	1.28	0.10	1.35	0.06	0.94	1.06	1.52	
	Apatite/Phosphates	0.35	0.05	0.31	0.02	0.21	0.01	0.15	0.27	0.39	
	Fluorite	0.02	0.01	0.09	0.00	0.01	0.00	0.03	0.00	0.01	
	Other Oxides	0.05	0.00	0.02	0.00	0.02	0.00	0.02	0.05	0.07	
	Other	0.04	0.00	0.02	0.00	0.01	0.00	0.01	0.03	0.05	
Gram Size (µm)	Molybdenite	+	44		28		14		8		
	Pyrite	+	72		49		24		8		
	Chalcopyrite	+	72		38		18		5		
	Pyrrhotite	+	26		20		8		6		
	Sphalerite	+	19		80		19		8		
	Other Cu-Sulphides	+	8		15		7		8		
	Other Sulphides	+	7		6		12		3		
	Quartz	+	66		40		14		5		
	Feldspars	+	43		28		14		6		
	Amphibole	+	11		10		5		5		
	Clays/Talc	+	8		8		4		3		
	Micas/Phyllosilicates	+	11		9		5		6		
	Rutile	+	23		18		11		7		
	Fe-Oxides	+	21		16		7		4		
	Carbonates	+	32		25		16		5		
	Apatite/Phosphates	+	34		21		9		4		
	Fluorite	+	26		11		14		4		
	Other Oxides	+	13		9		5		5		
	Other	+	9		9		8		4		



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MIS004-DEC07  
Crown Minerals-Hurdal

## Bulk Modal Analysis

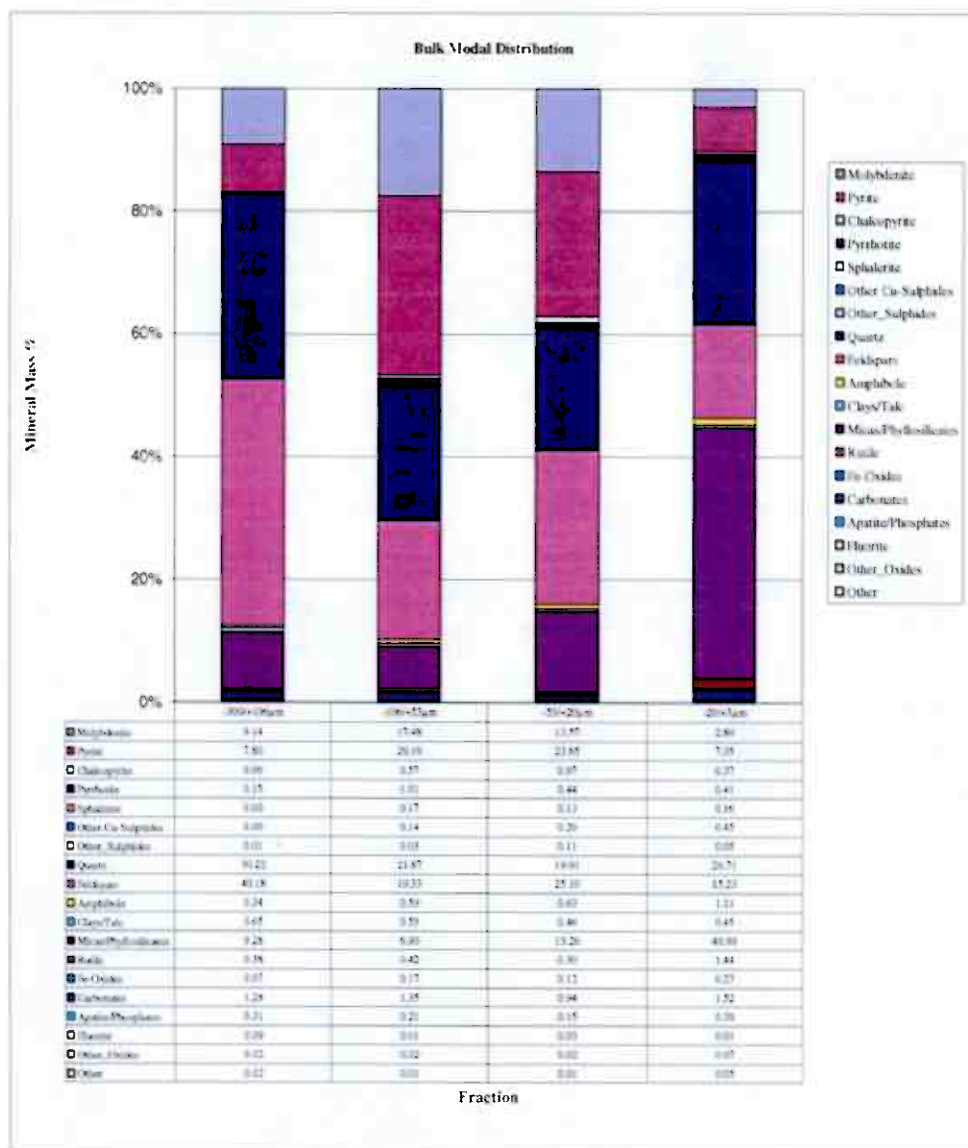


Mineral Mass %		Combined		-300 + 10µm		-106 + 5µm		-53 + 20µm		-20 + 3µm	
		Sample	Fraction	Sample	Fraction	Sample	Fraction	Sample	Fraction	Sample	Fraction
	Molybdenite	5.66	1.51	9.14	1.29	17.48	0.85	13.57	2.02	2.89	
	Pyrite	10.04	1.29	7.80	2.14	29.19	1.48	23.65	5.14	7.35	
	Chalcopyrite	0.37	0.01	0.06	0.04	0.57	0.06	0.97	0.26	0.37	
	Pyrrhotite	0.41	0.02	0.15	0.07	1.01	0.03	0.44	0.29	0.41	
	Sphalerite	0.13	0.00	0.00	0.01	0.17	0.01	0.13	0.11	0.16	
	Other Cu Sulphides	0.34	0.00	0.00	0.01	0.14	0.01	0.20	0.32	0.45	
	Other Sulphides	0.05	0.00	0.01	0.00	0.03	0.01	0.11	0.04	0.05	
	Quartz	26.51	4.98	30.22	1.60	21.87	1.25	19.91	18.68	26.71	
	Feldspar	20.25	6.63	40.18	1.42	19.33	1.57	25.10	10.65	15.23	
	Amphibole	0.91	0.06	0.34	0.04	0.59	0.04	0.63	0.77	1.11	
	Clays/Tals	0.49	0.11	0.65	0.04	0.53	0.03	0.46	0.32	0.45	
	Micas/Phyllosilicates	31.53	1.52	9.29	0.50	6.90	0.83	13.26	28.66	40.99	
	Rutile	1.12	0.06	0.38	0.03	0.42	0.02	0.30	1.01	1.44	
	Fe Oxides	0.22	0.01	0.07	0.01	0.17	0.01	0.12	0.19	0.27	
	Carbonates	1.43	0.21	1.29	0.10	1.35	0.06	0.94	1.06	1.52	
	Apatite/Phosphates	0.35	0.05	0.31	0.02	0.21	0.01	0.15	0.27	0.39	
	Fluorite	0.02	0.01	0.09	0.00	0.01	0.00	0.03	0.00	0.01	
	Other Oxides	0.05	0.00	0.02	0.00	0.02	0.00	0.02	0.05	0.07	
	Other	0.04	0.00	0.02	0.00	0.01	0.00	0.01	0.03	0.05	

Mineral Mass %		-300 + 10µm		-106 + 5µm		-53 + 20µm		-20 + 3µm	
		Sample	Fraction	Sample	Fraction	Sample	Fraction	Sample	Fraction
	Molybdenite	9.14	17.48	13.57	2.89				
	Pyrite	7.80	29.19	23.65	7.35				
	Chalcopyrite	0.06	0.57	0.97	0.37				
	Pyrrhotite	0.15	1.01	0.44	0.41				
	Sphalerite	0.00	0.17	0.13	0.16				
	Other Cu Sulphides	0.00	0.14	0.20	0.45				
	Other Sulphides	0.01	0.03	0.11	0.05				
	Quartz	30.22	21.87	19.91	26.71				
	Feldspar	40.18	19.33	25.10	15.23				
	Amphibole	0.34	0.59	0.63	1.11				
	Clays/Tals	0.65	0.53	0.46	0.45				
	Micas/Phyllosilicates	9.29	6.90	13.26	40.99				
	Rutile	0.38	0.42	0.30	1.44				
	Fe Oxides	0.07	0.17	0.12	0.27				
	Carbonates	1.29	1.35	0.94	1.52				
	Apatite/Phosphates	0.31	0.21	0.15	0.39				
	Fluorite	0.09	0.01	0.03	0.01				
	Other Oxides	0.02	0.02	0.02	0.07				
	Other	0.02	0.01	0.01	0.05				

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MIS-04-DEC07  
Crew Minerals Hurdal

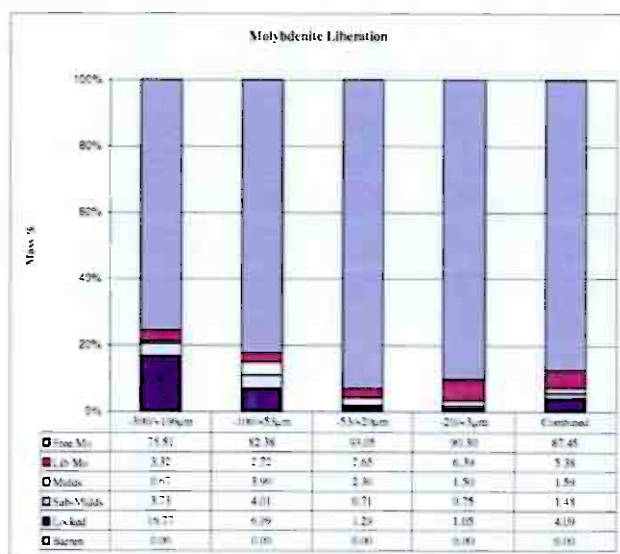
Bulk Mineral Analysis



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MIS904-DEC07  
Crew Minerals-Hurdal

Note: All Molybdenum occurs as molybdenite

#### Molybdenite Liberation



Categories are based on particle area percent

Free ≥ 95%; Lib <95%; < ≥ 80%; Midds <80% & ≥ 50%; Sub-Midds <50% & ≥ 20%; Locked <20%.

#### Calculations

##### Absolute Mineral Mass

	-300+106µm	-106+53µm	-53+20µm	-20+3µm	Combined
Free Mo	1.14	1.05	0.79	1.83	4.81
Lib Mo	0.05	0.03	0.02	0.13	0.24
Midds	0.01	0.05	0.02	0.03	0.11
Sub-Midds	0.06	0.05	0.01	0.02	0.13
Locked	0.25	0.09	0.01	0.02	0.37
Barren	0.00	0.00	0.00	0.00	0.00
Total	1.51	1.28	0.85	2.02	5.66

##### Normalized Mineral Mass

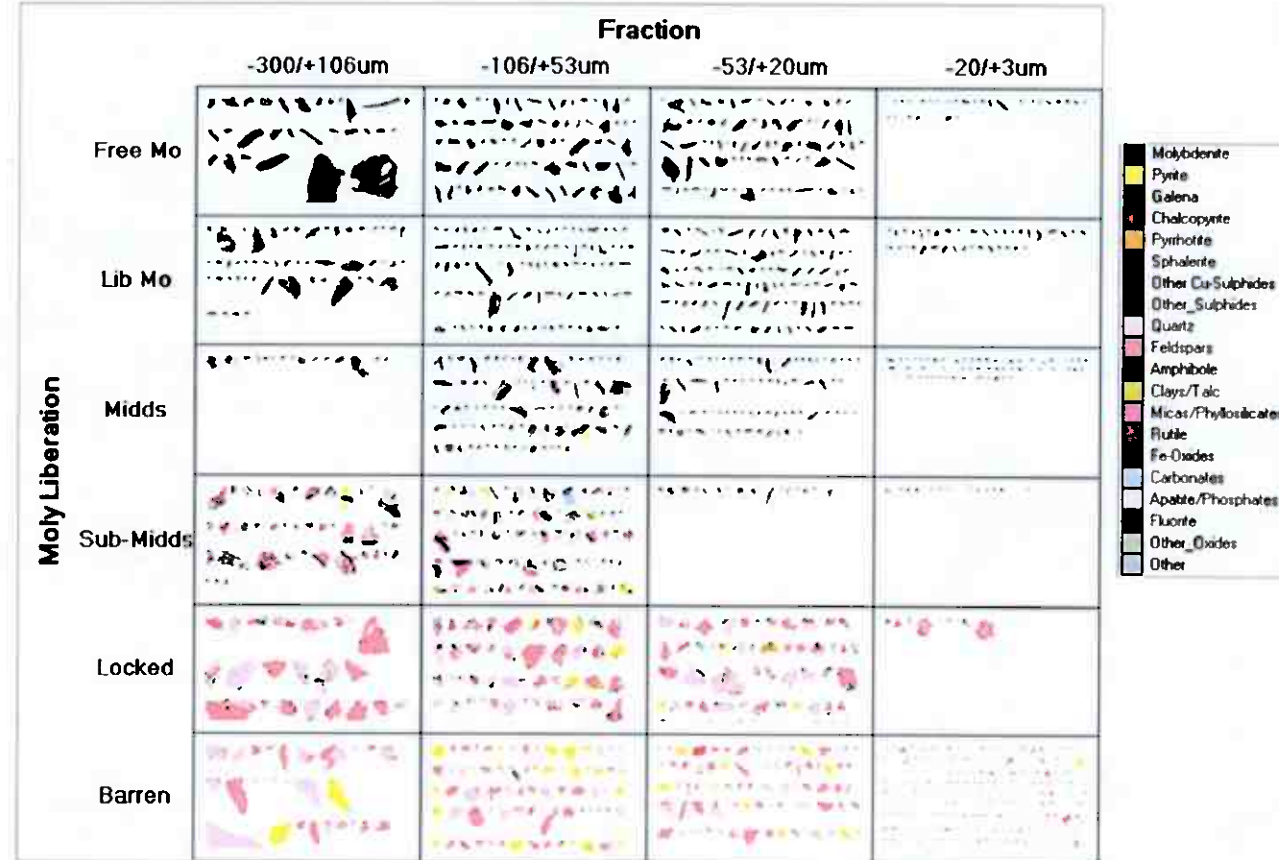
	-300+106µm	-106+53µm	-53+20µm	-20+3µm	Combined
Free Mo	75.51	82.38	93.05	90.30	87.45
Lib Mo	3.32	2.72	2.65	6.39	5.38
Midds	0.67	3.90	2.30	1.50	1.89
Sub-Midds	3.73	4.01	0.71	0.75	1.48
Locked	16.77	6.99	1.29	1.05	4.09
Barren	0.00	0.00	0.00	0.00	0.00
Total	100.00	100.00	100.00	100.00	100

##### Free - Liberated Molybdenite

	-300+106µm	-106+53µm	-53+20µm	-20+3µm
Free - Liberated Molybdenite	75.51	82.38	93.05	90.30

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Image Grid - Cu Sulphide Liberation

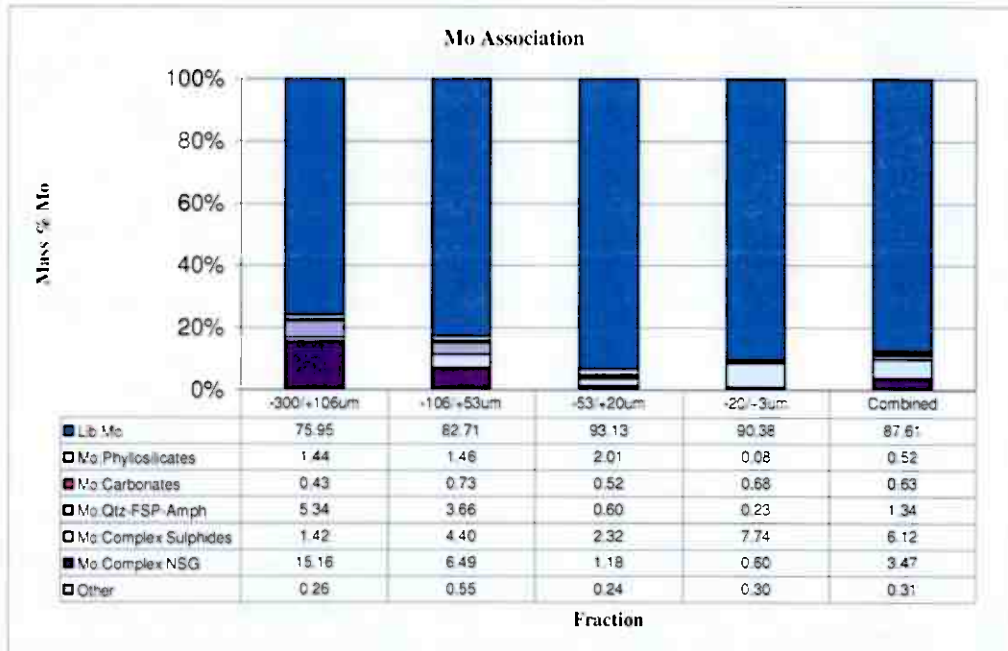


Categories are based on particle area percent:

Free >= 95%; Lib <95% & >= 80%; Midds <80% & >= 50%; Sub-Midds <50% & >= 20%; Locked <20%.

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M15004-DEC07  
Crew Minerals-Hurdal

#### Molybdenite Association



Note: Categories are based on having particles more than 95% of the combined mineral masses.

#### Mass of Molybdenite (g)

	-300/+106um	+106/+53um	-53/+20um	-20/+3um	Combined
Lib Mo	1.14	1.06	0.79	1.83	4.82
Mo:Qtz-FSP-Amph	0.08	0.05	0.01	0.00	0.14
Mo:Carbonates	0.01	0.01	0.00	0.01	0.03
Mo:Phyllosilicates	0.02	0.02	0.02	0.00	0.06
Mo:Complex Sulph	0.02	0.06	0.02	0.16	0.25
Mo:Complex NSG	0.23	0.08	0.01	0.01	0.33
Other	0.00	0.01	0.00	0.01	0.02
Total:	1.51	1.28	0.85	2.02	5.66

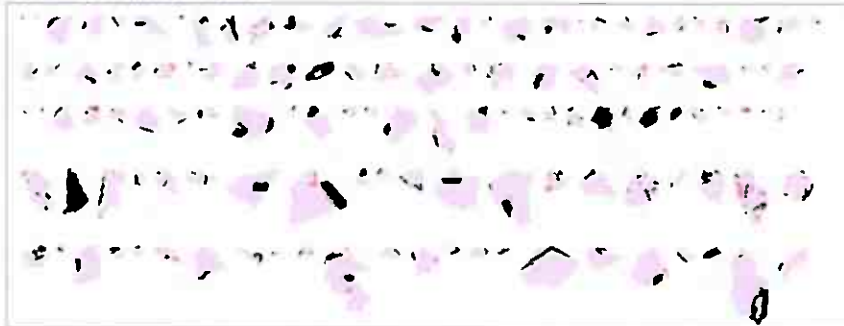
#### Normalized by fraction

	-300/+106um	+106/+53um	-53/+20um	-20/+3um	Combined
Lib Mo	75.95	82.71	93.13	90.38	87.61
Mo:Qtz-FSP-Amph	5.34	3.66	0.60	0.23	1.34
Mo:Carbonates	0.43	0.73	0.52	0.68	0.63
Mo:Phyllosilicates	1.44	1.46	2.01	0.08	0.52
Mo:Complex Sulphides	1.42	4.40	2.32	7.74	6.12
Mo:Complex NSG	15.16	6.49	1.18	0.60	3.47
Other	0.26	0.55	0.24	0.30	0.31
Total:	24.05	17.29	6.87	9.62	100.00

CALR-11656-001  
MIS004-DEC07  
Crew Minerals/Hurdal

Examples of Primary and Tertiary Mineral Textures in the Crew Minerals samples  
*Examples are from all fractions combined.*

Molybdenite + Quartz/Feldspar/Amphibole



Molybdenite Carbonates



Molybdenite Phyllosilicates



Molybdenite Complex Sulphides



Molybdenite Complex NSG

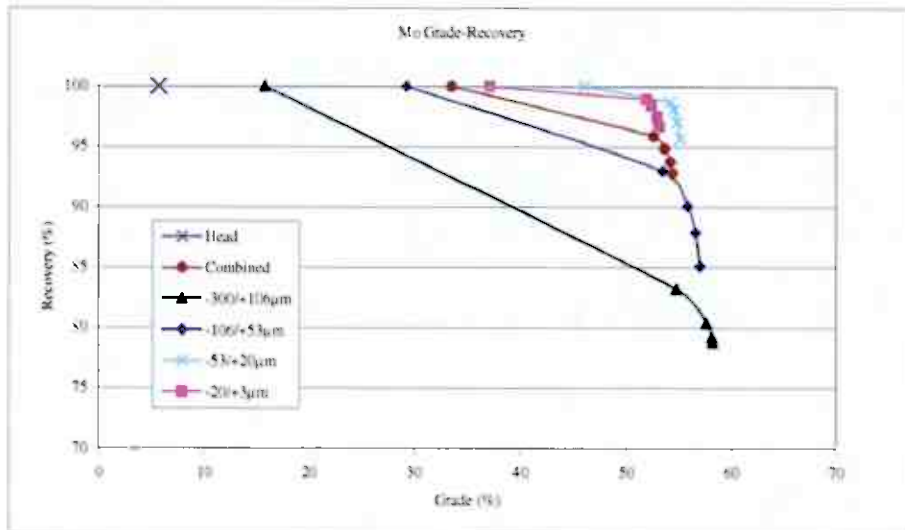


■	Molybdenite
■	Pyrite
■	Galena
■	Chalcopyrite
■	Pyrrhotite
■	Sphalerite
■	Other Cu Sulphides
■	Other Sulphides
■	Quartz
■	Feldspar
■	Amphibole
■	Clays/Talc
■	Micas/Phyllosilicates
■	Rutile
■	Fe-Oxides
■	Carbonates
■	Apatite/Phosphates
■	Fluorite
■	Other Oxides
■	Other



CALR-11656-001  
M15004-DEC07  
Crew Minerals-Hurdal

Mn Grade vs. Recovery



### Cautions

A. C. mode  
A. 2. 870-1000[illegible]

	30% $\alpha$ -value	50% $\alpha$ -value	70% $\alpha$ -value	90% $\alpha$ -value	Exponential
30% $\alpha$	0.71	0.68	0.66	1.13	0.68
50% $\alpha$	0.66	0.62	0.61	0.61	0.64
70% $\alpha$	0.61	0.62	0.61	0.61	0.64
90% $\alpha$	0.60	0.62	0.60	0.61	0.66
Exponential	0.76	0.68	0.67	0.61	0.62
Exponential	0.68	0.60	0.60	0.60	0.64
Exponential	0.61	0.61	0.61	0.61	0.65

### A.2. FURTHER VARIATION OF THE SCALAR CURVATURE

2000, 4, 11]

	Calc. (2000)	Exp. (2000)	Calc. (2000)	Exp. (2000)	Calc. (2000)	Exp. (2000)
Calc. (2000)	2.08	18.15	1.47	16.16	16.16	16.17
Calc. (2000)	0.71	0.62	0.22	0.39	0.39	0.34
Calc. (2000)	0.71	0.49	0.16	0.35	0.35	0.31
Calc. (2000)	0.75	0.66	0.09	0.36	0.36	0.36
Calc. (2000)	4.47	2.78	0.04	0.08	0.08	0.03
Calc. (2000)	0.00	0.00	0.00	0.00	0.00	0.00
Calc. (2000)	0.00	0.00	0.00	0.00	0.00	0.00

\_\_\_\_\_

542 A

	Male (n=10)	Female (n=10)	Male (n=10)	Female (n=10)	Unpaired
mean	21.99	19.77	18.77	24.56	97.11
SD	11.09	10.88	14.78	14.87	90.41
meanSD	21.00	20.77	14.74	37.29	49.72
SD	12.18	11.94	14.93	37.29	91.98
meanSD	28.67	22.60	37.22	37.74	100.00
SD	28.67	27.93	37.22	37.74	100.00

	2004-2005	2005-2006	2006-2007	2007-2008	2008-2009
2004	38.13	37.39	38.14	33.50	34.32
2004-2005	44.82	42.58	41.61	38.30	40.86
2005-2006	38.40	36.30	38.18	29.29	29.28
2006-2007	32.84	29.73	29.29	16.58	16.60
2007-2008	3.46	4.15	3.73	1.33	1.00
2008-2009	0.00	0.00	0.00	0.00	0.00

A. S. M... .. T. S. R. A. ...

15.25-6

	1997-1998	1998-1999	1999-2000	2000-2001	2001-2002
Female	19.38	17.77	26.76	27.17	46.71
Female(0)	10.71	1.78	0.50	0.71	10.86
Female(1)	8.67	1.78	0.44	1.04	1.62
Female(2)	3.29	2.65	0.27	0.97	4.06
Female(3)	175.14	38.80	5.11	28.02	47.79
Male	0.00	0.00	0.00	0.00	0.00

Figure 1. Schematic diagram of the experimental setup. The subjects were seated in a dimly lit room and viewed the screen through a mirror. The screen displayed the target and the starting position of the hand. The hand was moved from the starting position to the target position by the subject's own effort. The hand was then moved back to the starting position by the subject's own effort. The hand was then moved back to the starting position by the subject's own effort.

## 2422-5-79

	1990-1994	1995-1999	2000-2004	2005-2009	2010-2014	2015-2019
Age 60	16.58	13.33	16.38	67.17	66.11	66.11
Age 60-69	16.00	13.13	16.50	67.00	56.07	56.07
Age 70-79	17.18	16.57	17.00	67.00	60.00	60.00
Age 80-89	40.47	28.36	27.00	68.23	64.00	64.00
Age 90	108.50	77.47	71.00	86.53	100.00	100.00
All	108.55	71.47	71.00	86.53	100.00	100.00

8.22 1.2 4.2 4.2

## (5146)

	1995-1996	1996-1997	1997-1998	1998-1999	1999-2000
1995-1996	1995	1996	1997	1998	1999
1996-1997	1996	1997	1998	1999	2000
1997-1998	1997	1998	1999	2000	2001
1998-1999	1998	1999	2000	2001	2002
1999-2000	1999	2000	2001	2002	2003
2000-2001	2000	2001	2002	2003	2004

## B. Necessary

Year	Number of Males	Number of Females	Total
1990	100	100	200
1991	100	100	200
1992	100	100	200
1993	100	100	200
1994	100	100	200
1995	100	100	200
1996	100	100	200
1997	100	100	200
1998	100	100	200
1999	100	100	200
2000	100	100	200
2001	100	100	200
2002	100	100	200
2003	100	100	200
2004	100	100	200
2005	100	100	200
2006	100	100	200
2007	100	100	200
2008	100	100	200
2009	100	100	200
2010	100	100	200
2011	100	100	200
2012	100	100	200
2013	100	100	200
2014	100	100	200
2015	100	100	200
2016	100	100	200
2017	100	100	200
2018	100	100	200
2019	100	100	200
2020	100	100	200
2021	100	100	200
2022	100	100	200
2023	100	100	200
2024	100	100	200
2025	100	100	200
2026	100	100	200
2027	100	100	200
2028	100	100	200
2029	100	100	200
2030	100	100	200
2031	100	100	200
2032	100	100	200
2033	100	100	200
2034	100	100	200
2035	100	100	200
2036	100	100	200
2037	100	100	200
2038	100	100	200
2039	100	100	200
2040	100	100	200
2041	100	100	200
2042	100	100	200
2043	100	100	200
2044	100	100	200
2045	100	100	200
2046	100	100	200
2047	100	100	200
2048	100	100	200
2049	100	100	200
2050	100	100	200
2051	100	100	200
2052	100	100	200
2053	100	100	200
2054	100	100	200
2055	100	100	200
2056	100	100	200
2057	100	100	200
2058	100	100	200
2059	100	100	200
2060	100	100	200
2061	100	100	200
2062	100	100	200
2063	100	100	200
2064	100	100	200
2065	100	100	200
2066	100	100	200
2067	100	100	200
2068	100	100	200
2069	100	100	200
2070	100	100	200
2071	100	100	200
2072	100	100	200
2073	100	100	200
2074	100	100	200
2075	100	100	200
2076	100	100	200
2077	100	100	200
2078	100	100	200
2079	100	100	200
2080	100	100	200
2081	100	100	200

Grille Mo	2014	2015	2016	2017	2018	2019	2020	2021
Grille Mo	0.75	0.80	0.85	0.90	0.95	1.00	1.05	1.10
Grille Mo	0.80	0.85	0.90	0.95	1.00	1.05	1.10	1.15
Grille Mo	0.85	0.90	0.95	1.00	1.05	1.10	1.15	1.20
Grille Mo	0.90	0.95	1.00	1.05	1.10	1.15	1.20	1.25
Grille Mo	0.95	1.00	1.05	1.10	1.15	1.20	1.25	1.30
Grille Mo	1.00	1.05	1.10	1.15	1.20	1.25	1.30	1.35
Grille Mo	1.05	1.10	1.15	1.20	1.25	1.30	1.35	1.40
Grille Mo	1.10	1.15	1.20	1.25	1.30	1.35	1.40	1.45
Grille Mo	1.15	1.20	1.25	1.30	1.35	1.40	1.45	1.50
Grille Mo	1.20	1.25	1.30	1.35	1.40	1.45	1.50	1.55
Grille Mo	1.25	1.30	1.35	1.40	1.45	1.50	1.55	1.60
Grille Mo	1.30	1.35	1.40	1.45	1.50	1.55	1.60	1.65
Grille Mo	1.35	1.40	1.45	1.50	1.55	1.60	1.65	1.70
Grille Mo	1.40	1.45	1.50	1.55	1.60	1.65	1.70	1.75
Grille Mo	1.45	1.50	1.55	1.60	1.65	1.70	1.75	1.80
Grille Mo	1.50	1.55	1.60	1.65	1.70	1.75	1.80	1.85
Grille Mo	1.55	1.60	1.65	1.70	1.75	1.80	1.85	1.90
Grille Mo	1.60	1.65	1.70	1.75	1.80	1.85	1.90	1.95
Grille Mo	1.65	1.70	1.75	1.80	1.85	1.90	1.95	2.00
Grille Mo	1.70	1.75	1.80	1.85	1.90	1.95	2.00	2.05
Grille Mo	1.75	1.80	1.85	1.90	1.95	2.00	2.05	2.10
Grille Mo	1.80	1.85	1.90	1.95	2.00	2.05	2.10	2.15
Grille Mo	1.85	1.90	1.95	2.00	2.05	2.10	2.15	2.20
Grille Mo	1.90	1.95	2.00	2.05	2.10	2.15	2.20	2.25
Grille Mo	1.95	2.00	2.05	2.10	2.15	2.20	2.25	2.30
Grille Mo	2.00	2.05	2.10	2.15	2.20	2.25	2.30	2.35
Grille Mo	2.05	2.10	2.15	2.20	2.25	2.30	2.35	2.40
Grille Mo	2.10	2.15	2.20	2.25	2.30	2.35	2.40	2.45
Grille Mo	2.15	2.20	2.25	2.30	2.35	2.40	2.45	2.50
Grille Mo	2.20	2.25	2.30	2.35	2.40	2.45	2.50	2.55
Grille Mo	2.25	2.30	2.35	2.40	2.45	2.50	2.55	2.60
Grille Mo	2.30	2.35	2.40	2.45	2.50	2.55	2.60	2.65
Grille Mo	2.35	2.40	2.45	2.50	2.55	2.60	2.65	2.70
Grille Mo	2.40	2.45	2.50	2.55	2.60	2.65	2.70	2.75
Grille Mo	2.45	2.50	2.55	2.60	2.65	2.70	2.75	2.80
Grille Mo	2.50	2.55	2.60	2.65	2.70	2.75	2.80	2.85
Grille Mo	2.55	2.60	2.65	2.70	2.75	2.80	2.85	2.90
Grille Mo	2.60	2.65	2.70	2.75	2.80	2.85	2.90	2.95
Grille Mo	2.65	2.70	2.75	2.80	2.85	2.90	2.95	3.00
Grille Mo	2.70	2.75	2.80	2.85	2.90	2.95	3.00	3.05
Grille Mo	2.75	2.80	2.85	2.90	2.95	3.00	3.05	3.10
Grille Mo	2.80	2.85	2.90	2.95	3.00	3.05	3.10	3.15
Grille Mo	2.85	2.90	2.95	3.00	3.05	3.10	3.15	3.20
Grille Mo	2.90	2.95	3.00	3.05	3.10	3.15	3.20	3.25
Grille Mo	2.95	3.00	3.05	3.10	3.15	3.20	3.25	3.30
Grille Mo	3.00	3.05	3.10	3.15	3.20	3.25	3.30	3.35
Grille Mo	3.05	3.10	3.15	3.20	3.25	3.30	3.35	3.40
Grille Mo	3.10	3.15	3.20	3.25	3.30	3.35	3.40	3.45
Grille Mo	3.15	3.20	3.25	3.30	3.35	3.40	3.45	3.50
Grille Mo	3.20	3.25	3.30	3.35	3.40	3.45	3.50	3.55
Grille Mo	3.25	3.30	3.35	3.40	3.45	3.50	3.55	3.60
Grille Mo	3.30	3.35	3.40	3.45	3.50	3.55	3.60	3.65
Grille Mo	3.35	3.40	3.45	3.50	3.55	3.60	3.65	3.70
Grille Mo	3.40	3.45	3.50	3.55	3.60	3.65	3.70	3.75
Grille Mo	3.45	3.50	3.55	3.60	3.65	3.70	3.75	3.80
Grille Mo	3.50	3.55	3.60	3.65	3.70	3.75	3.80	3.85
Grille Mo	3.55	3.60	3.65	3.70	3.75	3.80	3.85	3.90
Grille Mo	3.60	3.65	3.70	3.75	3.80	3.85	3.90	3.95
Grille Mo	3.65	3.70	3.75	3.80	3.85	3.90	3.95	4.00
Grille Mo	3.70	3.75	3.80	3.85	3.90	3.95	4.00	4.05
Grille Mo	3.75	3.80	3.85	3.90	3.95	4.00	4.05	4.10
Grille Mo	3.80	3.85	3.90	3.95	4.00	4.05	4.10	4.15
Grille Mo	3.85	3.90	3.95	4.00	4.05	4.10	4.15	4.20
Grille Mo	3.90	3.95	4.00	4.05	4.10	4.15	4.20	4.25
Grille Mo	3.95	4.00	4.05	4.10	4.15	4.20	4.25	4.30
Grille Mo	4.00	4.05	4.10	4.15	4.20	4.25	4.30	4.35
Grille Mo	4.05	4.10	4.15	4.20	4.25	4.30	4.35	4.40
Grille Mo	4.10	4.15	4.20	4.25	4.30	4.35	4.40	4.45
Grille Mo	4.15	4.20	4.25	4.30	4.35	4.40	4.45	4.50
Grille Mo	4.20	4.25	4.30	4.35	4.40	4.45	4.50	4.55
Grille Mo	4.25	4.30	4.35	4.40	4.45	4.50	4.55	4.60
Grille Mo	4.30	4.35	4.40	4.45	4.50	4.55	4.60	4.65
Grille Mo	4.35	4.40	4.45	4.50	4.55	4.60	4.65	4.70
Grille Mo	4.40	4.45	4.50	4.55	4.60	4.65	4.70	4.75
Grille Mo	4.45	4.50	4.55	4.60	4.65	4.70	4.75	4.80
Grille Mo	4.50	4.55	4.60	4.65	4.70	4.75	4.80	4.85
Grille Mo	4.55	4.60	4.65	4.70	4.75	4.80	4.85	4.90
Grille Mo	4.60	4.65	4.70	4.75	4.80	4.85	4.90	4.95
Grille Mo	4.65	4.70	4.75	4.80	4.85	4.90	4.95	5.00
Grille Mo	4.70	4.75	4.80	4.85	4.90	4.95	5.00	5.05
Grille Mo	4.75	4.80	4.85	4.90	4.95	5.00	5.05	5.10
Grille Mo	4.80	4.85	4.90	4.95	5.00	5.05	5.10	5.15
Grille Mo	4.85	4.90	4.95	5.00	5.05	5.10	5.15	5.20
Grille Mo	4.90	4.95	5.00	5.05	5.10	5.15	5.20	5.25
Grille Mo	4.95	5.00	5.05	5.10	5.15	5.20	5.25	5.30
Grille Mo	5.00	5.05	5.10	5.15	5.20	5.25	5.30	5.35
Grille Mo	5.05	5.10	5.15	5.20	5.25	5.30	5.35	5.40
Grille Mo	5.10	5.15	5.20	5.25	5.30	5.35	5.40	5.45
Grille Mo	5.15	5.20	5.25	5.30	5.35	5.40	5.45	5.50
Grille Mo	5.20	5.25	5.30	5.35	5.40	5.45	5.50	5.55
Grille Mo	5.25	5.30	5.35	5.40	5.45	5.50	5.55	5.60
Grille Mo	5.30	5.35	5.40	5.45	5.50	5.55	5.60	5.65
Grille Mo	5.35	5.40	5.45	5.50	5.55	5.60	5.65	5.70
Grille Mo	5.40	5.45	5.50	5.55	5.60	5.65	5.70	5.75
Grille Mo	5.45	5.50	5.55	5.60	5.65	5.70	5.75	5.80
Grille Mo	5.50	5.55	5.60	5.65	5.70	5.75	5.80	5.85
Grille Mo	5.55	5.60	5.65	5.70	5.75	5.80	5.85	5.90
Grille Mo	5.60	5.65	5.70	5.75	5.80	5.85	5.90	5.95
Grille Mo	5.65	5.70	5.75	5.80	5.85	5.90	5.95	6.00
Grille Mo	5.70	5.75	5.80	5.85	5.90	5.95	6.00	6.05
Grille Mo	5.75	5.80	5.85	5.90	5.95	6.00	6.05	6.10
Grille Mo	5.80	5.85	5.90	5.95	6.00	6.05	6.10	6.15
Grille Mo	5.85	5.90	5.95	6.00	6.05	6.10	6.15	6.20
Grille Mo	5.90	5.95	6.00	6.05	6.10	6.15	6.20	6.25
Grille Mo	5.95	6.00	6.05	6.10	6.15	6.20	6.25	6.30
Grille Mo	6.00	6.05	6.10	6.15	6.20	6.25	6.30	6.35
Grille Mo	6.05	6.10	6.15	6.20	6.25	6.30	6.35	6.40
Grille Mo	6.10	6.15	6.20	6.25	6.30	6.35	6.40	6.45
Grille Mo	6.15	6.20	6.25	6.30	6.35	6.40	6.45	6.50
Grille Mo	6.20	6.25	6.30	6.35	6.40	6.45	6.50	6.55
Grille Mo	6.25	6.30	6.35	6.40	6.45	6.50	6.55	6.60
Grille Mo	6.30	6.35	6.40	6.45	6.50	6.55	6.60	6.65
Grille Mo	6.35	6.40	6.45	6.50	6.55	6.60	6.65	6.70
Grille Mo	6.40	6.45	6.50	6.55	6.60	6.65	6.70	6.75
Grille Mo	6.45	6.50	6.55	6.60	6.65	6.70	6.75	6.80
Grille Mo	6.50	6.55	6.60	6.65	6.70	6.75	6.80	6.85
Grille Mo	6.55	6.60	6.65	6.70	6.75	6.80	6.85	6.90
Grille Mo	6.60	6.65	6.70	6.75	6.80	6.85	6.90	6.95
Grille Mo	6.65	6.70	6.75	6.80	6.85	6.90	6.95	7.00
Grille Mo	6.70	6.75	6.80	6.85	6.90	6.95	7.00	7.05
Grille Mo	6.75	6.80	6.85	6.90	6.95	7.00	7.05	7.10
Grille Mo	6.80	6.85	6.90	6.95	7.00	7.05	7.10	7.15
Grille Mo	6.85	6.90	6.95	7.00	7.05	7.10	7.15	7.20
Grille Mo	6.90	6.95	7.00	7.05	7.10	7.15	7.20	7.25
Grille Mo	6.95	7.00	7.05	7.10	7.15	7.20	7.25	7.30
Grille Mo	7.00	7.05	7.10	7.15	7.20	7.25	7.30	7.35
Grille Mo	7.05	7.10	7.15	7.20	7.25	7.30	7.35	7.40
Grille Mo	7.10	7.15	7.20	7.25	7.30	7.35	7.40	7.45
Grille Mo	7.15	7.20	7.25	7.30	7.35	7.40	7.45	7.50
Grille Mo	7.20	7.25	7.30	7.35	7.40	7.45	7.50	7.55
Grille Mo	7.25	7.30	7.35	7.40	7.45	7.50	7.55	7.60
Grille Mo	7.30	7.35	7.40	7.45	7.50	7.55	7.60	7.65
Grille Mo	7.35	7.40	7.45	7.50	7.55	7.60	7.65	7.70
Grille Mo	7.40	7.45	7.50	7.55	7.60	7.65	7.70	7.75
Grille Mo	7.45	7.50	7.55	7.60	7.65	7.70	7.75	7.80
Grille Mo	7.50	7.55	7.60	7.65	7.70	7.75	7.80	7.85
Grille Mo	7.55	7.60	7.65	7.70	7.75	7.80	7.85	7.90
Grille Mo	7.60	7.65	7.70	7.75	7.80	7.85	7.90	7.95
Grille Mo	7.65	7.70	7.75	7.80	7.85	7.90	7.95	8.00
Grille Mo	7.70	7.75	7.80	7.85	7.90	7.95	8.00	8.05
Grille Mo	7.75	7.80	7.85	7.90	7.95	8.00	8.05	8.10
Grille Mo	7.80	7.85	7.90	7.95	8.00	8.05	8.10	8.15
Grille Mo	7.85	7.90	7.95	8.00	8.05	8.10	8.15	8.20
Grille Mo	7.90	7.95	8.00	8.05	8.10	8.15	8.20	8.25
Grille Mo	7.95	8.00	8.05	8.10	8.15	8.20	8.25	8.30
Grille Mo	8.00	8.05	8.10	8.15	8.20	8.25	8.30	8.35
Grille Mo	8.05	8.10	8.15					

P. J. CHEN, M. A. L. W. S. YIP, S. C. CHAN

**Box 1**

	1990-1991	1991-1992	1992-1993	1993-1994	1994-1995	1995-1996
Arabi	79.53	85.11	90.10	95.09	99.08	100.00
(Arabi/Arabi)	1.00	1.09	1.27	1.53	1.64	1.66
Algeria/Arabi	1.56	2.05	1.90	2.00	2.00	2.00
(Arabi/Algeria)	2.62	2.33	2.58	2.45	2.45	2.45
(Algeria/Algeria)	16.77	6.89	1.29	1.50	1.50	1.50
Iran	0.00	0.00	0.00	0.00	0.00	0.00
Iran/Algeria	0.00	0.00	0.00	0.00	0.00	0.00

\_\_\_\_\_

Fig. 14

	100, $\mu\text{m}$	176, $\mu\text{m}$	63, $\mu\text{m}$	25, $\mu\text{m}$	Range
A <sub>1</sub> -A <sub>2</sub>	75.23	66.13	67.35	68.75	65.94
A <sub>1</sub> 0-A <sub>1</sub> 00	75.24	67.96	67.91	68.72	65.94
A <sub>1</sub> 0-A <sub>1</sub> 00	86.45	77.68	78.11	78.52	75.97
A <sub>1</sub> 0-A <sub>1</sub> 00	83.20	74.41	74.71	75.35	72.91
A <sub>1</sub> 0-A <sub>1</sub> 00	77.50	68.70	69.08	70.20	67.46
A <sub>1</sub> 0	75.23	66.13	67.35	68.75	65.94

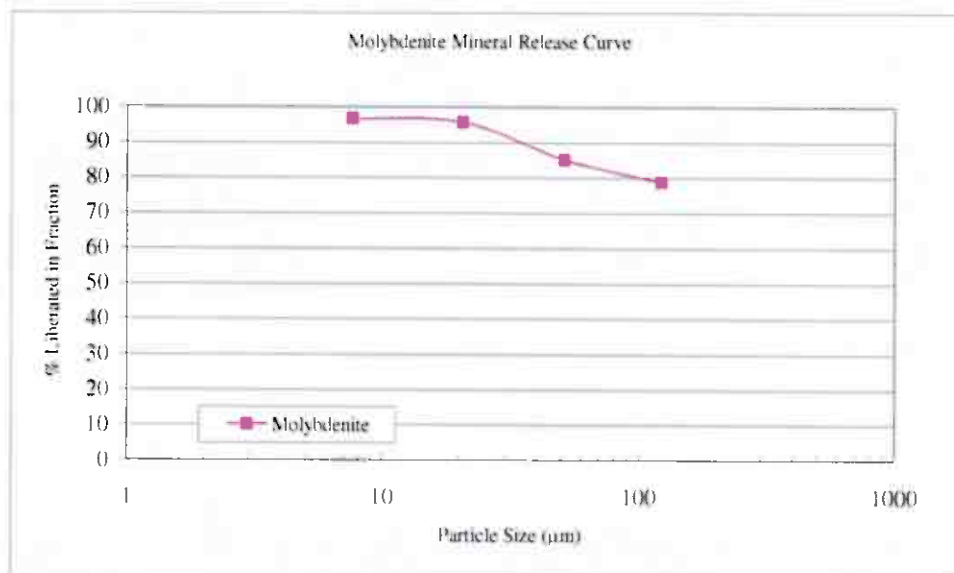
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	Number	Percentage
Absent	7	10%



CALR-11656-001  
 M15004-DEC07  
 Crew Minerals-Hurdal

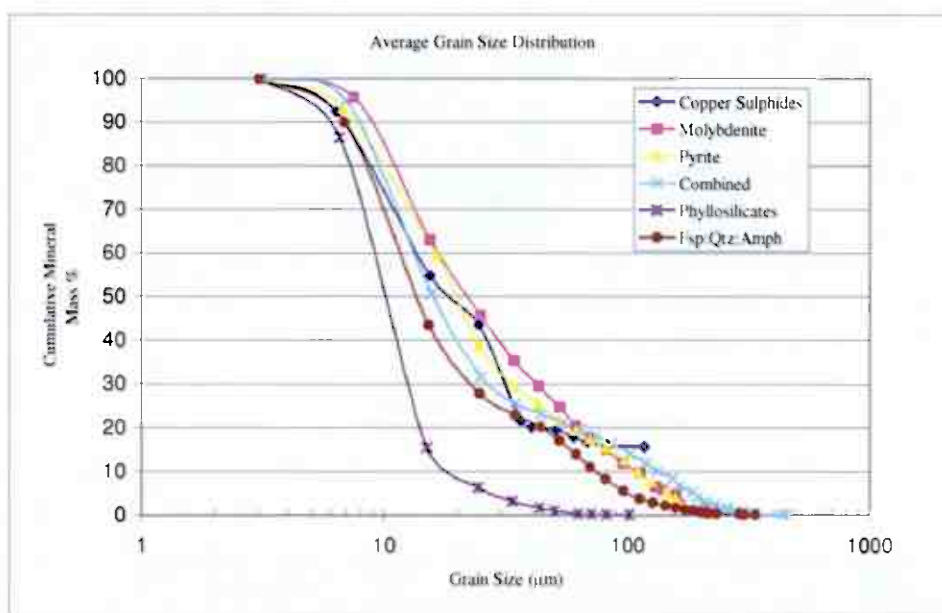
# Mineral Release Curves



Name	-300/+106µm	-106/+53µm	-53/+20µm	-20/+3µm
Particle Size	121.92	51.08	20.61	7.59
Mineral Mass %				
Molybdenite 80% Lib	78.83	85.10	95.70	96.69

CAIR-11656-001  
M15004-DEC07  
Crew Minerals-Hurdal

Average Grain Size Distribution



All Particles

	Size	Mass		Size	Mass
+600	0.00	0.00	+600		0.00
+540	0.00	0.00	+540		0.00
+480	0.00	0.00	+480		0.00
+420	460.40	0.09	+420	460.40	0.09
+390	436.68	0.06	+390	436.68	0.15
+360	0.00	0.00	+360		0.15
+330	338.74	0.04	+330	338.74	0.19
+300	330.97	0.27	+300	330.97	0.45
+270	296.79	0.30	+270	296.79	0.75
+255	277.98	0.15	+255	277.98	0.90
+240	259.03	0.44	+240	259.03	1.35
+225	256.13	0.42	+225	256.13	1.76
+210	229.73	0.66	+210	229.73	2.42
+195	209.19	0.64	+195	209.19	3.06
+180	195.09	1.00	+180	195.09	4.06
+165	185.78	1.26	+165	185.78	5.32
+150	163.66	1.42	+150	163.66	6.74
+135	154.03	1.58	+135	154.03	8.32
+120	133.53	1.74	+120	133.53	10.06
+105	119.26	1.93	+105	119.26	11.99
+90	102.61	2.11	+90	102.61	14.10
+75	87.05	2.34	+75	87.05	16.44
+66	74.07	1.58	+66	74.07	18.01
+57	64.27	1.50	+57	64.27	19.51
+48	53.96	1.62	+48	53.96	21.13
+39	44.20	1.99	+39	44.20	23.13
+30	34.60	2.30	+30	34.60	25.43
+21	25.10	6.28	+21	25.10	31.70
+12	15.67	18.92	+12	15.67	50.62
+4	6.95	44.21	+4	6.95	94.84
-4	3.15	5.16	-4	3.15	100.00
Total:		100.00			

Molybdenite

	Size	Mass	Norm		Size	Mass
+600	0.00	0.00	0.00	+600		0.00
+540	0.00	0.00	0.00	+540		0.00
+480	0.00	0.00	0.00	+480		0.00
+420	0.00	0.00	0.00	+420		0.00
+390	0.00	0.00	0.00	+390		0.00
+360	0.00	0.00	0.00	+360		0.00
+330	0.00	0.00	0.00	+330		0.00
+300	0.00	0.00	0.00	+300		0.00
+270	0.00	0.00	0.00	+270		0.00
+255	0.00	0.00	0.00	+255		0.00
+240	0.00	0.00	0.00	+240		0.00
+225	226.20	0.04	0.62	+225	226.20	0.62
+210	0.00	0.00	0.00	+210		0.62
+195	206.74	0.04	0.68	+195	206.74	1.30
+180	0.00	0.00	0.00	+180		1.30
+165	165.69	0.06	1.00	+165	165.69	2.31
+150	158.01	0.13	2.37	+150	158.01	4.67
+135	140.06	0.06	0.98	+135	140.06	5.65
+120	131.49	0.04	0.79	+120	131.49	6.44
+105	112.73	0.18	3.28	+105	112.73	9.72
+90	96.05	0.12	2.10	+90	96.05	11.83
+75	81.71	0.18	3.24	+75	81.71	15.07
+66	69.95	0.15	2.66	+66	69.95	17.73
+57	61.41	0.15	2.76	+57	61.41	20.49
+48	52.64	0.23	4.12	+48	52.64	24.61
+39	43.11	0.27	4.88	+39	43.11	29.50
+30	34.15	0.32	5.75	+30	34.15	35.25
+21	24.96	0.59	10.44	+21	24.96	45.69
+12	15.42	0.97	17.32	+12	15.42	63.00
+4	7.50	1.83	32.69	+4	7.50	95.69
-4	3.10	0.24	4.31	-4	3.10	100.00
Total:		5.61	100.00			

Pyrite

	Size	Mass		Size	Mass
+600	0.00	0.00	+600		0.00
+540	0.00	0.00	+540		0.00
+480	0.00	0.00	+480		0.00
+420	0.00	0.00	+420		0.00
+390	0.00	0.00	+390		0.00
+360	0.00	0.00	+360		0.00
+330	0.00	0.00	+330		0.00
+300	0.00	0.00	+300		0.00
+270	0.00	0.00	+270		0.00
+255	0.00	0.00	+255		0.00
+240	0.00	0.00	+240		0.00
+225	0.00	0.00	+225		0.00
+210	216.52	0.25	+210	216.52	0.25
+195	201.12	0.56	+195	201.12	0.81
+180	192.20	0.66	+180	192.20	1.47
+165	170.43	0.39	+165	170.43	1.86
+150	157.23	1.98	+150	157.23	3.85
+135	144.23	1.38	+135	144.23	5.23
+120	124.89	2.40	+120	124.89	7.63
+105	110.95	2.26	+105	110.95	9.89
+90	96.79	2.73	+90	96.79	12.62
+75	81.86	2.93	+75	81.86	15.56
+66	70.09	1.89	+66	70.09	17.44
+57	61.53	1.88	+57	61.53	19.33
+48	52.44	2.20	+48	52.44	21.52
+39	42.89	4.04	+39	42.89	25.56
+30	34.36	3.83	+30	34.36	29.40
+21	24.47	9.24	+21	24.47	38.64
+12	16.37	20.66	+12	16.37	59.30
+4	6.76	33.86	+4	6.76	93.16
-4	3.11	6.84	-4	3.11	100.00
Total:		100.00			

## Phyllosilicates

	Size	Mass		Size	Mass
+600	0.00	0.00	+600		0.00
+540	0.00	0.00	+540		0.00
+480	0.00	0.00	+480		0.00
+420	0.00	0.00	+420		0.00
+390	0.00	0.00	+390		0.00
+360	0.00	0.00	+360		0.00
+330	0.00	0.00	+330		0.00
+300	0.00	0.00	+300		0.00
+270	0.00	0.00	+270		0.00
+255	0.00	0.00	+255		0.00
+240	0.00	0.00	+240		0.00
+225	0.00	0.00	+225		0.00
+210	0.00	0.00	+210		0.00
+195	0.00	0.00	+195		0.00
+180	0.00	0.00	+180		0.00
+165	0.00	0.00	+165		0.00
+150	0.00	0.00	+150		0.00
+135	0.00	0.00	+135		0.00
+120	0.00	0.00	+120		0.00
+105	0.00	0.00	+105		0.00
+90	101.81	0.06	+90	101.81	0.06
+75	82.08	0.00	+75	82.08	0.07
+66	70.99	0.11	+66	70.99	0.17
+57	62.85	0.05	+57	62.85	0.22
+48	50.12	0.78	+48	50.12	1.01
+39	43.40	0.60	+39	43.40	1.60
+30	33.54	1.52	+30	33.54	3.12
+21	24.39	3.19	+21	24.39	6.32
+12	14.97	9.15	+12	14.97	15.47
+4	6.55	71.00	+4	6.55	86.47
-4	3.08	13.53	-4	3.08	100.00
Total:		100.00			

Fsp:Qtz:Amph

	Size	Mass		Size	Mass
+600	0.00	0.00	+600		0.00
+540	0.00	0.00	+540		0.00
+480	0.00	0.00	+480		0.00
+420	0.00	0.00	+420		0.00
+390	0.00	0.00	+390		0.00
+360	0.00	0.00	+360		0.00
+330	335.76	0.07	+330	335.76	0.07
+300	302.11	0.02	+300	302.11	0.09
+270	288.30	0.17	+270	288.30	0.26
+255	0.00	0.00	+255		0.26
+240	0.00	0.00	+240		0.26
+225	232.31	0.07	+225	232.31	0.33
+210	213.28	0.08	+210	213.28	0.40
+195	200.51	0.18	+195	200.51	0.58
+180	186.00	0.45	+180	186.00	1.03
+165	171.98	0.22	+165	171.98	1.25
+150	157.30	0.39	+150	157.30	1.64
+135	142.62	0.47	+135	142.62	2.11
+120	126.97	0.66	+120	126.97	2.77
+105	111.96	0.99	+105	111.96	3.76
+90	96.35	1.71	+90	96.35	5.47
+75	81.24	2.72	+75	81.24	8.19
+66	70.10	2.76	+66	70.10	10.95
+57	61.49	2.93	+57	61.49	13.87
+48	52.36	3.17	+48	52.36	17.04
+39	43.65	3.21	+39	43.65	20.25
+30	34.49	2.61	+30	34.49	22.87
+21	24.71	4.94	+21	24.71	27.81
+12	15.26	15.67	+12	15.26	43.48
+4	6.85	46.48	+4	6.85	89.96
-4	3.03	10.04	-4	3.03	100.00
Total:		100.00			

## Copper Sulphides

	Size	Mass		Size	Mass
+600	0,00	0,00	+600		0.00
+540	0,00	0,00	+540		0.00
+480	0,00	0,00	+480		0.00
+420	0,00	0,00	+420		0.00
+390	0,00	0,00	+390		0.00
+360	0,00	0,00	+360		0.00
+330	0,00	0,00	+330		0.00
+300	0,00	0,00	+300		0.00
+270	0,00	0,00	+270		0.00
+255	0,00	0,00	+255		0.00
+240	0,00	0,00	+240		0.00
+225	0,00	0,00	+225		0.00
+210	0,00	0,00	+210		0.00
+195	0,00	0,00	+195		0.00
+180	0,00	0,00	+180		0.00
+165	0,00	0,00	+165		0.00
+150	0,00	0,00	+150		0.00
+135	0,00	0,00	+135		0.00
+120	0,00	0,00	+120		0.00
+105	117,51	15,54	+105	117,51	15.54
+90	0,00	0,00	+90		15.54
+75	83,28	0,46	+75	83,28	16.00
+66	68,58	0,65	+66	68,58	16.65
+57	59,95	1,09	+57	59,95	17.74
+48	50,93	1,77	+48	50,93	19.51
+39	40,16	0,56	+39	40,16	20.06
+30	36,22	1,47	+30	36,22	21.53
+21	24,53	21,97	+21	24,53	43.50
+12	15,44	11,26	+12	15,44	54.76
+4	6,37	37,56	+4	6,37	92.32
-4	3,09	7,68	-4	3,09	100.00
Total:		100.00			